# ASKAP's primary beams and their measurement PAF & Advanced Receivers 2022

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Image credit: Alex Cherney / terrastro.com

www.csiro.au

- Importance of antenna reception pattern
  - Interpretation of receiver output
  - Including polarisation response

Fig. 2.5 The power pattern  $A(\theta)$  of an antenna pointed in the direction OC, and the intensity profile of a source  $I_1(\theta')$ , used to illustrate the convolution relationship. The angle  $\theta$  is measured with respect to the beam center OC. The profile of the source is a function of  $\theta'$ , measured with respect to the direction of the nominal position of the source OB.



From Interferometry and Synthesis in Radio Astronomy, Thompson, Moran and Swenson (2017)

- Conventional receivers have stable reception patterns
  - Transducer normally inside a machined metal feed
    - Initial measurement of pattern
    - Subsequent occasional confirmation





**Figure 3.** Co-polar and cross-polar directivity patterns of the feed horn. Each pane shows the performance of the feed over the 0.7-4.2GHz frequency range. The Gaussian pattern used to optimize the beam patterns is displayed in each plane as a reference (dashed, black).

Dunning, Bowen, Bourne, Hayman and Smith, *An ultra-wideband dielectrically loaded quad-ridged feed horn for radio astronomy*, 2015 IEEE-APS Topical Conference on Antennas and Propagation in Wireless Communications (APWC), Turin, 2015, pp. 787-790.

URL: <u>http://ieeexplore.ieee.org/stamp/stamp.jsp?tp=&arnumber=7300180&isnumber=7300131</u>

- Synthetic beams from PAFs are
  - Less stable dependence on many electronic components



ASKAP Mk II PAF

Image credit: Steve Barker

• Are frequently reconfigured for different astronomical applications



- •Therefore successful astronomy demands routine measurement of patterns
- For ASKAP, we use holography
- •The lesson from RACS:

(Rapid ASKAP Continuum Survey; McConnell et al., 2020)



## **Measurement practice with ASKAP**

#### Sampling the data



## The formalism

Measured electric field

$$\begin{split} \mathbf{E}' &= \begin{pmatrix} E'_X \\ E'_Y \end{pmatrix} = \begin{pmatrix} a_1 & a_2 \\ a_3 & a_4 \end{pmatrix} \begin{pmatrix} E_X \\ E_X \end{pmatrix} = \mathbf{J}\mathbf{E} \\ \mathbf{J}_{\text{gain}} &= \begin{pmatrix} g_X & 0 \\ 0 & g_Y \end{pmatrix} \qquad \mathbf{J}_{\text{leak}} = \begin{pmatrix} 1 & D_X \\ D_Y & 1 \end{pmatrix} \end{split}$$

Correlation between two antennas (coherency vector)

$$\mathbf{R}_{ij}' = \langle \mathbf{E}_{i}' \otimes \mathbf{E}_{j}'^{*} \rangle = \langle \mathbf{J}_{i} \mathbf{E}_{i} \otimes \mathbf{J}_{j}^{*} \mathbf{E}_{j}^{*} \rangle = \begin{pmatrix} R_{XX}' \\ R_{YY}' \\ R_{YX}' \\ R_{YY}' \end{pmatrix}_{ij}$$

$$\mathbf{R}'_{ij} = (\mathbf{J}_i \otimes \mathbf{J}_j^*) \mathbf{R}_{ij}$$

$$\mathbf{R}'_{ij} = \begin{pmatrix} g_{iX}g_{jX}^{*} & g_{iX}g_{jX}^{*}D_{jX}^{*} & g_{iX}g_{jX}^{*}D_{iX} & g_{iX}g_{jX}^{*}D_{iX}D_{jX}^{*} \\ g_{iX}g_{jY}^{*}D_{jY}^{*} & g_{iX}g_{jY}^{*} & g_{iX}g_{jY}^{*}D_{iX}D_{jY}^{*} \\ g_{iY}g_{jX}^{*}D_{iY} & g_{iY}g_{jX}^{*}D_{iY}D_{jX}^{*} & g_{iY}g_{jX}^{*}D_{*jX} \\ g_{iY}g_{jY}^{*}D_{iY}D_{jY}^{*} & g_{iY}g_{jY}^{*}D_{iY} & g_{iY}g_{jY}^{*}D_{jY}^{*} \\ g_{iY}g_{jY}^{*}D_{iY}D_{jY}^{*} & g_{iY}g_{jY}^{*}D_{iY} & g_{iY}g_{jY}^{*}D_{jY}^{*} \\ \end{pmatrix} \mathbf{R}_{ij}$$

# The formalism

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Let antennas *i*, *j* be the reference and target.

Antenna *i* is fixed in the reference source

Assume  $g_{iX}$ ,  $g_{iY}$  constant and  $D_{iX}$ ,  $D_{iY} = 0$ 

Assume reference source is unpolarised so  $R_{ij} = (R_{XX}, 0, 0, R_{YY})$ 

$$R'_{XX} = R_{XX}g_{iX}g_{jX}^*$$
$$R'_{XY} = R_{XX}g_{iX}g_{jY}^*D_{jY}^*$$
$$R'_{YX} = R_{YY}g_{iY}g_{jX}^*D_{jX}^*$$
$$R'_{YY} = R_{YY}g_{iY}g_{jY}^*$$

## The formalism

 $R'_{XX} = R_{XX}g_{iX}g_{jX}^*$  $R'_{XY} = R_{XX}g_{iX}g_{jY}^*D_{jY}^*$  $R'_{YX} = R_{YY}g_{iY}g_{jX}^*D_{jX}^*$  $R'_{YY} = R_{YY}g_{iY}g_{jY}^*$ 

For the target antennas, the apparent gain is a function of angular coordinates  $g_j = g_j(l,m)$ 

So we can normalise the *R*' quantities by their values at the beam centre:

$$\mathcal{R}'_{XX}(l,m) = \frac{R_{XX}g_{iX}g_{jX}^*(l,m)}{R_{XX}g_{iX}g_{jX}^*(0,0)} = \frac{g_{jX}^*(l,m)}{g_{jX}^*(0,0)}$$

Conversion to relative power images in Stokes (I,Q,U,V)

# The procedure

- Select correlations between reference and each target antenna
- For each antenna, beam and frequency channel, normalise the image by its value at beam centre
- Convert to power in (I,Q,U,V)
- Detect and flag bad data
- Form mean over antennas from good data.
- Interpolate over missing frequencies and write output.
- Output used by LINMOS for constructing astronomical images



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# **Detecting bad data - anomalous amplitudes**



# **Detecting bad data - beam shapes, positions**



# The mysterious case of the variable sources

 Time series analysis of LIGO follow-up field by Yuanming Wang (USyd)



### The case of the variable sources

1.04

1.02

1.00

0.98

0.96

20

The apparent flux of individual sources observed though adjacent beams behaved differently.

Perhaps the beams were moving back and forth relative to the sky?



### The case of the variable sources

Indeed, we found that the discrepancies between fluxdensities of sources in adjacent beams could be minimised with a bulk shift of all beams.



## The case of the variable sources

Declination -29:00:0.000



## **The Future**

- Improved telescope control to enable faster measurement and/ or larger or finer sampling grid
- Use of individual antenna patterns (not array-wide mean)
  - -> A-projection
- Larger grid would give better measurement of dish illumination pattern enable A-projection imaging.

#### We acknowledge the Wajarri Yamatji people as the traditional owners of the observatory site.