

# SHOC

*Sparse Hydrodynamic Ocean Code*



**Coastal Ocean Marine Prediction Across Scales**

*V1.0  
(rev 7182)*

*User Manual*



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The latest SHOC User Manual may be downloaded from:

<https://research.csiro.au/cem/software/ems/ems-documentation/>

Revision history is available at the same address.

## 1 Introduction

**SHOC** (Sparse Hydrodynamic Ocean Code - Herzfeld, 2006) and **COMPAS** (Coastal Ocean Model Predication Across Scales) are finite difference and unstructured hydrodynamic models respectively, developed by the Coastal Environmental Modelling team at CSIRO (Commonwealth Scientific and Industrial Research Organization) Oceans and Atmospheres. These models are intended to be general purpose models applicable to scales ranging from estuaries to regional ocean domains. Outputs from the models include three dimensional distributions of velocity, temperature, salinity, density, passive tracers, mixing coefficients and sea level. Inputs required by the model include forcing due to wind, atmospheric pressure gradients, surface heat and water fluxes and open boundary conditions (e.g. tides). **SHOC** and **COMPAS** are based on the three dimensional equations of momentum, continuity and conservation of heat and salt, employing the hydrostatic and Boussinesq assumptions. The equations of motion are discretized on a stencil corresponding to the Arakawa C grid.

**SHOC** uses a sparse coordinate system which maps all cells in the grid into a 1-dimensional vector. This process effectively eliminates all land from the domain representation in computer memory. Arbitrary domain composition can be efficiently performed, allowing **SHOC** to operate in a true distributed processing environment. The sparse representation leads to increases in speed and simplified housekeeping, allowing techniques such as distributed process, 2-way nesting and hybrid physics to be performed with no overhead.

The sparse coordinate system is essentially an unstructured coordinate system for curvilinear grids. It is possible to generalize this system to be suitable for any shaped grid (e.g. triangles, squares, hexagons), which would then make it suitable for finite volume algorithms. In recognition of the superiority of unstructured meshes over orthogonal curvilinear grids in complex coastal environments, **SHOC** has been transitioned into a full finite volume code, **COMPAS**. This essentially results in a new hydrodynamic model, albeit with full backwards compatibility regarding the peripheral infrastructure of the model (core libraries, sediment, BGC, wave libraries, IO, parameter file configuration). The difference between **SHOC** and **COMPAS** lies in treatment of the horizontal dimension. All vertical processes are the same between the models. Similarly both models support similar functionality in terms of open boundaries, advection, diagnostics etc., and the same parameter file is compatible between both models. As such, this manual details usage for both models; where there are differences or functionality is not supported, then this will be clearly stated using '**COMPAS only**', or '**SHOC only**'. Similarly, SHOC and COMPAS can be interchangeable in examples cited in this manual unless explicitly stated, e.g. the following are equivalent for each respective model.

```
shoc -p in.prm or compas -p in.prm
```

**SHOC** uses a curvilinear orthogonal grid in the horizontal. **COMPAS** uses an orthogonal centroidal Voronoi tessellation on arbitrary polygons. Both the unstructured generalisation and replacement of dynamic core algorithms in **COMPAS** follow the MPAS-O (<https://mpas-dev.github.io/>) framework as described by Ringler et al (2010) and Ringler et al. (2013). This framework uses placement of variables on a C grid, and employs the vector invariant approach to solving momentum advection and the Coriolis term. The scheme conserves total energy and potential vorticity, and mass, velocity and potential vorticity evolve in a consistent manner. The framework is grid agnostic, such that the solution is valid for any orthogonal mesh. While the MPAS-O model is a global model suitable for coupling with atmospheric and sea-ice models for investigation of climate impacts, the model proposed here is aimed for use at the coastal or regional sea scale.

Both models use fixed 'z' or  $\sigma$  coordinates in the vertical. The 'z' vertical system allows for wetting and drying of surface cells, useful for modelling regions such as tidal flats where large areas are periodically dry. The models have a free surface and use mode splitting to separate the two dimensional (2D) mode from the three dimensional (3D) mode. This allows fast moving gravity waves to be solved independently from the slower moving internal waves

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allowing the 2D and 3D modes to operate on different time-steps, resulting in a considerable contribution to computational efficiency. The models use explicit time-stepping throughout except for the vertical diffusion scheme which is implicit. The implicit scheme guarantees unconditional stability in regions of high vertical resolution. A Laplacian diffusion scheme is employed in the horizontal on geopotential surfaces. Several turbulence closure schemes can be invoked, including  $k$ - $\epsilon$ ,  $k$ - $\omega$ , Mellor-Yamada 2.5, Mellor-Yamada 2.0 and Csanady type parameterisations. Input and output is handled through netCDF data formatted files, with the option of submitting ascii text files for simple time-series forcing. The netCDF format allows input of spatially and temporally varying forcing and initialization data in a grid and time-step independent manner. Output from **COMPAS** can either be in equivalent **SHOC** formats for structured curvilinear grids (including CF1.0 compliance) or the CF UGRID standard. **SHOC** is capable of performing particle tracking and may be coupled to ecological and sediment transport models.

**SHOC** is written in C and evolved during 2002 from the **MECO** model, with subsequent improvements post 2002. **COMPAS** was developed from 2016 onwards.

This document is designed to assist the user in operating **SHOC** or **COMPAS**. For a description of the theory **SHOC** is based on refer to Herzfeld et al (2002).



## 2 Installation and operation

This section describes how to acquire, compile, and install **SHOC** or **COMPAS**. At present, these models are designed to run under the UNIX operating system. It has successfully been installed on SUN workstations, Silicon Graphics workstations, and Intel Linux which is the current development platform.

### 2.1 Getting the model source code

The source code to SHOC, COMPAS and associated libraries and utilities is available from CSIRO Marine Research, subject to approval and acceptance of a license agreement. If you wish obtain the source code, or require further information please contact [Mike.Herzfeld@csiro.au](mailto:Mike.Herzfeld@csiro.au).

### 2.2 Building and installing the model executable file

This section provides a brief description of how to compile and install **SHOC** or **COMPAS** and the supporting libraries, **ecology**, **sediments** and **tracerstats** as provided with the model source distribution. Additional compilation and installation instructions are provided with each package (see the INSTALL file).

Note that all packages depend on the uunits and netCDF packages. Please ensure that uunits and netCDF have been installed before attempting to compile or install either **SHOC/COMPAS** or the libraries. netCDF and uunits are available from Unidata <http://www.unidata.ucar.edu/>.

**SHOC** and **COMPAS** resides in a directory structure called the Environmental Modelling Suite (EMS), which also contains source code for various supporting libraries and the sediment transport and ecology models. Once EMS is installed on the computer it must be configured. During this step a script checks for the presence of external and internal libraries, searches for compilers, linkers, and other utilities required to compile the source code. If `configure` was successful, it will generate a `makefile` which can be used to build the model and related utilities. The configure script is run as follows:

```
./conf/configure
```

By default the configure script searches for all architecture independent files (e.g. netCDF libraries) in the directory `/usr/local`. If an alternate path is required use:

```
./conf/configure -prefix=PATH
```

For a full list of configure's command line options, enter `configure --help`. Once `ems` is configured, all source code is compiled using:

```
make
```

The libraries and executables are installed using the `make install` command. The directories are cleared of object files and executables by using `make clean` command. Additionally, `make distclean` removes any files created by `configure`, as well as all object files, etc. If `make distclean` is used, it will be necessary to re-run `./conf/configure` in order to re-build the model.

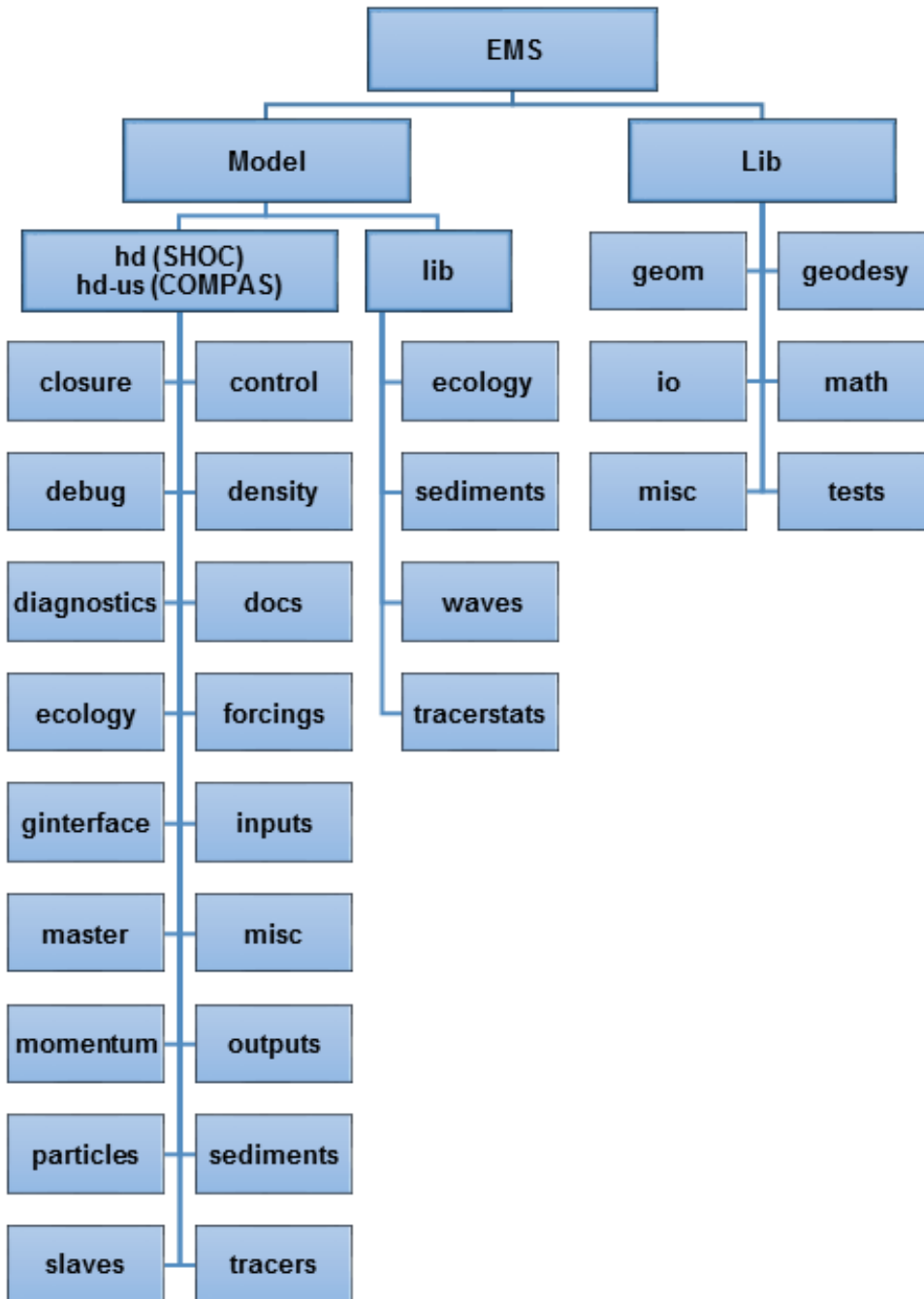
The `ems` packing is stand-alone in the sense that once it is installed the user is free to modify any of the libraries or core code without being dependent on external libraries or code. Individual components of `ems` can be compiled by using the `makefile` in the subdirectories

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of ems (the directory structure of ems is illustrated in Figure 2.1). For example to re-make **SHOC** if it has been modified, go to `/ems/main/model/hd` and type `make`.

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Figure 2.1 : EMS directory structure



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## 2.2.1 Configure flags

Configuration options can be controlled with the following flags:

```
--enable-do-timing
```

Enables timing instrumentation of the various stages of the simulation loop, like `hd_step`, `tracer_step` etc... writes these out to `timing.h`

```
--enable-omp
```

Sets up building with OpenMP. Note that this doesn't automatically change anything and to use OpenMP, the following should be included in the parameter file:

```
DP_MODE OPENMP
```

The semi-Lagrangian transport mode (`-t` option) cannot be used with multiple windows, however, ecology can. Use the following to specify the number of threads to use for ecology:

```
eco_omp_num_threads n # n is an integer
```

```
--enable-da
```

Enables the data assimilation library. This has a dependency on the GNU scientific library; make sure it is installed on your system.

```
--with-metis
```

Enables the METIS window portioning software (see Section 4.2).

Use `--with-metis=$METIS_ROOT`.

```
--enable-swan
```

Enables building with the SWAN library.

## 2.2.2 MPI

A new distributed memory implementation (MPI) based on direct window-window (i.e. slave-slave) transfers has been developed. The code now part of the main Subversion EMS trunk

Configure using;

```
--with-mpi=<mpi_root>
```

The MPI library must be thread enabled and configuration options cannot also use the `--enable-omp` flag.

Execute using `mpirun`. Each window will run in its own SHOC/COMPAS process and run only one window. Therefore it is **important** to make sure the number of `WINDOWS` in the parameter file is the same as the number of processes `mpirun` will spawn.

Exact `mpirun` configuration and run-time performance may be model/HPC system and MPI library dependent. There are various `mpirun` options, e.g. `-np` and `--map-by` options which either lets the job scheduler choose the best distribution of jobs across nodes or you can force it by `core/socket/node`. The latter is useful when more cores are requested than processes needed for a SHOC/COMPAS run and hence OpenMP can be used within nodes/windows. See `slaves/Transfers.cpp` for examples of OMP pragma's that are not

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guarded by `HAVE_OMP`. This allows, for example, the master to collect window data from slaves in parallel. Future versions of SHOC/COMPAS may make more use of this paradigm.

There is one `runlog_X` file per process, where `X` is the window number.

There is one `buffers.txt` file produced that shows the number of bytes that require transfer between windows/master.

Note that the new distributed memory code is still not 100% foolproof in its compilation/building and needs some understanding of the underlying structure of the MPI libraries on each system. Not all features the models will work in distributed mode, e.g. zoomed grids in SHOC, DA and some others. Performance scaling is model dependent.

## 2.3 Running the model

To set-up and run **SHOC/COMPAS**, it is necessary to provide a parameter file containing information about the model geometry, run parameters and forcing inputs. A specially formatted netCDF file is also required that contains the initial values for the model variables over the model grid. The netCDF file may be the result of a previous model run, or may be generated from the parameter file using the `-g` option (see section 8).

The parameter file contains essentially all the information needed to describe a particular model implementation, and its contents are described in detail in the Model setup section.

The model may be run in one of two modes. The auto-configuration mode is invoked via:

```
shoc -a prmname
```

where `prmname` is the name of the model auto-config file (see section 5). These files are vastly simplified versions of the full parameter file. In this mode **SHOC/COMPAS** will internally generate all parameters required for the run, write this information to a parameter file, generate a netCDF input file and commence the run. If the `-ag` option is used then **SHOC/COMPAS** will not commence the run but will terminate once all input files are created and written. In the auto mode model parameters are set to fixed default values or are calculated from the bathymetry and grid geometry.

Alternatively, a run may be initiated using an existing complete parameter file and input netCDF file using:

```
shoc -p prmname
```

where `prmname` is the name of the model parameter file. Model parameters used for the run in this mode are those specified in the parameter file.

Various diagnostic information about the internal status of **SHOC/COMPAS** can be obtained using the `--debug` or `-l` command line option. This option is followed by a sequence of diagnostics types separated by commas e.g. `-debug time,dump`, where each type defines a desired diagnostic output. By default the output is written to the C standard error. Depending on the type requested, the diagnostic output may be quite voluminous. Some diagnostic types depend on the presence of others. **SHOC/COMPAS** will automatically enable any dependent diagnostics.

To display the command line arguments and a list of all diagnostic types **SHOC** should be run with the `-help` option. Following is an example output:

```
% shoc -help
```

```
SHOC: Sparse Hydrodynamic Ocean Code
```

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Version: v1.1 rev()  
Run start: Thu Apr 19 12:51:47 2018

## Usage:

shoc -p prmfile [-restart] [-nrt] <options>

Run SHOC using standard parameter file.

prmfile : Standard parameter file  
[-restart] : Start using 'restart.nc' file  
[-nrt] : Near-real-time operation

shoc -g prmfile dumpfile <options>

Generate initial dump using standard parameter file.

prmfile : Standard parameter file  
dumpfile : Initialisation dump file

shoc -p prmfile -cr <options>

Run SHOC using restarts when model crashes.

prmfile : Standard parameter file

shoc -a prmfile <options>

Run SHOC using autostart parameter file.

prmfile : Autostart parameter file

shoc -ag prmfile <options>

Generate initial dump using autostart parameter file.

prmfile : Autostart parameter file

shoc -t prmfile <options>

Run SHOC in the transport mode.

prmfile : Transport parameter file

shoc -ps

Generate percentile statistics.

shoc -v

Print shoc version information.

## options:

-warnings on|off Enable/disable warning messages (default: on).

-diag\_log <file>|off Enable/disable diagnostic log (default: diag.txt).

-setup\_log <file>|off Enable/disable setup log (default: setup.txt).

-window\_log on|off Enable/disable window log (default: off). A text file listing all master-slave mappings is stored in 'window\_map.txt' and the spatial distribution of all windows in 'window\_geom.txt'.

-l tag,tag... Set library log level. The more tags listed, the more messages are printed. All messages are printed to file 'runlog'. In order of output detail, supported tags are:

- main # print information on major general events
- info # print information on minor general events
- warn # non-fatal warning information
- debug # print high level debug information

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```
- trace          # print low level debug information
- metric        # information on time spent in routines,
                # (for development only).

-debug tag,tag,...  Set debug level. Supported debug tags are:
- all           # print all debug information
- conversions   # list time unit conversions
- time         # list model time
- dump         [ time ] # list next dump
- particles     [ time ] # list particle resets
- init_m       # master initialisation info
- init_w       # slave initialisation info
- ecology      # ecology info
- sediments    # sediment info
```

### Examples :

```
shoc -g input.prm in.nc -debug init_m,init_w
```

```
compas -p input.prm -l main,info,warn -window_log on
```

It is often useful to run the model as a background process with the output captured into a file. How this is done, depends on the UNIX shell being used. For a csh the following command is sufficient:

```
shoc -p prlname >&! logfile &
```

## 3 Model setup

### 3.1 Setting up a model application

There are many steps required to successfully configure **SHOC/COMPAS**. Following are some of the major steps:

- Installation of the model software. This is described in section 2.
- Definition of the horizontal and vertical geometry of the model grid. This may require the use of an interactive grid generation program with the ability to plot coastlines, etc, or may be a simple specification of a test area such as a 'swimming pool'.
- Construction of the model parameter file. This step incorporates the grid geometry obtained above along with information about bathymetry and the location and types of boundary points. As well, forcing data sets are specified, and the physical parameters (mixing, friction, etc) are chosen. With the auto-config mode this file is automatically generated.
- Creation of the model variable initialisation netCDF file, either from the parameter file by using the `-g` option, described in section 8, or by using output from a previous model run.
- Running the model. Commands needed to do this are described in section 4.
- Examination of the results. This is done either by using an interactive viewer (`dive`, `jvismeco`, `olive`), or by producing plots with various scripts or tools such as `gnuplot`.

To set up the model for a particular area or application, it is necessary to gather together a diverse set of parameter specifications and input data. These are all defined in the model parameter file, an easily edited ASCII file which completely defines the model for a particular application and run. Amongst other things, the parameter file describes the model geometry, forcing data, run period and where and how to write results. This section describes the various datasets that are needed to create a model parameter file, and the elements of the parameter file itself.



## 4 The parameter file

The parameter file is an ASCII text file containing comments, keywords and values. Its contents completely describe a particular model implementation and run parameters (apart, possibly, from initial values for model variables). All lines starting with a # character are considered as comment lines. Comment lines are valuable for documenting certain choices of parameter values, or for reminders of the significance of certain infrequently used parameters. Comment lines and blank lines are generally ignored by the model itself, but may not appear in certain positions described below. Other lines typically contain a keyword (the parameter name) and a value. Parameter values may be strings, integers, floating point values, arrays of floating point values or more complex lists (such as boundary point lists, or time series point lists). The order in which parameters appear in the file is largely unimportant.

Examples of string parameters are:

```
PARAMETERHEADER  River model
file0.name       out
```

Examples of boolean parameters (and comment lines) are:

```
# All boolean parameters may be set with either {TRUE|FALSE},
# {YES|NO}, {1|0}, {INCLUDE|EXCLUDE}. Case is not important.
NONLINEAR  TRUE
CALCDENS   no
```

Examples of integer and floating point parameters are:

```
NCE1      20
G          9.81
```

Arrays are entered by giving the keyword and the number of values in the array on the same line, followed on the next lines by the array values separated by spaces, tabs or new lines. Comment lines may not appear in the middle of the list of array values. Following are two examples:

```
# Fills the bathymetry array with four values.
BATHY 4
0.002 0.0025
0.0026
0.0027

# If insufficient data is provided, then the last value
# is used to pad out the array
BATHY 4
0.002
```

Having described the general syntax of the parameters, the following sections describe the wide range of parameters needed to specify a particular model application.

### 4.1 Parameter header

Most parameter files begin with some comment lines which describe the model application, and mandatory parameters which specify the **SHOC/COMPAS** code version to be used, and descriptive string for this run. Most of these model descriptions are reported in model setup files and appear as global attributes in netCDF output files. The format is as shown below:

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```
# This is the parameter file header. It usually describes the
# model application.
#
# The code header must be identical to the 'Version' string
# specified when SHOC or COMPAS is compiled (in version.c). This
# provides a check that the intended version of the model code is
# being used at run time.
CODEHEADER          SHOC default version

# A single line description of the model run. This string is
# written into all output files.
PARAMETERHEADER    NWS 20km rectangular grid, Run 1

# An additional description of the model
DESCRIPTION        Includes realistic forcing

# A name of the model
NAME               MOD1

# A revision code for this run
REVISION           1.0test

# An optional reference describing the model setup
REFERENCE          https://doi.org/10.1000/182

# Technology Readiness Level. This describes the status of
# the model and its associated intended use. These levels are
# derived from
# https://en.wikipedia.org/wiki/Technology\_readiness\_level
# as:
# TR1: Basic principles observed and reported
# TR2: Technology concept formulated.
# TR3: Experimental proof of concept.
# TR4: Technology validated in laboratory environment.
# TR5: Technology validated in relevant environment.
# TR6: Technology demonstrated in relevant environment (pilot
#       model).
# TR7: System prototype demonstration in operational environment
#       (prototype model).
# TR8: System complete and qualified (calibrated model).
# TR9: Actual system proven in operational environment
#       (operational model).
TECHNOLOGY_READINESS_LEVEL  TR6
```

## 4.2 Windows

**SHOC** and **COMPAS** are designed to operate in a distributed processing environment, where domain decomposition is performed on the grid to divide it into a number of partitions or 'windows', which are solved on different processors. The number of windows used is set via:

```
# Indicates the number of windows in the model domain.
WINDOWS      2
```

Generally the number of windows is equal to the number of processors available. If **SHOC** is to operate on a single processor, the `WINDOWS = 1`. The domain decomposition be a striping or blocking method, or may be any arbitrary congregation of grid points. This allows total flexibility when decomposing geographically complex domains. The distributed processing procedure requires common information to be transferred between windows, hence by

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minimising the size of boundaries between windows (e.g. by utilizing the geography and placing window boundaries across narrow regions) the amount of data transferred is minimised and execution speed increases.

The window partitioning method is specified using the `WINDOW_TYPE`, where:

```
WINDOW_TYPE    STRIPE_E1    # Stripe in the e1 direction (default).
WINDOW_TYPE    STRIPE_E2    # Stripe in the e2 direction.
WINDOW_TYPE    BLOCK_E1 n   # Blocking. n is an optional integer;
                           # when present the block is made
                           # rectangular in the e1 direction by n
                           # cells.
WINDOW_TYPE    BLOCK_E2 n   # Same as BLOCK_E1, but rectangles
                           # are in the E2 direction.
WINDOW_TYPE    EXPLICIT     # The user supplies the partitioning,
                           # see below.
```

### COMPAS only:

Since the specification of cells in an unstructured grid containing non-quadrilateral cells is essentially random, and there are no consistent `e1` or `e2` directions, the above partitioning methods are generally unsuccessful using COMPAS and result in overly fragmented windows. To overcome this, COMPAS allows grid partitioning using the METIS software (<http://glaros.dtc.umn.edu/gkhome/metis/metis/overview>).

```
WINDOW_TYPE    METIS
```

This is set up to minimize the *edge-cut*, and uses a multilevel *k*-way partitioning scheme. If `WINDOW_SIZE` is specified in the parameter file then these are passed in as the *target weights*. The `WINDOW_SIZE default` implies equal target weights.

The METIS software must be available on the system being used in order for it to operate, and may be required to be loaded as a module. Additionally, the `configure` command (Section 2.2) must use the additional argument;

```
-with-metis=<root_path_to_metis>.
```

On some HPC clusters, this is available as a module and the `$METIS_ROOT` (or similar) environment variable can be used as the root path, e.g;

```
module load metis
./conf/configure -with-metis=$METIS_ROOT
```

If METIS is unavailable, then to keep the windows as groups of cells, use:

```
WINDOW_TYPE    GROUPED
```

Note that this partitioning method does not always result in contiguous partitions which can cause issues in some cases, particularly for large numbers of windows.

Alternatively, a region file may be supplied, and the windows are partitioned according to the regional polygons contained in the file. It is the users's responsibility to ensure the regions are reasonable, cover the entire domain and will result in load balancing.

```
WINDOW_TYPE    REGION windows.bncc
```

The striping methods divides the wet domain into the number of specified windows, hence all 2D partitions contain the same number of cells (the last window may not if the total number of wet cells is not divisible by the number of windows). The blocking methods divide the total grid size into blocks of size  $\sqrt{n_{e1} \times n_{e2}}$  or  $\sqrt{n_{\text{Mesh2\_face}}}$  for SHOC and

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COMPAS respectively. A block must contain at least 1 wet cell for it to be valid (i.e. blocks that contain all dry cells are ignored). This results in blocks containing quite different numbers of cells, depending on how many wet cells are encountered in each block. Consequently load balance may be poor. However, for large numbers of windows, it may be preferable, since the amount of information exchanged between windows decreases as windows increase with blocking, and the model load balance will be determined by blocks containing all wet cells (which will be more numerous as the number of windows increases).

For STRIPE\_E1, STRIPE\_E2 and GROUPED, The window sizes may be set using the command:

```
# Sets the window sizes for n windows
WINDOW_SIZE      a1 a2 . . . . an
or
WINDOW_SIZE      default
```

Where  $a_1$  to  $a_n$  are fractions whose sum adds up to 1.0, or for default,  $a_1$  to  $a_n = 1 / \text{WINDOWS}$ . The surface of the domain is then partitioned into windows according to the specified fractions, e.g. if two windows are specified with sizes 0.5 and 0.5, then the surface is split into two equal windows. Note that the number of cells in a windows may not be equal if the surface is split into equal sizes, since windows with deeper water will contain more cells than windows with shallow water. When this option is used, the 'diag.txt' diagnostic file (section 4.33) will contain the amount of CPU time spent in each window. Also shown is the actual load balance used (i.e. the prescribed window sizes) and the predicted window sizes that are required to achieve equal amounts of CPU time in each window (i.e. an even load balance). This load balancing may be automated using:

```
# Resets window sizes to balance the CPU
WINDOW_RESET      m
```

Where every  $m$  time steps the windows are automatically re-generated with sizes that attempt to balance the CPU load.

The window partitions may be explicitly defined for  $\text{WINDOWS} - 1$  windows using `WINDOW<n>_POINTS` where  $\langle n \rangle$  is the window number. The number of points in the list should be specified, followed by a list of the (i,j) locations of the window cells, e.g:

```
# Define the first window to contain 2 cells
WINDOW1_POINTS    2
2 1
2 2
```

Note the 'Marked' facility in `jvismeco` is a useful tool for extracting (i,j) locations from a domain. The last window is created to consist of all cells not included in a list.

The window partitioning can be written to the output file using:

```
SHOW_WINDOWS      YES    # Creates a tracer 'window_partitions'
                    # containing window configuration.
```

This facility is switched off by default.

The window map may be written to netCDF file using:

```
DUMP_WIN_MAP      <mapfile.nc>
```

Where `<mapfile.nc>` is the name of the file the map is written to. This may then be subsequently read at runtime (rather than computed) using:

```
READ_WIN_MAP      <mapfile.nc>
```

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Note that computing the sparse map for many windows on very large grids can take several hours; reading the window map from file provides a means of rapidly starting a simulation. DUMP\_WIN\_MAP will operate in the -p and -g modes, and READ\_WIN\_MAP operates in the -p mode.

When using multiple windows, the message passing library must also be specified, e.g.

```
DP_MODE      openmp      # Use the openMP libraries
             pthreads    # Use the pthreads library
```

Comparisons using 1 or multiple windows have shown identical results in simple test domains and a complicated real case study. However, not all functionality (advection schemes, mixing schemes, open boundaries etc) or combinations of bathymetry, geography and window partitions have been tested, hence it is possible that some combinations of the above do not result in identical solutions using 1 and multiple windows. It is known that if the model is subjected to SUB-STEP (Section 4.27) then at window boundaries values from different time levels are used resulting in solutions that differ. To avoid sub-stepping, the time-step should be reduced. When invoking extended functionality with multiple windows it is prudent to check results against a single window.

## 4.3 Time

Internally, the model represents time in seconds since some epoch date/time. These parameters allow the specification of that epoch, the period of the simulation, the ramp-up period for external forcing, and the model's internal (3-d) and external (2-d) time steps for integration.

```
# Defines the epoch for all time related parameters, as well as
# for all output files generated by the model. Currently, the
# units must be 'seconds since ...', but this may change in future
# versions. The epoch is specified in standard ISO date/time
# format, including a possible timezone specification. The
# timezone here is 8 hours ahead of UTC.
TIMEUNIT      seconds since 1990-01-01 00:00:00 +08

# Defines the base time unit that will be used for all
# timeseries and netCDF output files.
OUTPUT_TIMEUNIT  days since 1990-01-01 00:00:00 +08

# Define length units - this parameter is redundant and must
# always be metre!
LENUNIT       metre

# Defines the start and stop time of the model simulation period,
# relative to the epoch defined above. Relative time
# specifications here and elsewhere in the parameter file can be
# specified in seconds, minutes, hours, or days. Here, the start
# time corresponds to 1995-02-10 00:00:00 +8, and the end time to
# 1995-03-13 00:00:00 +8
START_TIME     1866 days
STOP_TIME      1897 days

# Defines the period during which external forcing variables
# (wind, open boundary elevations and/or velocities) are smoothly
# ramped from 0 to their normally prescribed values. This
# mechanism allows the suppression of start-up transients and
# shocks in the simulation.
```

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```
# Prior to RAMPSTART, forcing is set to zero. After RAMPEND,
# forcing is applied normally. In between, forcing values are
# scaled by a raised cosine ramp.
RAMPSTART      1866 days
RAMPEND        1866.5 days

# Defines which variables are ramped in. Suppression of wind and
# boundary forcing (global tide, file or custom specification) are
# invoked by listing the processes subject to the ramp. All
# processes are suppressed by default. E.g. all processes are
# suppressed via;
RAMPVARS WIND      # Ramp the wind
          TIDALH    # Tidal OBC  $\eta$  computed using TIDALH
          TIDALC    # Tidal OBC  $\eta$  using custom constituents
          TIDEBC    # Tidal OBC  $\eta$  using tidal synthesis
          FILEIN    # OBC  $\eta$  using FILEIN input
          CUSTOM    # OBC velocity using CUSTOM
          INV_BARO  # OBC inverse barometer contribution
          ETA_RELAX # Relaxation to eta
          FLUX_ADJUST # OBC local flux adjustment
          STOKES   # Stokes Coriolis and vortex forces

# Specifies the internal (3-d) time-step, and the number of times
# the external (2-d) code will be run per 3-d time-step.
# The external (2_d) time-step is thus DT divided by IRATIO.
DT          120 seconds
IRATIO      5
```

## 4.4 Computational settings and flags

A number of parameters change the way in which calculations are performed, as follows:

```
# A flag which includes or excludes the non-linear terms in
# both the momentum equations and the surface elevation.
NONLINEAR      YES

# A flag which enables the calculation of density at each time
# step from the salinity and temperature of the water. If this
# flag is turned on, then the model must include tracers called
# salt and temp. If it is turned off, the density field used by
# the model is as read from the input netCDF file, and doesn't
# change over time, regardless of the behaviour of any tracers
# in the model. If a valid tracer name is input for CALCDENS,
# then the density used in the model is the distribution
# represented by that tracer.
CALCDENS      YES

or
CALCDENS      density_tracer

# Includes equilibrium tide forcing (COMPAS only); see Sakamoto
# et. al., (2013), doi:10.5194/os-9-1089-2013.
# If tidal potential is turned on, then a diagnostic field
# 'equitide' of the equilibrium tide (m) is written to file.
TIDE_POTENTIAL YES # Include equilibrium tide forcing
EQT_ALPHA     0.948 # Self-attraction / loading constant
EQT_BETA      0.7  # Tidal body force constant

# The minimum layer thickness (m) value to be used when dividing
```

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```
# by the layer thickness in any of the momentum equations.
# This prevents numerical problems, particularly in areas which
# are drying. Usually set to ~7% of the surface layer.
HMIN          0.01

# SHOC only:
# Specification of the slip condition at solid horizontal
# boundaries. This effectively specifies the tangential velocity
# value at the land (or at any solid vertical face) used by the
# horizontal momentum equations. Valid values are:
#   1.0      Full slip condition - most commonly used
#   0.0      Half-slip condition
#  -1.0      No slip condition
# Other values may be accepted by the model, but may give
# unexpected or erroneous results.
SLIP          1.0

# Specification of what constitutes a simulation fatality. If ETA
# is specified the model will exit if absolute sea level is
# greater than ETAMAX. If VEL3D is specified exits occur if
# absolute 3D velocity is greater than VELMAX. If VEL2D is
# specified exits occur if 2D velocity is greater than VELMAX_2D.
# If T/S is present, temp. and salinity are checked for NaN.
# If NAN is present, exits occur if ETA, VEL3D or VEL2D assume
# the NaN value. The default is ETA NAN with ETAMAX = 10.
FATAL        ETA VEL3D VEL2D
ETAMAX       10
VELMAX       5
VELMAX_2D    3

# Specifies the quantity of messages / information written to the
# file 'runlog'. Same as -l option (see Section 2.3). The levels
# supported may be a subset of the following:
log_levels    main,warn,info,debug,trace

- main        # print information on major general events
- info        # print information on minor general events
- warn        # non-fatal warning information
- debug       # print high level debug information
- trace       # print low level debug information
- metric      # information on time spent in routines,
              # (for development only).

# Allows smoothing of various fields at initialisation. Currently
# valid fields are:
CD            # Bottom roughness
U1VH         # Horizontal viscosity in the e1 direction
U2VH         # Horizontal viscosity in the e2 direction
U1KH         # Horizontal diffusivity in the e1 direction
U1KH         # Horizontal diffusivity in the e2 direction
# The form of smoothing is:
SMOOTH_VARS  <name>:n
# where <name> is one of the names above, and n is the number of
# smoothing passes, e.g;
SMOOTH_VARS CD:2 U2VH:1
# will perform 2 smoothing passes on bottom drag, and one pass on
# e2 horizontal viscosity.

# Allows scaling of various fields at initialisation. Valid
# fields are the same as for SMOOTH_VARS. The form of scaling is:
SCALE_VARS   <name>:s
```

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```
# where <name> is one of the names above, and s is a scaling
# fraction, e.g;
SCALE_VARS CD:1.2 U2VH:0.9
# will scale bottom drag by 1.2, and e2 horizontal viscosity by
# 0.9.

# Records a sequence of runs in the file 'setup.txt' and netCDF
# output files. The sequence is invoked via:
SEQUENCE      n
# The following field is then printed in the file setup.txt and
# as a global attribute in all output netCDF file:
Run # n
# If a setup.txt file is entered as the input to SEQUENCE, and
# the file contains 'Run # n', then the run identifier recorded
# in the setup.txt for the current run is:
Run # n+1

# Sets a unique identifier that is tagged in output. <n> is a
# floating point number (e.g. 1.1).
ID_NUMBER     <n>

# Sets a unique text code that is tagged in output. The code
# is a set of floating point numbers separated by '|', and if
# present will be reported in the 'setup.txt' file as a
# hydrodynamic version identifier (first number), sediment
# transport identifier (second number) and biogeochemical
# identifier (last number). See Section 4.33.5.
ID_CODE       2.1|1.0|0.0

# COMPAS only:
# A description of any run re-configuration associated with a
# change to the ID_NUMBER. This may be summarized using the
# HISTORY flag, so that a quick overview of the historical
# model configuration is possible.
NOTES         New bathymetry

# SHOC only: Applies a Shapiro filter to selected tendencies.
FILTERING     ADVECT # 1st order Shapiro filter applied to
                  # momentum advection tendencies.

# Sets the model configuration to be V1562 with previous
# versions of SHOC. Backwards incompatibility may be due to
# bugfixes in the code, or implementation of improved numerics.
# The backwards compatibility is currently defines as:
# SHOC only:
COMPATIBLE    V1246 # Pre v1246: global boundary cells include
                  # R_EDGE and F_EDGE OUTSIDE cells.
              V1283 # Pre v1283: Numerous bugfixes for multiple
                  # windows are not included. Refer to Revision
                  # History Nov 16 2009, v1283-1331.
              V1562 # Pre v1562: swr added explicitly to the water
                  # column.
              V1598 # Pre v1598: wtop uses 2D detadt and low order
                  # approximations. U1 and u2 = 0 above the free
                  # surface for horizontal fluxes.
              V4201 # Run with 32 bit netCDF output (default is
                  # 64 bit).
              V5342 # Turbulence closure quantities vertically
                  # diffused in both closure and vertical
                  # diffusion schemes.

# COMPAS only:
```



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There are currently no compatibility flags for COMPAS.

```
# Exclude certain points in the model domain from wave, tracer
# statistic, sediment transport or biogeochemical computations.
EXCLUDE_PROCESS_POINTS    <n>    # Number of points to exclude
i1 j1 CODE1               # i1 j1 are (i,j) locations of
i2 j2 CODE2               # the cell to exclude.
.                           # CODE is a list of keywords:
.                           # EX_WAVE to exclude waves
i_n j_n CODE_n           # EX_TRST for tracer statistics
                          # EX_SED for sediment transport
                          # EX_BGC for biogeochemistry

EXCLUDE_BGCSED           # EX_SED & EX_BCG using blocks
e.g.
EXCLUDE_BGCSED    3      # Set a series of rectangular regions to
(0,3)-(82,69)      # exclude BGC and sediments.
(184,3)-(248,69)
248 131

SHOC only:
MOM_CONVERT    momgrid          # Convert the input file to a
                                # MOM4 compatible grid_spec.nc
                                # Output file is momgrid_spec.nc.

ROMS_CONVERT    romsgrid        # Convert the input file to a
                                # ROMS compatible file. Output
                                # file is romsgrid_roms.nc.
```

## 4.5 Physical constants

Values must be provided for a number of physical constants. Most are rarely changed far from the values shown below. An exception is the Coriolis parameter, which is latitude dependent.

```
# Acceleration due to gravity (m s-2)
G          9.81

# Air density - note that it might be better to calculate this
# internally in the model code, based on the air temperature.
# For the moment, however, it is specified in the parameter file
# as a constant value (kg m-3).
AIRDENS    1.225

# Specific heat of water. Again, the model could calculate this
# based on salinity, temperature, etc. For now, however, this
# is specified as a constant (J C-1 kg-1) - FIX - CHECK THIS
SPECHEAT   3990

# The Coriolis parameter value for the area of interest.
# This is an NCE1*NCE2 floating point array, so that it is
# possible to set a different value in every grid cell. However,
# for most applications where the grid geographical extent is not
# large, a uniform value can be used, as shown here, for a
# hypothetical 40*50.
# The CORIOLIS parameter will be automatically computed if not
```

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```
# supplied, but the PROJECTION parameter is.  
CORIOLIS          2000  
-0.000019
```

## 4.6 Horizontal coordinate system

**SHOC** uses a sparse, or compressed, array configuration (Herzfeld, 2006) which represents a three dimensional region as a one dimensional vector in computer memory. One of the advantages of this approach is that all non-wet land cells may be omitted from the grid in memory. This means that when constructing a grid there is no computational penalty when large amounts of land are included in the grid. This approach requires, however, that **at least one land cell must be adjacent to wet cells at coastal boundaries** (i.e. a solid boundary is not allowed to be adjacent to a cell containing water; land cells only must be adjacent to wet cells).

**COMPAS** uses a generalized version of SHOC's coordinate system, where a mesh is defined within the interior of a supplied coastline, and there is no requirement for land to be specified.

A unique feature of **SHOC/COMPAS** is not only its ability to support a myriad of different horizontal grid geometries, but also its ability to handle different coordinate systems. Currently **SHOC** supports three coordinate systems:

- Arbitrary Cartesian
- Geographic - Latitude/Longitude
- Geographic - Map projected

The Cartesian system defines the coordinates on a rectangular plane with no physical association to real locations on the Earth. The geographic based coordinate systems however, map directly to real-world locations. For a Latitude/Longitude coordinate system all grid metrics are computed on the spheroid, while for the map projected coordinate system the metrics are computed on the projected plane.

The coordinate system is defined using the `PROJECTION` parameter and applies to ALL windows.

### 4.6.1 *Defining a Cartesian coordinate system*

An arbitrary Cartesian coordinate system can be specified by either leaving the `PROJECTION` blank, or by not specifying the parameter at all. Please note, it is assumed that the XY units are in metres, even though they have no real-world significance.

### 4.6.2 *Defining a latitude/longitude coordinate system*

The Latitude/Longitude coordinate system is specified as follows:

```
# The 'geographic' projections implies that all coordinates  
# should be provided as decimal longitude and latitude.  
PROJECTION geographic
```

Unfortunately at this time no mechanism is provided to specify the ellipsoid parameters, instead it is hard-coded as a sphere with a radius of 6370997.0m. It is hoped this restriction will be relaxed in a later version of **SHOC**.

### 4.6.3 *Defining a map projected coordinate system*

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Of the three coordinate systems supported, defining the map projection is by far the most complicated, with a variety of map projections each with their own arguments.

The basic syntax is as follows:

```
PROJECTION proj=<projection-name> [<proj-param0>=<arg> [...]]
```

## *Standard projections*

**SHOC/COMPAS** support six standard projections. A description of each projection and their arguments are described below:

### **Transverse Mercator (Transverse Central Cylindrical)**

The Transverse Mercator is a conformal cylindrical projection where the cylinder is rotated horizontally (transverse) across the ellipsoid.
---

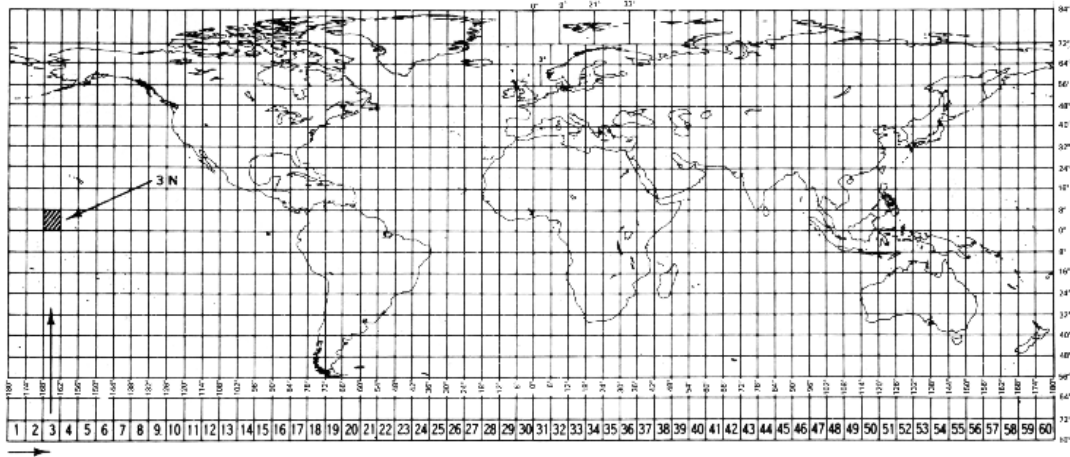
<b>proj=tcc lon_0=&lt;long&gt; k_0=&lt;number&gt;</b>
---

<b>lon_0</b>	Central meridian.
<b>k_0</b>	Scale factor.

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## Universal Transverse Mercator (UTM)

The Universal Transverse Mercator (UTM) projection is based on the Transverse Mercator projection described above. However, the scale factor is fixed to 0.9996, and the central meridian is parameterised by zone. Each zone defines a 6 degree window in longitude around the Earth, making a total of 60 zones. Zone 1 is located at a 180W, with the zone number increasing in an easterly direction.



The default ellipsoid is clark66, and false eastings and northings are (500000E, 1000000N) for the southern hemisphere and (500000E, 0N) for the northern hemisphere.

Defined by	<b>proj=utm zone=&lt;number&gt; [south north]</b>	
	<b>zone</b>	UTM zone (1-60).
	<b>south</b>	Enabled if for southern hemisphere.
	<b>north</b>	Enabled if for northern hemisphere (default).

## Australian Map Grid

A projection for the Australian region, based on the UTM projection, but using the gda66 ellipsoid.

Defined by	<b>proj=amg zone=&lt;number&gt;</b>	
	<b>zone</b>	UTM zone (1-60).

## Map Grid of Australia

A more recent projection for the Australian region, based on the UTM projection, but using the gda94 ellipsoid. This is the current Australian Standard Projection.

Defined by	<b>proj=mga zone=&lt;number&gt;</b>	
	<b>zone</b>	UTM zone (1-60).

## Lambert Conformal Conic

A conformal, conic projection, where parallels are unequally spaced arcs of concentric circles. Meridians are equally spaced radii of the same circles. The scale is true along two standard parallels.

The default ellipsoid is wgs84, and false eastings and northings are (0E, 0N).

Defined by	<b>proj=lcc lon_0=&lt; long&gt; lat_0=&lt;lat&gt; lat_1=&lt;lat&gt; [lat_2=&lt;lat&gt;]</b>		
	<b>lon_0</b>	Central meridian.	
	<b>lat_0</b>	Central latitude.	
	<b>lat_1</b>	First standard parallel latitude.	
	<b>lat_2</b>	Second standard parallel latitude.	

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## Mercator

The Mercator map projection is a cylindrical and conformal map projection, where the cylinder is aligned north/south. It has the properties that all meridians are equally spaced straight lines, parallels are unequally spaced (closer at the equator), and Rhumb lines are down as strait lines.

The default ellipsoid is wgs84, and false eastings and northings are (0E, 0N).

Defined by	<code>proj=merc lon_0=&lt;long&gt;</code>
	<code>lon_0</code>   Central meridian.

## Other projections

**SHOC/COMPAS** also supports a number of other projections if compiled and linked with the USGS PROJ 4 projection library. The list of projections supported by PROJ 4 are described below. For a full description of each projection and their arguments please consult the PROJ 4 manual (Evenden, 1995).

Projection	Description
aea	Albers Equal Area
aeqd	Azimuthal equidistant
alsk	Alaska Mod. Stereographic
apian	Apian Globular
bipc	Bipolar Conic
bonne	Bonne
cass	Cassini
cc	Central Cylindrical
cea	Cylindrical Equal Area
collg	Collignon
eck1	Eckert I
eck2	Eckert II
eck3	Eckert III
eck4	Eckert IV
eck5	Eckert V
eck6	Eckert VI
eqc	Equidistant Cylindrical
eqdc	Equidistant Conic
gall	Gall (Stereographic)
gnom	Gnomonic
gs50	50 State U.S. Mod. Stereographic
gs48	48 State U.S. Mod. Stereographic
hataea	Hatano Asymmetrical Equal Area
labrd	Laborde
laea	Lambert Azimuthal Equal Area
leac	Lambert Equal Area Conic
Projection	Description
lee_os	Lee Oblate Stereographics Pacific
loxim	Loximuthal
lsat	LANDSAT Space Oblique Mercator
mbtfpp	McBryde Thomas Flat Polar Parabolic
mbtfps	McBryde Thomas Flat Polar Sinusoidal
mbtfpq	McBryde Thomas Flat Polar Quartic
mill	Miller
mill_os	Miller Oblate Stereographics Euro-Africa
moll	Mollweides
nicol	Nicolosi Globular
nsper	General Vertical Persepective
nzmng	New Zealand Map Grid
oceq	Oblique Cylindrical Equal Area

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omerc	Oblique Mercator
ortho	Orthographic
parab	Caster Parabolic
poly	Polyconic (American)
putp2	Putnins P2'
putp5	Putnins P5
quau	Quartic Authalic
robin	Robinson
sinu	Sinusoidal
stere	Stereographic
tcea	Transverse Cylindrical Equal Area
tpers	Tilted perspective
ups	Universal Polar Stereographic
vandg	Van der Grinten
wink1	Winkel I

### Global parameters

In addition to the projection specific parameters, there are also a number of parameters supported by all projections.

Parameter	Description
ellps	Ellipsoid name (see Ellipsoid table below).
es	Eccentricity.
a	Major ellipsoid axis radius.
b	Minor ellipsoid axis radius.
rf	Reverse flattening.
x_0	False easting (automatically specified for the UTM projection).
y_0	False northing.

### Ellipsoids

Supported ellipsoid include:

Ellipsoid	Parameters	Description
merit	a=6378137.0 rf=298.257	MERIT 1983.
grs80	a=6378137.0 rf=298.257222	GRS 1980 (IUGG, 1980).
iau76	a=6378140.0 rf=298.257	IAU 1976.
airy	a=6377563.396 b=6356256.910	Airy 1830.
mod_airy	a=6377340.189 b=6356036.143	Modified Airy.
aust_ntl	a=6378160.0 rf=298.25	Australian Natl, S. Amer., IAU 64.
grs67	a=6378160.0 rf=247.247167	GRS 67 (IUGG 1967).
bessel	a=6377397.155 rf=299.1528128	Bessel 1841.
bess_nam	a=6377483.865 rf=299.1528128	Bessel 1841 (Namibia).
clrk66	a=6378206.4 b=6356583.8	Clarke 1866.
clark66	a=6378206.4 b=6356583.8	Clarke 1866.
clrk80	a=6378249.145 rf=293.4663	Clarke 1880 mod.
everest	a=6377276.3452 b=6356075.4133	Everest 1830.
hough	a=6378270.0 b=6356794.343479	Hough.
intl	a=6378388.0 rf=297.	International 1909 (Hayford).
krass	a=6378245.0 rf=298.3	Krassovsky, 1942.
mercury	a=6378166.0 b=6356784.283666	Mercury 1960.
mod_ever	a=6377304.063 b=6356103.039	Modified Everest.
mod_merc	a=6378150.0 b=6356768.337303	Modified Merc 1968.
new_intl	a=6378157.5 b=6356772.2	New International 1967.
Seasia	a=6378155.0 b=6356773.3205	Southeast Asia.
walbeck	a=6376896.0 b=6355834.8467	Walbeck.
wgs66	a=6378145.0 b=6356759.769356	WGS 66.
wgs72	a=6378135.0 b=6356750.519915	WGS 72.
wgs84	a=6378137.0 rf=298.257223563	WGS 84.

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Ellipsoid	Parameters	Description
agd66	a=6378160.0 rf=298.25	Same as aust_ntl.
agd84	a=6378160.0 rf=298.25	Same as aust_ntl.
gda94	a=6378137.0 rf=298.25722101	New Aust. ellip.
sphere	a=6370997.0 es=0.0	Sphere of 6370997 m.

An example definition of an AMG projection for Port Phillip Bay in Eastern Australia follows:

```
# Port Phillip Bay is located at Zone 55 of the UTM projection
PROJECTION proj=amg zone=55
```

Note that all modelling is commonly performed in a Geographic - Latitude/Longitude coordinate system.

## 4.7 Horizontal grid geometry

**SHOC/COMPAS** support five orthogonal horizontal grid geometries - *rectangular*, *polar*, *geographic\_rectangular*, *elliptic* and *numerical*. All internal grid metrics are stored in units of metres, although the coordinates maybe specified in either x/y or latitude/longitude units depending on how the `PROJECTION` parameter was specified. Note that if these grids are used in COMPAS, then quadrilateral meshes result.

All grid definitions share the following two parameters; `NCE1` and `NCE2`. `NEC1` and `NEC2` define the number of cells in the `e1` (or `i` or `x`) and `e2` (`j` or `y`) directions respectively.

### 4.7.1 Rectangular grid

Following is an example file fragment that describes all of the parameters required to define a rectangular grid:

```
# Type of grid
GRIDTYPE          RECTANGULAR

# Number of grid cells in the e1 (i) and e2 (j) directions
NCE1              57
NCE2              72

# Real-world coordinates of the lower left hand corner of
# the lower left-hand grid cell (i=0, j=0)
X00               257300
Y00               5770180

# Grid cell size in e1 (i) and e2 (j) directions
DX                1000
DY                1000

# Angle (in degrees) between e1 (i) direction and the real-world
# X axis (which is East in most reasonable projections).
# This represents a mathematical rotation, so that the value of
# 315 degrees would probably make the grid i axis run in a
# south-easterly direction.
ROTATION          315
```

The rectangular grid is defined as being 57 by 72 cells, with a 1000m resolution along both axes, rotated at 315 degrees, and an origin (the bottom left corner of cell (`i = 0`, `j = 0`)) at Easting 257300, Northing 5770180. If no `PROJECTION` parameter is specified, then it should the grid should only be used to model 'local' areas where the Earth's curvature is not

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considered significant. This also true if a map projection is specified, but it's appropriateness depend on the region and projection.

### 4.7.2 Polar grid

Polar grids are specified is a similar way to rectangular grids, as shown below:

```
# Type of grid
GRIDTYPE POLAR

# Number of cells in the e1, i, or azimuthal direction.
NCE1 5

# Number of cells in the e2, j, or radial direction.
NCE2 10

# Coordinates of polar origin
X00 250000
Y00 5770000

# Radial distance from origin to edge of first grid cell
# (metres).
R0 40

# Angle (in degrees) between e1=0 radial (i=0) direction and the
# real-world X axis (which is East in most reasonable
# projections).
# This represents a mathematical rotation (+ve anticlockwise).
ROTATION 20

# Angular extent of grid (degrees), running clockwise from the
# e1=0 (i=0) radial.
ARC 120
```

The above describes a polar grid with 5 by 10 cells, with a minimum radius of 40m and covering an angular range of 120°, from 110° to 230° with respect to true north. The grid polar origin is located at Easting 250000, Northing 5770000. The polar grids generated for the model have 'square' cells, in the sense that the size of any given cell is approximately equal in the azimuthal and radial directions. A brief analysis shows that this causes the cell size to increase exponentially in the radial direction (as j increases), so that the grid has higher resolution near the origin, and lower resolution further away. The origin itself cannot be part of the grid (ie, R0 must be greater than zero), as the grid becomes singular at that point.

Like the rectangular grid, Polar grids are generally suitable for 'local' areas only, unless a Latitude/Longitude PROJECTION is used.

### 4.7.3 Numerical grid

The numeric grid allows the specification of a general orthogonal curvilinear grid using the XCOORDS and YCOORDS parameters. The grid must include not only the cell corners, but also the position of the cell centre and the u1 and u2 positions. In effect the parameters define a grid twice the resolution of that being modelled. At this time there is no simple toolkit available for generating such grids, and grid generation is left to the reader.



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## 4.7.4 Geographic rectangular grid

A Geographic rectangular differs from a normal rectangular grid, as it defines a grid that is orthogonal on a spheroid. A geographic rectangular grid can only be specified if the PROJECTION parameter is set to 'geographic'.

**SHOC/COMPAS** supports three different ways of defining a geographic rectangular grid.

### *Auxiliary pole*

The first method computes the grid metrics using an auxiliary coordinate system, defined by a false pole.

```
PROJECTION geographic
GRIDTYPE GEOGRAPHIC_RECTANGULAR
NCE1 10
NCE2 20
DLAMBDA 0.01 # Long. cell interval in aux. coords.
# (degrees)
DPHI 0.01 # Lat. cell interval in aux. coords.
# (degrees)
X00 144.3856 # Longitude of origin (degrees)
Y00 -38.2030 # Latitude of origin (degrees)
POLE_LONGITUDE 0 # Longitude of false pole (degrees).
POLE_LATITUDE 90 # Latitude of false pole (degrees).
```

### *Equally spaced grid in degrees*

This is almost identical to the auxiliary pole definition, except that a rotation is used, instead on a false pole. The resulting cells are unequally spaced on the sphere, but equally spaced in degree space.

```
PROJECTION geographic
GRIDTYPE GEOGRAPHIC_RECTANGULAR
NCE1 10
NCE2 20
DLAMBDA 0.01 # Long. cell interval in aux. coords.
# (degrees)
DPHI 0.01 # Lat. cell interval in aux. coords.
# (degrees)
X00 144.3856 # Longitude of origin (degrees)
Y00 -38.2030 # Latitude of origin (degrees)
ROTATION 315 # Grid orientation.
```

### *Equally spaced grid over sphere*

The third method requires that the grid cells preserve their distances over the sphere. The lat/long's of the grid are computed by projecting the interval (or multiple there of) along given a direction. This method does not always produce perfectly orthogonal grids, but the error is minimal.

```
PROJECTION geographic
GRIDTYPE GEOGRAPHIC_RECTANGULAR
NCE1 10
NCE2 20
DX 1000 # 1000m along i axis.
DY 1000 # 1000m along j axis.
ROTATION 315 # Grid orientation (degrees).
# This rotation is on the sphere.
X00 144.3856 # Longitude of origin (degrees)
Y00 -38.2030 # Latitude of origin (degrees)
FALSE_POLE YES # Optional; if YES then a grid is constructed
# using a false pole where the equator lies
```

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# through the grid's middle.

## 4.7.5 COMPAS meshes

A mesh in COMPAS is defined by specifying a list of groups that define a cell. This consists of a list of indexed coordinates (**mesh indices**,  $I_i$ ) defining the geographic location of every cell centre and vertex in the mesh, e.g.

```
Coordinates
I1    lon1  lat1
I2    lon2  lat2
.
.
Im    lonm  latm
```

The groups defining a cell (**cell indices**) then reference the mesh indices,  $I_i$ , and take the form (e.g. for the  $n^{\text{th}}$  cell):

```
Indices
Celln NPEn  Centren
V1    I1,1  I1,2
V2    I2,1  I2,2
.
.
VNPE  INPE,1 INPE,2
```

Where:

Cell<sub>n</sub> is the cell index representing the  $n^{\text{th}}$  cell,  
NPE<sub>n</sub> the number of edges this cell contains,  
Centre<sub>n</sub> the mesh index corresponding to the cell centre  
V<sub>n</sub> an index for the  $n^{\text{th}}$  edge  
I<sub>n,1</sub> the mesh index of the start coordinate for the edge  
I<sub>n,2</sub> the mesh index of the end coordinate for the edge

An example for the third hexagonal cell in a mesh may be:

```
3      6      8687
1      1400   1358
2      1358   1338
3      1338   1340
4      1340   5250
5      5250   4684
6      4684   1400
```

The full mesh is then defined by a list of these cell groups. The information in the parameter file defining the full mesh is specified as:

```
GRIDTYPE          UNSTRUCTURED    # grid type
nMaxMesh2_face_nodes 8             # Maximum number of edges that
                                     # cells in the mesh contain.
nMesh2_face_indices 10131          # Number of Coordinates
nMesh2_face        3353           # Number of Indices (cells)
```

The definition of these cells groups to make a viable compass mesh is non-trivial, and is usually generated by dedicated software. COMPAS uses the JIGSAW software (<https://github.com/dengwirda/jigsaw>) written by Darren Engwirda as its primary meshing tool, and can ingest JIGSAW output files directly to create a mesh, e.g.:

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```
JIGSAW_FILE      <mesh_out.msh>
```

JIGSAW can be run offline to create a mesh, and its output used directly with the JIGSAW\_FILE keyword. The file <mesh\_out.msh> has its own format which is a little similar to the COMPAS mesh specification, but not identical. The format of the .msh file is described at <https://sites.google.com/site/dengwirda/jigsaw/jigsaw-documentation/msh-file-format>.

JIGSAW is included in the EMS package as a library function that can be called inline to create a mesh. This involves specifying a closed coastline loop which bounds the mesh. Creating this closed loop is generally not straightforward in real applications, and is assisted in COMPAS with dedicated software, COASTMESH, installed as an EMS library (see Section 14 for details of COASTMESH usage). The entry keyword for a COASTMESH mesh specification is the provision of a weighting function file:

```
HFUN_BATHY_FILE  <bathy.nc>
```

Once COASTMESH parameters have been specified as per Section 14, then JIGSAW is called inline to create the mesh. JIGSAW has its own parameter specification (e.g. see <https://sites.google.com/site/dengwirda/jigsaw/jigsaw-documentation/jig-file-format> for details), however JIGSAW is invoked from COASTMESH using default settings. Additionally, power meshes (triange centres are computed using a weighted circumcentre) can be invoked within JIGSAW using:

```
POWER_MESH      YES
```

The mesh may be computed on the sphere (as opposed to a plane), including triange centre computation, by specifying:

```
STEREOGRAPHIC_MESH  YES
```

The default JIGSAW parameterisation does not invoke these options. A standard circular mesh can be created using JIGSAW where maximum resolution is placed at the mesh centre and minimum around the mesh edges. This is achieved using:

```
HEX_RADIUS      100000      # Radius of the mesh in m
X00              151.0      # Longitude of mesh centre
Y00              -35.0      # Latitude of mesh centre
DX_MIN          1200        # Minimum grid size (m)
DX_MAX          10000       # Maximum grid size (m)
HEX_GSCALE      0.3         # Controls the transition of
                          # resolution. Default is 0.25.
```

Regular triangular or hexagonal meshes can be created using the geographic rectangular grid specification (Section 4.7.4) above, except the grid sizes DX, DY, DLAMBDA or DPHI are replaced with:

```
TRI_DX          x          # Triagonal edge length for tri-meshes
HEX_DX          x          # Hexagonal edge length for hex-meshes
```

Here x is the resolution in metres for rectangular meshes, and in degrees for geographic rectangular meshes.

Lastly, structured quadrilateral meshes can be converted to regular triangular or hexagonal meshes using:

```
CONVERSION      TRI      # Convert to triangular mesh
CONVERSION      HEX      # Convert to hexagonal mesh
```

The mesh conversion is achieved by creating triangles using the grid locations as a base, and the u2 velocity location as the apex (see Fig. 4.1).

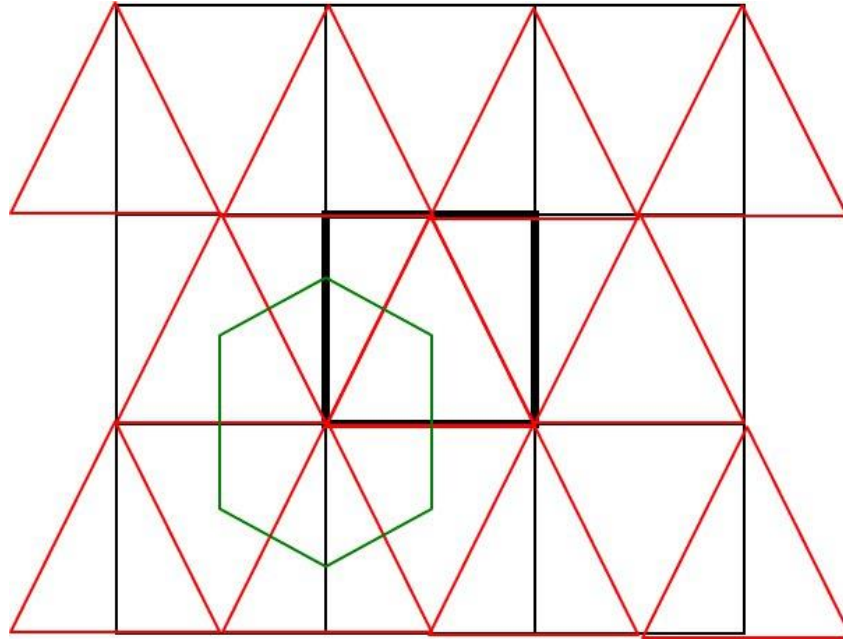


Figure 4.1. Construction of unstructured mesh from a curvilinear grid. Black lines are the structures orthogonal curvilinear grid. Red lines are the Delaunay triangulation generated from the curvilinear grid. Green lines are the hexagonal mesh.

The COMPAS mesh is defined as a series of independent cell specifications, and it is relatively simple to create a new set of cells representing an orthogonal curvilinear grid and 'patch' these into the mesh by referencing one edge to a common set of coordinates. This is useful for adding 2-dimensional orthogonal curvilinear channels into the mesh representing a river or narrow channel. These grids are included when a mesh is generated using the '-g' option. Note: if the mesh is already defined in the parameter file (i.e. `Coordinates` and `Indices` are listed in the parameter file) then the grids to be added are processed, with centre and edges written to the files `quad_c.xy` and `quad_e.xy` respectively, but is NOT included in the mesh. The format of grid addition is:

```
ADD_QUAD          n      # Number of grids to patch
QUAD0 grid0.auto  # Grid specification 1
.
.
QUADn gridn.auto  # Grid specification n
```

Alternatively the grids can be listed consecutively after `ADD_QUAD`. These grids must be a basic curvilinear grid specification used in SHOC containing:

```
NCE1      nx      # x dimension of grid
NCE2      ny      # y dimension of grid

XCOORDS   nc      # List of (2*NCE1+1)*(2*NCE2+1) x coordinates
xcl
.
Xcn

YCOORDS   nc      # List of (2*NCE1+1)*(2*NCE2+1) y coordinates
ycl
.
ycn
BATHYVAL  2.0     # Bathymetry value for the grid
```

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```
# Common set of coordinates to merge the curvilinear grid with
# the unstructured mesh.
MERGE_LOC (x1 y1)-(x2 y2)

# A second set of common coordinates to merge the curvilinear
# grid with the unstructured mesh, e.g. for joining two end of
# a channel.
MERGE_LOC2 (x1 y1)-(x2 y2)

# If MERGE_DIR = YES then the orthogonal grid coordinates are
# ordered with values increasing sequentially across the
# channel. If MERGE_DIR = NO then the coordinates are ordered
# such that values sequentially increase along the channel.
# The user must discern which is the case and set MERGE_DIR
# accordingly.
MERGE_DIR YES or NO

# Optional polygon where any mesh cells inside the polygon
# are removed from the mesh prior to patching in the grid.
# Useful for isolating the mesh edge to use as the common
# coordinates.
REMOVE poly.xy
```

This process is iterative; an un-merged mesh should be generated first in order to find the MERGE\_LOC locations, then the mesh should be re-generated using the above specifications. If the MERGE\_LOC locations do not align well with the start and end of the curvilinear channel, then imperfect mesh cells can result. The MERGE\_LOC locations do not need to be exact (a distance minimization routine is used to find the nearest mesh vertices), but they should be closer to the desired mesh vertices than any other vertices in the mesh.

### 4.7.6 Indexing

As seen above, the indexing for structured (SHOC or COMPAS quad) grids differs from that of unstructured meshes. The former uses a Cartesian (i,j) indexing where  $1 \leq i \leq n_{ce1}$  and  $1 \leq j \leq n_{ce2}$ , while the latter uses the cell indices where  $1 \leq c \leq n_{Mesh2\_face}$ . A list or range of indices for structured grids is provided, for example, as:

```
1 2          # List of (i,j) points for structured grids
2 1

(1,1)-(2,1)  # Range for structured points

12          # List of cell indices for unstructured meshes
20
62

(12)-(20)   # Range for unstructured meshes
```

These conventions should be used when prescribing index lists for various functions in SHOC/COMPAS (e.g. see BATHY\_MASK below).

### 4.7.7 Grid import

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Grids from the ROMS or MOM4 modelling packages may be imported into SHOC:

```
ROMS_GRID    roms_grid.nc      # Import ROMS grid
MOM_GRID     grid_spec.nc      # MOM4 grid spec import
```

## 4.8 Vertical grid geometry

**SHOC/COMPAS** are 'z' or  $\sigma$  coordinate models. In the z coordinate system each layer height is the same across the whole grid domain. The layers are specified by giving the z-coordinate of their interfaces, relative to mean sea level. Because the model z-coordinate is positive up, with origin at mean sea level, this means that layer interface z-coordinates are usually negative (below the surface). For example, a model with 5 layers in the vertical, extending from 10m depth to the surface, and with uniform 2m vertical resolution, would be specified as follows:

```
# The z coordinates of the model layer interfaces.
LAYERFACES 6
-10.0
-8.0
-6.0
-4.0
-2.0
0.0
```

Layers need not all have the same thickness, but, for numerical reasons, care should be taken to avoid sudden large changes in layer thickness. The top layer need not be at mean sea-level. An example covering these points is shown below:

```
# A non-uniform vertical grid with 10 layers, covering from
# 15m depth to 5m above mean sea-level.
LAYERFACES 11
-15.0
-10.0
-6.0
-3.0
-1.0
0.0
1.0
2.0
3.0
4.0
5.0
```

The model includes drying and wetting algorithms, and the simulated water surface in the model is free to move up and down through the layers. The uppermost layer automatically grows thicker as required, to incorporate increases in surface elevation, up to some maximum height, specified as follows:

```
# Maximum allowable z-coordinate for water surface elevation.
# If the water surface ever exceeds this value, the model
# run stops and produces an error message.
#
# This value is also used by the grid generation program
# to decide whether the top layer is land or not (land if
# bathymetry above ETAMAX)
ETAMAX          10.0
```

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The  $\sigma$  coordinate system scales the layer interfaces to the total water depth. This allows the bottom to be well resolved at any depth. If the sigma option is invoked (see section 4.26) then the  $\sigma$  levels are generated by **SHOC/COMPAS** such that a logarithmic distribution exists at the surface and bottom and a linear distribution in the interior. The user need only specify the number of layers to be used in this case.

```
# The number of  $\sigma$  coordinates for the model layer interfaces.  
LAYERFACES 6
```

**NOTE:** The vertical grid geometry described above is not used by the model when a run is initiated using the `-p` option. Layers are defined when the `-g` option is invoked (see section 8) to generate the model input netCDF file, which contains model initial values and geometric information. Any alteration to model vertical grid geometry must be accompanied by the creation of a new model input netCDF file, using the `-g` option.

## 4.9 Bathymetry

When a run is initiated using an existing parameter file and input netCDF file (i.e. using the `-p` option) the bathymetry used is read from the netCDF input file. Any bathymetry data, and bathymetry manipulation options (e.g. bathymetry limits, smoothing etc.) present in the parameter file are ignored. This is because data for all the model variables read from the netCDF file is assumed to correspond to a particular layer configuration over a particular depth range, and changing the layer structure or bathymetry range will result in discrepancies between the data read from file and the assumed model geometry.

Using the `-a` or `-g` option (see section 5 and 8) the bathymetry of the area to be modelled is specified by providing a depth value for each horizontal grid cell. Thus, there are  $NCE1 * NCE2$  bathymetry values for SHOC or `nMesh2_face` values for COMPAS. They are specified as an array parameter, as follows.

```
# Example depth values for a 3 by 4 grid  
BATHY 12  
22.2  
12.3  
7.4  
23.5  
12.0  
6.0  
25.8  
13.7  
5.8  
27.6  
14.2  
4.9
```

**SHOC only:** the values run in order from the bottom left corner of the grid ( $i=0, j=0$ ), with  $i$  varying fastest. This means that for a single column bathymetry list (as in the above example) any cell  $(i,j)$  is located at position  $j * NCE1 + i + 1$  in the list.

**COMPAS only:** the values run in order of the cell groups (see Section 4.7.5).

Note that the values are depths, rather than z-coordinate values, and hence are usually positive. **Beware, as this can easily cause confusion.** Negative values are also allowed, and signify that the sea-bed is above mean sea-level. Where the sea-bed is above `ETAMAX` (see above), the cell is taken to be a land cell. Values which are deeper than the deepest model layer (see section 4.8) signify that the corresponding grid cell is outside the domain of computation of the model (denoted `OUTSIDE` cells). This mechanism allows open boundaries to be located at arbitrary positions within the grid.

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Here is the above example again, but this time the right hand column of the model is land, and the top left cell is outside the computational domain:

```
# Example depth values for a 3 by 4 grid
BATHY 12
22.2
12.3
-99
23.5
12.0
-99
25.8
13.7
-99
9999
14.2
-99
```

A file containing the bathymetry may be supplied, where the format of the bathymetry conforms to the above:

```
BATHYTEXTFILE      bathy.txt
```

A database bathymetry may be supplied to interpolate the bathymetry from:

```
BATHYFILE          bathy.bth
```

This file is a asci text file containing a list of netCDF bathymetry tile files, and has the following (example) format:

```
# bathy tile file
VERSION nctiled
BASEDIR /home/a2002_tiled/      # Base directory of tile files
NROWS 2                          # Number of files in each row
NCOLS 3                          # Number of columns
COL1 dbdb2_1_1.nc dbdb2_1_3.nc
COL2 dbdb2_2_1.nc dbdb2_2_3.nc
COL3 dbdb2_3_1.nc agso2002_1_1.nc
```

Each netCDF bathymetry file must contain the bathymetry value (< 0) on a latitude / longitude grid.

**COMPAS only:** a netCDF file may be supplied for BATHYFILE in preference to the bathymetry database. The supplied netCDF bathymetry file must be a gridded (structured) file, and bathymetry is interpolated onto the grid using bi-linear interpolation by default. Alternative interpolations may be performed using:

```
BATHY_INTERP_RULE nearest      # Nearest neighbour
                        linear   # Linear interpolation on a
                                # triangulation.
                        cubic    # Cubic interpolation.
                        nn_sibson # Sibsonian natural neighbours.
                        nn_non_sibson # Natural neighbours.
```

Multiple gridded files may be specified for COMPAS; all but the last are successively interpolated onto the mesh with bi-linear interpolation where data is coincident, and if a BATHY\_INTERP\_RULE is specified, the last file is interpolated onto remaining mesh points using that rule. Alternatively a BATHY\_INTERP\_RULE can be specified for each file.

If these interpolations are specified, the input file may also be an asci .bty file, with format:



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longitude latitude bathy

where the bathymetry value (bathy) should be  $< 0$ .

These interpolations are sometimes more successful when interpolating onto unstructured meshes. This method only interpolates over valid wet cells, therefore no 'filling' of land cells that may be potentially included in interpolations is required. Valid bathymetry netCDF dimension names recognised are (for x dimension, y dimension, bathymetry name, x coordinate name, y coordinate name):

```
i_centre, j_centre, botz, x_centre, y_centre  
lon, lat, height, lon, lat
```

COMPAS may also ingest a .mnc file containing a list of bathymetries and interpolation rules, that preferentially are interpolated onto the intersections of convex hulls of the model domain and the bathymetry bounds in a sequential order. This allows bathymetry interpolation to be built up using small, detailed, datasets first and large regional datasets last. The format of the .mnc file is:

```
multi-netcdf-version 1.0  
nfiles n+1  
file0.filename /path0/file0.bty nn_sibson  
file1.filename /path1/file1.bty linear  
file2.filename /path2/file2.nc none  
.  
.  
filen.filename /pathn/filen.nc nn_sibson
```

COMPAS example bathymetry specifications may be:

```
BATHYFILE          bathy.nc      # Bi-linear interpolation  
  
BATHYFILE          bathy.nc      # Natural neighbour interpolation  
BATHY_INTERP_RULE nn_sibson  
  
# Bi-linear interpolation for bathy1.nc and natural neighbours  
# interpolation for bathy2.nc  
BATHYFILE          bathy1.nc bathy2.nc  
BATHY_INTERP_RULE nn_sibson  
  
# Natural neighbour interpolation for bathy1.nc and linear for  
# bathy2.nc  
BATHYFILE          bathy1.nc bathy2.nc  
BATHY_INTERP_RULE nn_sibson linear  
  
# Bi-linear interpolation for bathy1.nc and linear for  
# bathy2.nc  
BATHYFILE          bathy1.nc bathy2.nc  
BATHY_INTERP_RULE none linear  
  
BATHYFILE          bathy.bty     # Natural neighbour interpolation  
BATHY_INTERP_RULE nn_sibson  
  
BATHYFILE          bathy.mnc     # List of bathymetries and rules
```

Large bathymetry input files may exhaust memory during the triangulation process for unstructured interpolations (`BATHY_INTERP_RULE != NONE`). If a bathymetry file is greater than 80 million cells (currently), then the file is split into sub-sections that are then interpolated individually (with some overlap). The user may further reduce the bathymetry points used in

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the interpolation to only those lying within the convex hull (boundaing perimeter) of the mesh by setting:

```
BATHY_TRUNCATE      YES
```

This can speed the interpolation process considerably for large bathy files. The user may explicitly set the number of sub-sections to n using:

```
BATHY_SECTION      n
```

When using these bathymetry options for COMPAS with coastline fitted meshes (i.e. all cells are wet), it is possible that land values are included in interpolations to result in valid wet cells receiving a bathymetry value that is subsequently flagged as land. COMPAS will remove these land cells by default when building a mesh. If removal is not required, the following can be used to invoke altenative action:

```
BATHYFILL  REMOVE # Remove land cells from the mesh (default.)
           MIMIMUM # Replace land cells in the mesh with the minimum.
           AVERAGE # Replace land cells in the mesh with the average
                   # of valid surrounding wet cells.
```

Several further bathymetry options are supported for SHOC/COMPAS; if a ROMS grid has been converted (Section 4.7.6), then the ROMS bathymetry may also be used by specifying:

```
ROMS_GRID_OPTS     BATHY
```

If `MOM_GRID` has been specified for the grid generation (Section 4.7.6), then the bathymetry will be also read from the supplied `grid_spec.nc` file.

For convenience, some parameters are provided which allow the specification of minimum and maximum depth values, as follows:

```
# All cells will be at least 20m deep
BATHYMIN      20

# No cell will be more than 2000m deep
BATHYMAX     2000
```

The `BATHYMIN` and `BATHYMAX` parameters are optional. If present, they override values in the `BATHY` array where necessary.

The bathymetry can be smoothed using a 9 point low pass convolution filter if required. This may be done several times by invoking:

```
# n is the number of smoothing passes performed
SMOOTHING    n      #
```

Alternatively, a maximum gradient threshold may be supplied, and if the local bathymetry gradient becomes greater than this threshold then the bathymetry is locally smoothed until the gradient becomes less than the threshold. This is accomplished by invoking:

```
# x is the gradient threshold, typically 0.07
MAXGRAD     x
```

Bathymetry smoothing may be performed over a discrete number of cells (with n smoothing passes) using:

```
SMOOTH_MASK      m      # m is the number of cells to smooth
1 1              # List of (i,j) cell locations
```

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**COMPAS** only: Bathymetry may be smoothed in a series of supplied closed polygons only using:

```
SMOOTH_POLY          p1.xy p2.xy .. pn.xy
```

Where p1.xy, p2.xy are closed polygons defined by a series of geographic locations (e.g. longitude, latitude).

Using COMPAS, a bathymetry value may be replaced with a median value of its neighbours if that bathymetry value and all its neighbours values differ by more than a threshold, *diff*; e.g;

```
MAXDIFF             <diff>
```

A replacement with the median may occur only if the number of neighbouring cells whose difference is more than *diff* is  $NPE - thr$ , where *NPE* is the number of neighbouring cells and *thr* is supplied by the user;

```
MAXDIFF             <diff> <thr>
```

e.g. replace a cell with the median if all neighbouring cells minus one have a difference greater than 500m;

```
MAXDIFF             500 1
```

Median filtering over all bathymetry cells is invoked using;

```
MAXDIFF             median
```

Note that depth values need not correspond to layer interface positions. In each cell, the model implements a bottom layer which has a thickness which may be less than the full layer thickness, so that bathymetry is well resolved even in vertically coarse or single-layer (depth-averaged) grids. However, very thin bottom layers can cause numerical problems, so one final parameter prevents the creation of very thin layers, as follows:

```
# If the difference between a layer boundary and the bathymetry
# for a cell is too small, numerical instabilities can arise
# in the model. Specifying a minimum cell thickness ensures that
# no cell can get too thin.
# The value may be specified as a minimum thickness (in metres)
# or as a minimum percentage of the grid layer thickness, as
# shown below.
MIN_CELL_THICKNESS 15%
```

A sub-section of the bathymetry may be masked to a user defined value using the *BATHY\_MASK* attribute. This consists of a list of (i,j) values for structured grids, or a list of cell indices for unstructured meshes, whose bathymetry value in the grid is set to the value of *BATHY\_MASK\_VAL*, e.g;

```
# Structured grids (SHOC or COMPAS)
# Set the bathymetry at points (1,1) and (2,1) equal to 5.0m.
BATHY_MASK_VAL      5.0      # Value to set bathymetry to.
BATHY_MASK          2        # Number of points in the list.
1 1
2 1
```

or

```
BATHY_MASK_VAL      5.0      # Value to set bathymetry to.
```

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```
BATHY_MASK      1      # Number of blocks in the list.
(1,1)-(2,1)

# Unstructured grids (COMPAS only)
# Set the bathymetry at cell indices 12, 20 and 62 equal to
# 5.0m.
BATHY_MASK_VAL  5.0    # Value to set bathymetry to.
BATHY_MASK      2      # Number of points in the list.
12
20
62
```

or

```
# Set the bathymetry from cell index 12 to cell index 20 equal
# to 5.0m.
BATHY_MASK_VAL  5.0    # Value to set bathymetry to.
BATHY_MASK      2      # Number of points in the list.
(12)-(20)
```

The points list may be obtained using the 'Marked' facility in `jvismeco`. A linear gradient of bathymetry may also be applied to the masked sub-region in either the `e1` or `e2` direction (`i` or `j` direction), e.g. to apply a linear bottom slope in the `e1` direction from 5m to 10m:

```
# Set a linear bottom slope from 2m to 10m in the e1 direction
# from i=1 to i = 4. Any points in the list with i coordinates
# between the start and end coordinates are set to a linear
# interpolation of the start and end depths.
BATHY_MASK_IS   1      # Start i coordinate (or cell index for
# COMPAS) for gradient.
BATHY_MASK_IE   4      # End i coordinate (or cell index for
# COMPAS) for gradient
BATHY_MASK_DS   2.0    # Depth at start i coordinate / index
BATHY_MASK_DE   10.0   # Depth at end i coordinate / index
BATHY_MASK      40     # Number of points in the list
```

Similarly this applies to `BATHY_MASK_JS` and `BATHY_MASK_JE` for the `e2` direction (**SHOC only**).

Multiple blocks may be specified where a single bathymetry value only may be altered (i.e. no gradients of bathymetry) using:

```
BATHY_NBLOCKS   2      # Number of blocks
BATHY_MASK_VAL0  5.0    # Block 0 bathymetry value
BATHY_MASK0     1      # Block 0 blocks.
(1,1)-(2,1)
BATHY_MASK_VAL1  2.0    # Block 1 bathymetry value
BATHY_MASK1     2      # Block 1 blocks.
(10,1)-(20,10)
(50,1)-(50,20)
```

The format of the cell lists in these blocks should conform to the conventions outlined above for structured or unstructured grids.

### COMPAS only:

A path file may be submitted to `BATHY_MASK_VAL` after the bathymetry value. In this case, all cell centres having a minimum distance to the locations specified in the path are set to the bathymetry value, e.g.

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```
BATHY_MASK_VAL    5.0 bathypath.xy
```

With `bathypath.xy` a list of longitude / latitude locations:

```
147.1853943    -42.7399275
147.1868834    -42.7389463
147.1886657    -42.7374662
147.1911701    -42.7378653
```

If a closed polygon is submitted as the list of locations, then all cells lying within that polygon may be bathymetry masked using, e.g.;

```
BATHY_MASK_VAL    poly 5.0 bathypath.xy
```

The minimum bathymetry (BATHYMIN) may be set only within the polygon using, e.g.;

```
BATHY_MASK_VAL    min 5.0 bathypath.xy
```

Both the path and polygon may be used with the `BATHY_NBLOCKS` construct (above).

**NOTE:** The bathymetric parameters described above are not used by the model when a run is initiated using the `-p` option. They are used when the `-g` option is invoked (see section 8) to generate the model input netCDF file, which contains model initial values and geometric information. Any alteration to model bathymetry must be accompanied by the creation of a new model input netCDF file, using the `-g` option.

Cells can be changed to `OUTSIDE` or `LAND` status at runtime as a series of rectangular blocks e.g.;

```
NOUTSIDE    3    # Set a series of rectangular regions to
(0,3)-(82,69) # OUTSIDE.
(184,3)-(248,69)
(0,70)-(248,131)
```

or

```
NLAND 4    # Set a list of points to LAND.
0 1
0 2
0 3
0 4
```

### COMPAS only:

The `NOUTSIDE` option is redundant in COMPAS, and `NLAND` will remove the nominated cell from the mesh. Note that cell indices must be supplied when using `NLAND` with COMPAS, or a list of polygons may be supplied, with any cell centre lying inside the polygon removed:

```
NLAND    n    # Number of polygons
poly1.xy    # Polygon #1 to remove cells
poly2.xy    # Polygon #2 to remove cells
.
.
polyn.xy    # Polygon #n to remove cells
```

Bathymetry statistics can be generated using:

```
BATHY_STATS    <infile> e1i e2i
```

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Here <infile> is a path and filename of a bathymetry database and e1i and e2i are decimations in the e1 and e2 directions respectively. Bathymetry statistics are generated by comparing the database bathymetry at its native resolution (with the decimation applied) with the interpolated bathymetry in a model grid. Statistics generated are:

- Maximum depth between the shallowest database depth in a grid cell and the model grid cell depth, stored in `bathy_range_min`,
- Maximum depth between the deepest database depth in a grid cell and the model grid cell depth, stored in `bathy_range_max`,
- The gradient of the model grid cell;  $\sqrt{\left(\frac{\partial}{\partial x_1}\right)^2 + \left(\frac{\partial}{\partial x_2}\right)^2}$ , stored in `bathy_grad`,
- The maximum gradient difference between the database gradient and the gradient in the grid cell, where the gradient is defined above, stored in `bathy_grad_max`.

## 4.10 Tracers (salinity, temperature, and others)

The model may include salinity and temperature as dynamic tracers which affect the density field via an equation of state. As well, some of the more complex vertical mixing schemes may use variables (like turbulent kinetic energy) which also essentially act as tracers as far as most of the model code is concerned. Finally, the model can include an arbitrary number of passive tracers, which are advected and diffused in the model grid, but which play no dynamic role.

The set of tracers included and their physical behaviour are defined as shown in the example below. The number of tracers included is specified using the parameter `NTRACERS`, and attributes for each tracer are prefixed by `TRACER<M>`, where <M> corresponds to the tracer number (starting at zero).

Tracers can be defined to exist in the water column (3D tracers), the benthos (2D tracers; these tracers may also represent vertically integrated 3D tracers or values at the air-water or water-sediment interfaces) or in the sediment (3D sediment tracers).

The following example shows the specification of three tracers - salinity, temperature and a passive dissolved contaminant. Detailed comments are provided for the salinity tracer.

```
NTRACERS 3                # Three tracers in this grid

# The following tracer attributes are mandatory, and must
# be present for each tracer
#
# Tracer name (must be 'salt' for dynamic salinity variable)
TRACER0.name salt

# A more descriptive name.
TRACER0.long_name Salinity

# Units string
TRACER0.units PSU        # Standard units

# Fill value for use with the -g option if no data is present
# (see below).
TRACER0.fill_value 35.0

# Range (minimum and maximum) of valid values
TRACER0.valid_range 0 40
```

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```
#
# The following tracer attributes are optional
#
# The type of tracer. Options are WATER, WC3D or WC for 3D water
# column tracers, BENTHIC, INTER or WC2D for 2D tracers and
# SEDIMENT or SED for sediment tracers. Tracers are assumed to be
# 3D water column tracers by default.
TRACER0.type WATER

# Allow the tracer to be advected (default is 1, or TRUE)
TRACER0.advect 1

# Allow the tracer to be diffused (default is 1, or TRUE)
TRACER0.diffuse 1

# Decay constant in seconds (default is 0.0, meaning no decay).
# This may also be the name of a tracer; in this case the values
# of that tracer (with units of that tracer; seconds, minutes,
# hours, days) will be used as the decay rate. This allows for
# spatially and temporally varying decay rates. Negative decay
# is equivalent to growth.
TRACER0.decay 0.0

# Settling velocity if required (m/s, -ve down) (default is 0.0)
TRACER0.svel 0.0
```

The `.data` attribute allows the specification of initial values for each tracer. This is of use when the initial values vary in space, or are obtained from observations.

```
# Data to initialize the tracer
TRACER0.data <data_field>
```

The tracer data field, `<data_field>`, may be one of the following:

- The size of the grid, `nce1 x nce2 x nz`, followed by an array of values of size `nce1 x nce2 x nz`, listed in that order,
- a netCDF file on a regular grid, in which case the values will be bilinearly interpolated,
- a netCDF file on an irregular grid, in which case interpolation is performed using an inverse distance weighting scheme,
- an ascii file in column format with spatial information only (i.e. no time field, `lon` and `lat` must be present). In this case the tracer values are interpolated linearly by default, or as specified in the `.interp_type` field. This is useful for interpolating sparsely collected measurements onto the grid.

```
# Interpolation method for ascii data input
TRACER0.interp_type cubic # valid options are cubic, linear,
                          # average, nn_sibson or
                          # nn_non_sibson, where nn
                          # refers to Natural Neighbours.
```

- A data format of the type:

```
[data=file.nc(tracer=tracer_name)(t=<n>days)]
```

This must be used in conjunction with `interp_type`. In this case the wet cells only in the netCDF file `file.nc` on a regular grid are interpolated using the unstructured interpolation scheme `interp_type`. Variable substitution may be optionally used where the tracer name (`tracer`) uses the variable `tracer_name` in `file.nc`. The record at `n` days is used for interpolation (note; there should be no white space in this specification). An examples for tracer `salt` is:

```
TRACER0.data [data=file.nc(salt=salt_obs)(t=10days)]
```

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```
TRACER0.data [data=file.nc(t=100seconds)]
```

- Tracers may be scaled to a normalized density profile that exists through the water column (i.e. at the deepest point in the domain). This ensures that the gradient of the tracer profile is some constant multiple of the density gradient, and therefore ensures that mixed layer depths are consistent between the tracer and density. This is invoked using:

```
TRACER0.data dens_scale file.nc v1 v2 <code>
```

Where  $v_1$  is the depth at which the tracer value is equal to that in `file.nc` at the same depth and  $v_2$  is a scaling factor for the profile (if  $v_2 < 0$  the profile is inverted). Below depth  $v_1$  the profile in any layer  $k$  is determined by adding  $v_2 \times$  (density gradient) to the concentration in the layer  $k+1$ . This is iteratively computed down through the water column. Above depth  $v_1$  the profile in any layer  $k$  is determined by subtracting  $v_2 \times$  (density gradient) to the concentration in the layer  $k-1$ . This is iteratively computed up through the water column. If `<code> = c` then a copy of the values in `file.nc` is used for the profile below depth  $v_1$ , and if `<code> = t` then the profile values are truncated to those in `file.nc` below the depth  $v_1$  if the profile values become greater than those in `file.nc`.

This formulation is the most general for density scaling and is supported by an equivalent scaling at open boundaries (see Section 4.10.18) – other methods may be used that are not supported by equivalent open boundary methods.

```
TRACER0.data dens_scale v1 v2
```

Here, if  $v_2 > 0$  then  $v_1$  is the surface tracer concentration, and the profile in any layer  $k$  is determined by adding  $v_2 \times$  (density gradient) to the concentration in the layer  $k+1$ . This is iteratively computed down through the water column. If  $v_2 < 0$  then  $v_1$  is the bottom tracer concentration, and the profile in any layer  $k$  is determined by subtracting  $v_2 \times$  (density gradient) to the concentration in the layer  $k-1$ . This is iteratively computed up through the water column. A file (netCDF or ascii time series) may be used as the surface or bottom value in preference to  $v_1$ , in this case use;

```
TRACER0.data dens_scale file.nc v2
```

The tracer profile may be the inverse of the density profile if the following is specified:

```
TRACER0.data dens_scale v1 v2 n
TRACER0.data dens_scale file.nc v2 n
or
TRACER0.data dens_scale v1 v2 inverse
TRACER0.data dens_scale file.nc v2 inverse
```

- An alternative density scaling is possible where the normalized density profile is stretched between a surface value of  $v_1$  and bottom value of  $v_2$ . This is invoked using:

```
TRACER0.data dens_profile v1 v2
```

- Tracer values may be specified in regions using:

```
TRACER0.data region region.bnc r1:v1 r2:v2 .... rn:vn
```

Where `region.bnc` is a region file (see Section 4.31.21). The values in specified regions  $r_1, r_2 \dots r_n$  are then assigned the values  $v_1, v_2 \dots v_n$  respectively. Data from separate regular netCDF files can be interpolated using the unstructured interpolation scheme `interp_type` with:



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```
TRACER0.data      [region=region.bnc]
                  [r1:file1.nc(tracer=tracer_name)(t=<n1>days)]
                  [r2:file2.nc(tracer=tracer_name)(t=<n2>days)]
```

**COMPAS** only: a netCDF file on a regular grid can be supplied with an `interp_type`. In this case the gridded data is interpolated in an unstructured sense after being transposed to a triangulated mesh. This can often result in better interpolations onto unstructured meshes, and can extrapolate tracer data more accurately onto the unstructured mesh. This method also only interpolates over valid wet cells, therefore no 'filling' of land cells that may be potentially included in interpolations is required.

Tracer specification examples are:

```
# Temperature tracer - only mandatory attributes given here. The
# rest will assume their default values.
TRACER1.name temp
TRACER1.long_name Temperature
TRACER1.units degrees C
TRACER1.fill_value 20.0
TRACER1.valid_range 0 40

# Passive, dissolved contaminant tracer; specifying an
# initial distribution from a netCDF time-series file called
# profile.nc. Note that the fill_value attribute must still
# be present (but isn't used).
TRACER2.name contam
TRACER2.long_name Contaminant
TRACER2.units kg m-3
TRACER2.fill_value 0.0
TRACER2.valid_range 0 2
TRACER2.data profile.nc
```

Note that the valid range attribute is a recommendation only and **SHOC/COMPAS** takes no action other than supplying a warning if these bounds are violated. The exception is, however, if the minimum range is zero and the model begins to produce negative results. In this case the tracer value is clipped to zero in **SHOC/COMPAS** to ensure positive-definiteness.

## 4.10.1 Tracer initialisation

When a run is initiated, the initial distribution for each tracer are read from the `INPUT_FILE`. This file may be generated using the `-g` option or be an output file from a previous run. If the `-g` option was used, then the `INPUT_FILE` will contain tracer distributions that reflect either the `.fill_value` or `.data` specified for that tracer (see above). However, if a run is initiated which has tracers in the tracer list that do not have corresponding distributions in the `INPUT_FILE` (i.e. new tracers are added) then the initial distributions for those tracers will be specified using any `.data` specified, or if this is absent then the `.fill_value`. Additionally, a netCDF file may be specified using;

```
# Specify a netCDF file to initialise any new tracers
TRACER_DATA      <data_file>
```

In this case, if the `.data` attribute is absent for any new tracers, SHOC will search the file `<data_file>` for the new tracer, and if found interpolate the initial tracer distribution from that in the file. This is done for 3D, 2D and sediment tracers.

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## 4.10.2 Relaxation

Tracer values throughout the model domain can be relaxed towards some specified values (which may themselves vary in space and time). To enable relaxation for a particular tracer, three parameters are required: the relaxation data file (an ASCII or netCDF time-series file – see section 10), how often to perform the relaxation, and the relaxation time constant.

```
# Data file containing prescribed tracer values
TRACER0.relaxation_file      saltprof.nc

# How often to perform relaxation calculation
TRACER0.relaxation_input_dt  1 hour

# Relaxation time constant
TRACER0.relaxation_time_constant 20 days
```

Tracer relaxation may also be specified via a streamlined notation:

```
relax_trname      infile.nc dt.ts in units
```

where `trname` is the name of tracer, `infile.nc` is the file containing values to relax to, and `in units` is the `input_dt`; e.g. to relax salt to `saltprof.nc` with file input of 1 hour and relaxation constant set in `dt.ts`, then specify;

```
relax_salt  saltprof.nc dt.ts 1 hour
```

This specification is particularly useful with the automated `-a` or `-r` options, but will only operate if the relaxation time constant is input via file.

The `relaxation_time_constant` may be time dependent by specifying a netCDF or ascii filename. In this case the units for the time constant in the file must be a time unit, e.g.

```
# Ascii relaxation file where relaxation is 48 hours at day 0 and 2
# hours at day 10. Note 'Time' is converted to the model units
# specified by TIMEUNIT.
## COLUMNS 2
##
## COLUMN1.name      Time
## COLUMN1.long_name Time
## COLUMN1.units     days since 1990-01-01 00:00:00 +8
## COLUMN1.missing_value -999
## COLUMN1.fill_value  0.0
##
## COLUMN2.name      relaxation_time_constant
## COLUMN2.long_name Relaxation time constant
## COLUMN2.units     hours
## COLUMN2.missing_value -999
## COLUMN2.fill_value  0.0
##
0 48
10 2
```

Adaptive relaxation can be invoked by specifying:

```
TRACER0.relaxation_time_constant linear dv1 tc1 units1 dv2 tc2 units2
```

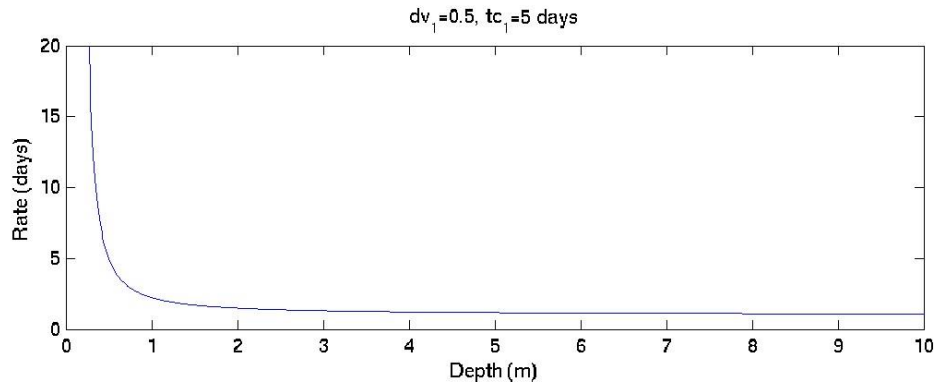
In this case if the absolute difference between modelled tracer and that read from `infile.nc` is `dv1`, then a relaxation constant of `tc1 units1` is used and if the absolute difference is `dv2`, then a relaxation constant of `tc2 units2` is used, with linear interpolation

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for other values of the absolute difference. The relaxation constant will therefore vary spatially and temporally throughout the domain and simulation. For exponential relaxation:

```
TRACER0.relaxation_time_constant exponential dv1 tc1 units1
```

In this case the relaxation constant is given by:  $rate = [\exp(\log(q)/d)]^{-1}$  where  $d$  is the absolute difference in modelled tracer and that read from `infile.nc`, e.g. for  $dv_1 = 0.5$  and  $tc_1 = 5$  day;



A depth scaled linear relaxation may be specified using:

```
TRACER0.relaxation_time_constant depth dv1 tc1 units1 dv2 tc2 units2
```

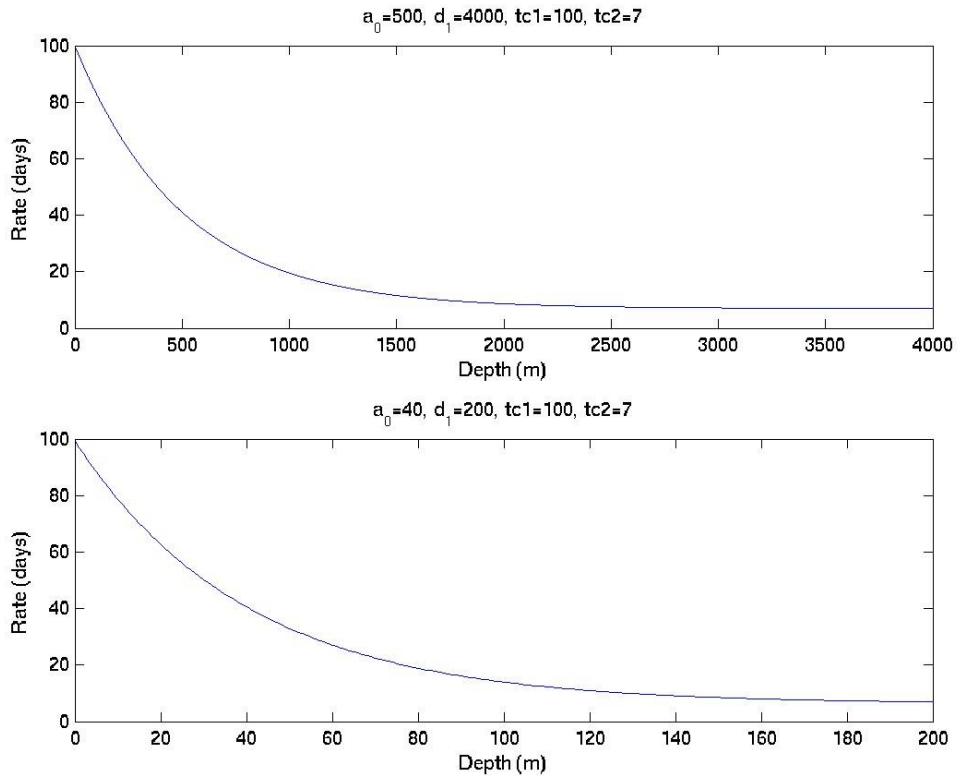
In this case if the depth is  $dv_1$ , then a relaxation constant of  $tc_1$  units<sub>1</sub> is used and if the depth is  $dv_2$ , then a relaxation constant of  $tc_2$  units<sub>2</sub> is used, with linear interpolation for other values of the depth. The relaxation constant will therefore vary spatially throughout the domain and simulation. Depths are truncated to the limits of  $dv_1$  and  $dv_2$ . Note that all depths should be negative (i.e.  $dv_1$  and  $dv_2 < 0.0$ ).

An exponential depth dependent rate may be specified using:

```
TRACER0.relaxation_time_constant exp_depth a0 tc1 units1 d1 tc2 units2
```

The relaxation rate is given by  $rate = (tc_2 - tc_1) \exp(\text{depth}/a_0) + (tc_2 - tc)$  where  $tc = tc_1 \exp(d_1/a_0)$ . Examples for different depths  $d_1$  are shown below.

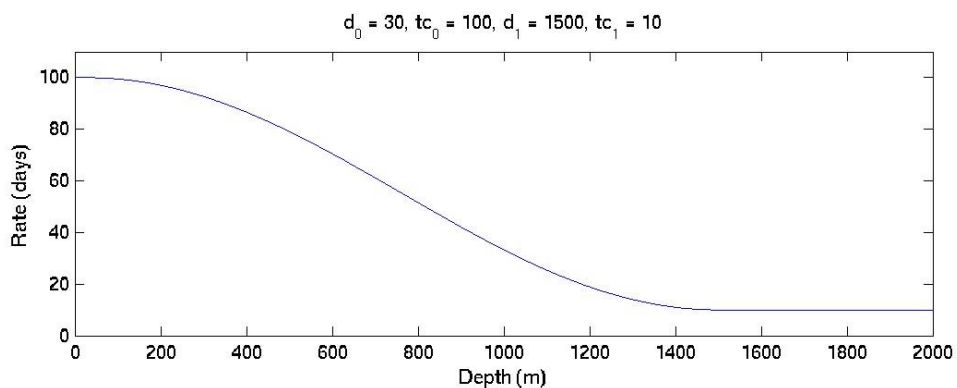
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An cosine depth dependent rate may be specified using:

```
TRACER0.relaxation_time_constant cos_depth d0 tc1 units1 d1 tc2 units2
```

The relaxation rate is given by  $rate=0.5*(tc_1-tc_2)\cos(\pi*depth/(d_1-d_0))-d_1*\pi/(d_1-d_0)+(tc_1+tc_2)$ . This formulation assumes  $d_1 > d_2$ . An example is shown below.



Relaxation rate linear in time may be specified using:

```
TRACER0.relaxation_time_constant temporal dv1 tc1 units1 dv2 tc2 units2
```

In this case the relaxation rate is  $tc_1 units_1$  at  $dv_1$  days (relative to the TIMEUNIT), changing linearly to  $tc_2 units_2$  at  $dv_2$  days, then thereafter capped at  $tc_2 units_2$ .

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## 4.10.3 *Resetting*

Tracer values throughout the model domain can be reset to some specified distribution (which may vary in space and time). To enable resetting for a particular tracer, two parameters are required: the reset data file (an ASCII or netCDF time-series file – see section 10) and how often to perform the reset. Using this option allows the user to effectively force the model with supplied distributions of tracer.

```
# Data file containing prescribed tracer values
TRACER0.reset_file  saltprof.nc

# How often to reset the tracer
TRACER0.reset_dt    1 hour
```

## 4.10.4 *Tracer Increments for State Variables*

The value of a tracer subject to resetting may be added to a state variable. This procedure is an easy way to update state variables if the reset file is created from a data assimilation process offline. The state variable the tracer is added to is specified via:

```
# Add the tracer values to temperature
TRACER0.increment  TEMP
```

Valid values for state variable increments are:

```
TEMP      # 3D tracer value added to temperature
SALT      # 3D tracer value added to salinity
ETA       # 2D tracer value added to surface elevation
```

## 4.10.5 *Scaling*

The initial conditions specified for any tracer may be scaled by another tracer's values. This is useful for easily manipulating input data without creating a new initialisation files, for example when scaling is required to convert to the correct units for tracer input. The scaling may either be additive or multiplicative. To scale a given tracer, e.g. `tracer1.name = temp`, the scaling tracer, e.g. `tracer2`, must be set up and initialised, e.g;

```
TRACER2.name      scale
TRACER2.long_name  Scaling tracer
TRACER2.units     degrees C
TRACER2.scale_s   temp # Add tracer2 values to tracer temp
TRACER2.fill_value 20.0
TRACER2.valid_range 0 40
TRACER2.advect    0
TRACER2.diffuse   0
TRACER2.diagn     0
TRACER2.data      scale_profile.nc # Initialisation for tracer2
```

In this case the tracer named 'temp' is scaled additively by the data contained in the file `scale_profile.nc`. If the tracer were to be scaled multiplicatively, then use:

```
TRACER2.scale_p   temp # Multiply tracer temp by tracer2 values
```

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Alternatively, within the tracer attributes for the tracer desired to be scaled (e.g. `temp` in this case), the following attributes may be set:

```
TRACER1.name temp
# Additively scale tracer 'temp' by the values in tracer 'scale'
TRACER1.tag scale_s:scale

# Multiplicatively scale tracer 'temp' by the values of 'scale'
TRACER1.tag scale_p:scale

# Additively scale tracer 'temp' by a constant (2 in this case)
TRACER1.tag scale_s:2.0

# Multiplicatively scale tracer 'temp' by a constant (0.01)
TRACER1.tag scale_p:0.01
```

Tracer scaling is invoked upon initialisation, and if any tracers are reset (Section 4.9.3).

## 4.10.5.1 Timeseries scaling

A tracer scaling file may be generated from time series files of moored instrument data, or from profile measurements. To invoke this option set the `create_scale` attribute to a scaling map file, the format of which is described below, e.g:

```
TRACER2.create_scale moor_temp.map
```

With the file `moor_temp.map` with the format:

```
VAR_NAME      temp           # name of the variable to scale
VAR_UNITS     Degrees_C    # Units of the variable
OUT_NAME      scale_temp_s  # Name of the scaling variable as
                        # it will appear in the output
                        # file.
OUT_FILE      scale_profile.nc # Output file name.
FORCING       profile.nc    # The initialisation file for the
                        # variable VAR_NAME that requires
                        # scaling. May be a multifile.
REF_VALUE     1             # Optional reference value.
REF_DEPTH     -100          # Optional reference depth (m).
BOT_VALUE     temp_init.nc  # Optional bottom value.
nfiles        2
file0         moor1.ts 147.34 -43.05 -15.0 temp
file1         prof1.nc 147.34 -43.05 profile temp
```

In the above example it is assumed that there exist files `profile.nc`, `moor1.ts` and `prof1.nc` that contain the variable `temp` with units `Degrees_C`. The file `profile.nc` is the initialisation file for the variable `temp` used in the model, and this file is known to contain errors which are required to be corrected by scaling to measured data contained in data files `moor1.ts` and `prof1.nc`. The geographic (longitude and latitude) locations and depth (depth < 0) for each mooring file are supplied (e.g. `file0`). Alternatively a profile at a geographic location may be used; in this case use `profile` instead of a numeric depth value (e.g. `file1`). The variable name used in the each mooring or profile file must also be supplied. Mooring files generally contain the variable as a function of time (`.ts` files), and profile files contain the variable at a specific time as a function of depth at a fixed geographic location (`.nc` files). The scaling routine will compute the difference between the measured data and the `FORCING` data, and store this as a spatially and temporally varying netCDF file,

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`OUT_FILE` (i.e. the sum of `OUT_FILE` and `FORCING` will equal the measured data). The scaling function is spatially interpolated over the model grid. Only an additive scaling function is available (i.e. product scaling is not supported). Additionally, an ascii file `OUT_NAME.ts` containing the raw data (`TIME`, `file#`, observed data `FORCING` data) is produced. This is useful for creating scatter plots of the observed vs `FORCING` data.

Additionally, the bottom value may be explicitly set to a particular value (temperature in this example) using the optional `BOT_VALUE`. This may be a number or a filename, whose value(s) are used in preference to those contained in the measured data files (`moor1.ts` and `prof1.nc`) at the sea bottom. For example, if the `BOT_VALUE` were the same data as used for the `FORCING` (i.e. `profile.nc`) then this would ensure that the scaling function would equal zero at the bottom. The scaling code actually adopts this approach by default for all depths greater than the deepest mooring at a particular geographic location.

The optional `REF_VALUE` and `REF_DEPTH` operate in a similar manner to the `BOT_VALUE`, except a particular value (temperature in this example) can be prescribed at the depth `REF_DEPTH` rather than at the bottom. In the absence of a `BOT_VALUE`, all values below the `REF_DEPTH` are set to the `REF_VALUE` in preference to those contained in the measured data files (`moor1.ts` and `prof1.nc`). The reference and bottom options are useful for prescribing the scaling function below depths where no measured data is available but the user has insight into what values are expected at those depths.

### 4.10.5.2 Glider Scaling

Scaling may also be generated using data from glider missions. In this case the scaling field is static (time-independent) but spatially variable. The scaling can be done for individual glider missions, applied to different forcing data. The spatial distribution can be uniform from a mean scaling profile, or interpolated using `grid_specs` interpolation. A cascade search may also be applied. In this case, the `.map` file takes the form:

```
VAR_UNITS      degrees_C      # Units of the tracer
START          9100 days    # Start time for scaling
STOP           9188 days    # End time for scaling
STEP           10 minutes
METHOD         cascade     # Filling method:
                        # cascade = cascade fill.
                        # profile = constant using a mean
                        #           vertical profile.
                        # linear, nn_sibson, nn_non_sibson,
                        # cubic, nearest = grid_spec
                        # interpolation.
nfiles 2        # Number of scaling files
file0 glider0.ts x y z temp_obs data0.nc temp
file1 glider1.ts x y z temp_obs data1.nc temp 9175 9176.5 days
```

The glider data `glider0.ts`, `glider1.ts` are timeseries output using the `GLIDER` timeseries metric (Section 4.31.22). The labels `x`, `y` and `z` are the geographic `x`, `y` and depth coordinates in this file, and `temp_obs` is the name of the variable in the file to use. The files `data0.nc`, `data1.nc` are the data to be scaled (e.g. global model output), and `temp` is the name of the variable in these files. An optional date range can be included within which glider data is only used for scaling.

The scaling tracer may be initialised with the `OUT_FILE` created using the `create_scale` option, and if this file is also used as a `reset_file` then the scaling tracer may be used to scale the open boundary forcing in a time dependent manner (Section 4.11.18).

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## 4.10.6 Filtering

Vertical edge enhancement may be performed on initialization with .data using a Laplacian edge enhancement 3x3 convolution filter. This is performed in the x-z plane followed by the y-z plane. Filtering is invoked using:

```
TRACER2.name           passive
TRACER2.long_name      Passive tracer
TRACER2.units          gm-3
TRACER2.fill_value     0.0
TRACER2.valid_range    0 100
TRACER2.advect         1
TRACER2.diffuse        1
TRACER2.diagn          0
TRACER2.tag            hipass_vert:c
TRACER2.data           data.nc
```

Where the value  $c$  is typically 1 or 2 as used in the convolution filter:

$$K = \begin{bmatrix} -1 & -c & -1 \\ 0 & 0 & 0 \\ 1 & c & 1 \end{bmatrix}$$

## 4.10.7 Surface fluxes

A 3D tracer defined in the tracer list may have a surface flux prescribed that acts as the upper boundary condition in the vertical diffusion equation (see Section 2.5, Science Manual). This implies that the tracer is allowed to be vertically diffused. The flux tracer is introduced by specifying the name of a valid 2D tracer in the tracer list as follows (e.g. for tracer `passive`);

```
TRACER2.name           passive
TRACER2.long_name      Passive tracer
TRACER2.units          gm-3
TRACER2.fill_value     0.0
TRACER2.valid_range    0 100
TRACER2.advect         1
TRACER2.diffuse        1
TRACER2.diagn          0
TRACER2.tag            surf_flux:flux
```

This implies a 2D tracer flux must exist, which may vary in space and time using the reset function. The tracer may also be scaled to achieve the correct units:

```
TRACER3.name           flux
TRACER3.long_name      Surface flux
TRACER3.units          kgm-2s-1
TRACER3.type           WC2D
TRACER3.fill_value     0.0
TRACER3.valid_range    0 100
TRACER3.advect         0
TRACER3.diffuse        0
TRACER3.diagn          0
TRACER3.tag            scale_p:0.001
TRACER3.data           flux_data.nc
TRACER3.reset_file     flux_data.nc
TRACER3.reset_dt       1 day
```



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Note that a positive flux implies a flux out of the surface layer.

## 4.10.8 Tracer types

The following flags are currently supported by the `TRACER.type` flag:

WATER	The tracer is a 3D water column tracer
SEDIM	The tracer is a 3D sediment tracer
INTER	The tracer is a 2D tracer
HYDRO	The tracer is a hydrodynamic tracer
SEDIMENT	The tracer is a sediment transport tracer
ECOLOGY	The tracer is a biogeochemical tracer
WAVE	The tracer is a wave tracer
TRACERSTAT	The tracer is a tracer statistic tracer
PROGNOSTIC	The tracer is prognostic
DIAGNOSTIC	The tracer is diagnostic
PARAMETER	The tracer represents a parameter
FORCING	The tracer contains forcing data

These flags may be assigned to tracers explicitly in the parameter file, e.g;

```
TRACER1.type      WATER HYDRO PROGNOSTIC
```

The above defines a tracer as a 3D hydrodynamic prognostic tracer. For auto-tracers, these flags are set internally. The `type` flag may be interrogated within the code for various purposes. The list may also be expanded as required.

## 4.10.9 Tracer filling and filtering

It is common that coastlines and bathymetries do not align when interpolating tracers onto a grid from an external file. Sometimes the limits of the grid that are to be interpolated onto lie outside the geographic bounds of the file from which the data is interpolated. There exist data filling options to set no-gradient conditions over cells whose geographic location is outside the bounds, or over cells that are associated with land, in the file from which data is interpolated. This can be done for 2D (including elevation), 3D or sediment tracers, and is invoked using:

```
TRACER_FILTER FILL      # Fill all tracers with a no-gradient
                FILL2D   # Fill only 2D tracers with a no gradient
                FILL3D   # Fill only 3D tracers with a no gradient
                FILLSED  # Fill only sediment tracers with a no gradient
                SMOOTH   # Apply 9 point smoothing filter to filled data
                SHAPIRO  # Apply Shapiro filter to filled data
                SHUMAN   # Apply Shuman filter to filled data
                MEDIAN   # Apply median filter to filled data
```

These keywords can be combined sequentially, e.g;

```
TRACER_FILTER FILL2D FILL3D SMOOTH SHUMAN MEDIAN
```

**COMPAS only:** the use of netCDF `TRACER.data` in conjunction with an `interp_type` (see above) will also extrapolate outside the geographic bounds of the file from which the data is interpolated, and is an alternative to the use of `TRACER_FILTER` options.

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## 4.11 Open boundaries

Each open boundary (if there are any) is specified as a list of horizontal grid cell locations, together with parameters which define the nature and behaviour of the boundary. The cells in a single open boundary do not necessarily need to be adjacent to one another, but it is usually desirable to group boundary cells that are physically or logically related. For each open boundary it is usually necessary to define data files from which the boundary values (surface elevations, velocities or tracer concentrations) may be read. Constant values, or custom routines returning boundary values may also optionally be specified.

Open boundaries may be defined anywhere in the grid, however, if a boundary is defined in the domain interior (as opposed to the limits of the domain) then the boundary must lie adjacent to an 'OUTSIDE' cell.

Open boundaries require that velocities normal and tangential to the open boundary, elevation and tracer concentrations are specified. Velocities are specified at the outer edge(s) of open boundary cells while elevation and tracers are specified at the cell centers. This formulation allows for a suite of BULK open boundary conditions to be implemented (radiation, extrapolation, relaxation conditions) and facilitates the implementation of higher order advection schemes. These open boundaries are generally called velocity boundaries below. More specifically, they are called `u1` boundaries if the left or right hand edge of the cell is open, or `u2` boundaries if the back or front edge of the cell is open.

When specifying open boundaries in the parameter file, it is first necessary to indicate how many open boundaries the model grid has:

```
# This grid has 3 open boundaries
NBOUNDARIES 3
```

Then, each boundary is described by a number of parameters of the form `BOUNDARY<M>.XXXX`, where `<M>` is the boundary index. The parameters specify the boundary type, name, boundary condition type used, cell indices, and forcing data.

A specified zone of wet cells may be changed to `OUTSIDE` cells by specifying:

```
BOUNDARY0.OUTSIDE_ZONE n      ! Set n wet cells into the
                               ! interior as OUTSIDE.
```

This must be performed using the both the `-g` and `-p` option. New boundary ranges are listed in the runlog file.

### 4.11.1 SHOC boundaries

The orientation of the `u1` or `u2` velocity boundaries must be known so that the normal and tangential velocity components may be identified in the **SHOC** code. Flagging a boundary as `u1` or `u2` requires the user to make this decision. Alternatively, a boundary may be classified as a `velocity` boundary in which case **SHOC** will decompose the boundary cell into `u1` and `u2` boundaries on left, right, front or back faces. The cell location provided in the `POINTS` list for `u1` and `u2` boundaries corresponds to the cell face. This means that the cell locations of `u1` boundaries on right faces and `u2` boundaries on front faces are incremented by one, in the `x` and `y` directions respectively, from the interior cell center adjacent to the boundary. If the boundary is specified as a `velocity` boundary, then the boundary cell location corresponds to the cell center.

Specification of a `u1` boundary is shown below.

```
BOUNDARY0.TYPE          u1
BOUNDARY0.NAME          Offshore boundary
BOUNDARY0.DATA          offshore.nc
```

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```
BOUNDARY0.BCOND_NOR      NOGRAD
BOUNDARY0.BCOND_TAN      CLAMPD
BOUNDARY0.BCOND_ELE      FILEIN
BOUNDARY0.BCOND_TRA_ALL  UPSTRM
BOUNDARY0.POINTS         3
4 7
4 8
4 9
```

Alternatively, if the `BOUNDARY.POINTS` are contiguous (e.g. not interrupted by land) then the `BOUNDARY.RANGE` specification may be used, e.g;

```
BOUNDARY0.RANGE      (4,7)-(4,9)
```

Generally this specification takes the form;

```
BOUNDARY0.RANGE      (is,js)-(ie,je)
```

where `is` and `js` are the start (i,j) coordinates and `ie` and `je` are the end (i,j) coordinates. Note that `is=ie` for `u1` boundaries, and `js=je` for `u2` boundaries. No white space is to be inserted in the syntax for this specification.

### 4.11.2 COMPAS boundaries

For unstructured meshes COMPAS does not discriminate directions in the mesh, and all open boundary `TYPE` should be `u1` boundaries. The exception is for structured grids, where the `type` should designate `u1` or `u2` boundaries, but all `CUSTOM` specifications should refer to `u1` as the normal component of velocity and `u2` the tangential component. For unstructured meshes, the shape of the polygon at the boundary may be such that for each boundary cell there are multiple edges associated with normal velocities, e.g. a hexagon may be associated with two or three normal velocity edges depending on its orientation. In contrast, a quadrilateral cell will always have only one normal velocity edge associated with any cell centre. This possibility of multiple edges must be accounted for in the unstructured boundary specification.

The explicit specification of unstructured OBC locations is:

```
BOUNDARY0.UPOINTS      n
v1 (i1,0 i1,1)
v2 (i2,0 i2,1)
.
.
vn (in,0 in,1)
```

Where  $v_n$  = cell index of the OBC cell

$i_{n,0}$  = mesh index of the start of the boundary edge

$i_{n,1}$  = mesh index of the end of the boundary edge

Alternatively, rather than specifying the mesh indices of the edge to use as the boundary, the geographic coordinates of the edge may be specified:

The explicit specification of unstructured OBC locations is:

```
BOUNDARY0.UPOINTS      n
v1 (lon1,0, lat1,0) - (lon1,1, lat1,1)
v2 (lon2,0, lat2,0) - (lon2,1, lat2,1)
.
.
v1 (lonn,0, latn,0) - (lonn,1, latn,1)
```

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where

$lon_{n,0}$  = longitude (or geographic coordinate) of the start of the boundary edge  
 $lat_{n,0}$  = latitude (or geographic coordinate) of the start of the boundary edge  
 $lon_{n,1}$  = longitude (or geographic coordinate) of the end of the boundary edge  
 $lat_{n,1}$  = latitude (or geographic coordinate) of the end of the boundary edge

The extraction of cell and mesh indices to define a boundary can be difficult without tools to assist in this process. A more flexible approach is to specify the geographic coordinates of the start, end and a mid-point of a boundary, then COMPAS will find all the cells between the start and end coordinates which also encompass the mid-point and convert internally to the required cell and mesh indices, e.g.

```
BOUNDARY0.START_LOC    lon1 lat1    # Start coordinates
BOUNDARY0.END_LOC      lon2 lat2    # End coordinates
BOUNDARY0.MID_LOC      lon3 lat3    # Mid-point coordinates
```

These coordinates should correspond to the cell centre of the boundary cells.

If the `START_LOC` is the same as the `END_LOC`, then the boundary only consists of one cell, and the `MID_LOC` is not required. The edges used for the boundary in this case are the edge(s) on the model perimeter. If the `START_LOC` and `END_LOC` are in adjacent cells, then the boundary consists of the edges on the perimeter sharing the common vertex between the cells, and again the `MID_LOC` is not required. The specification using the `MID_LOC` is only valid for open boundaries on the perimeter of the mesh.

### 4.11.3 Boundary condition types

The boundary conditions available are based on a variety of approaches and are listed in Table 3.2.9.1. The name and keyword used as input to **SHOC/COMPAS** are listed, along with a reference to the original study if this exists. The variables the condition may be applied to are also included, where  $un$  = normal velocity,  $Un$  = depth averaged normal velocity,  $ut$  = tangential velocity,  $\eta$  = surface elevation and  $T$  = tracers.

Implementation of the open boundaries requires that a boundary condition type is assigned to normal and tangential velocity components, elevation and tracers for each open boundary via the use of the following keywords:

```
BCOND_NOR              for normal velocity components
BCOND_TAN              for tangential velocity components
BCOND_ELE              for elevation
BCOND_TRAN             for tracers where  $0 \leq n < \text{number of tracers}$ , or
BCOND_<tr_name>       where <tr_name> is the name of the tracer.
                       e.g. BCOND_temp or BCOND_salt.
```

Different boundary conditions may be optionally set for the 2D components of velocity by defining the keywords:

```
BCOND_NOR2D for 2D normal velocity components
BCOND_TAN2D for 2D tangential velocity components
```

If these flags are absent then the 2D velocity components use the same open boundary condition as the 3D components specified by `BCOND_NOR` and `BCOND_TAN`.

The tracer boundary condition allows different conditions to be specified for each tracer. If all tracers are required to have the same boundary condition, the tracer flag used is:

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BCOND\_TRA\_ALL

If this condition precedes a condition for individual tracers, then all the tracers are set to BCOND\_TRA\_ALL except the individually specified tracers. This is useful if only a few tracers out of many need a specific boundary condition.

Table 3.2.9.1 : SHOC Open Boundary Conditions

Condition name	Keyword	Reference	Variable
Clamped	CLAMPD	-	un,ut,η,T
Data prescription from file	FILEIN	-	un,ut,η,T
Custom data prescription	CUSTOM	-	un,ut,η,T
Tidal synthesis	TIDEBC	Bye (1977)	η
Global tide model	TIDALH	Cartwright and Ray (1990)	η
Custom tide constituents	TIDALC	-	η
3D vertical integral for 2D	VERTIN	-	un,ut
No-gradient	NOGRAD	-	un,ut,η,T
Linear least squares	LINEXT	-	un,ut,η,T
2 <sup>nd</sup> order polynomial	POLEXT	-	un,ut,η,T
Cyclic	CYCLIC	-	un,ut,η,T
Linear calculation	LINEAR	-	un, ut
Gravity wave radiation	GRAVTY	Sommerfeld (1949)	un,ut,η
Orlanski	ORLANS	Orlanski (1976)	un,ut,η
Camerlengo and O'Brien	CAMOBR	Camerlengo & O'Brien (1980)	un,ut,η
Miller and Thorpe	MILLER	Miller and Thorpe (1981)	un,ut,η
Raymond and Kuo	RAYMND	Raymond and Kuo (1984)	un,ut,η
Flather	FLATHR	Flather (1976)	un
Upstream advection	UPSTRM	-	T
Tracer advection	TRCONC	-	T
Tracer flux	TRFLUX	-	T
Tracer flux using concentration	TRCONF	-	T
Statistical prescription	STATIS	-	T
Profile scaled to density	DEPROF	-	T
Idealised profile	PROFIL	-	T
Density gradient scaled	DESCAL	-	T
No condition imposed	NOTHIN	-	un,ut,η

**COMPAS only:** many radiation conditions implicitly assume that a wave approaching the open boundary does so in a direction normal to the open boundary (GRAVTY, ORLANS, CAMOBR, MILLER, FLATHR). For arbitrary unstructured polygons, this normal direction does not always exist, and values of state variables in a normal direction cannot be retrieved without some form of reconstruction. Therefore, while these radiation conditions will function in COMPAS, in practice there may be error associated with their solutions since some of the underlying assumptions are violated.

#### 4.11.4 Boundary Implementation (stagger)

The stencil for the open boundary stagger may use the outer face for normal velocity (the default, Fig. 4.1 Science Manual) or an inner stagger for normal velocity (Fig. 4.2 Science Manual). The outer stagger is generally more stable, and may use direct forcing (with or without relaxation to radiation conditions) for elevation forcing. The inner stagger must use a Flather condition if the model is to be forced with elevation. The stagger is imposed via:

```
BOUNDARY1.STAGGER      OUTFACE      # Outer stagger (default)
```

or

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```
BOUNDARY1.STAGGER      INFACE      # Inner stagger
```

If the STAGGER keyword is absent an outer stagger is assumed.

## 4.11.5 Forcing Data

The SHOC open boundary condition example given above describes a u1 boundary spanning 3 grid cells (i=4, j=7,8,9), where surface elevation values and tracer concentration values (if any) are found in the time series file `offshore.nc`. The surface elevation variable must be called `eta`, and the tracer variables must match the tracer names specified in the model parameter file (see section 4.10).

Unique among the input data forcing, the boundary DATA parameter supports the specification of multiple time-series data files. The files must all be defined on the same parameter line, and separated by white-space (spaces or tabs).

```
BOUNDARY1.DATA eta.ts salt.ts temp.ts
```

SHOC/COMPAS selects the first file that contains the requested variable and for which the current model time is within it's range. While overlap between files (in time) are permitted, care must be taken to ensure that there are no time gaps between files. The resulting extrapolation would be ill-defined. A path for all files included in the boundary specification (e.g. including custom velocity forcing files) for all boundaries may be specified using:

```
BDRY_PATH <file_path> # e.g. <file_path> = /home/disk/project/model/
```

## 4.11.6 Flather Radiation

The Flather condition is most successful when using an inner stagger; STAGGER = INFACE. A uniform bathymetry gradient across the boundary assists stability (BATHY\_CON = 1). This radiation condition requires data input for both normal depth averaged velocity and elevation. If depth averaged velocity and elevation are input as zero then the condition behaves in a passive manner. This scheme is invoked via:

```
BOUNDARY0.BCOND_NOR2D  FLATHR|<datain>
BOUNDARY0.BCOND_ELE    FLATHR|<datain>|<radiation>
```

Where <datain> is FILEIN if 2D velocity or elevation data is read from file, or CUSTOM if 2D velocity or elevation data is supplied by custom routines. <datain> = TIDALH or TIDALC may be used for elevation. For elevation, <datain> is the condition used to specify eta for the Flather OBC, and <radiation> may be any radiation condition, used to set the elevation OBC. A common specification is:

```
BOUNDARY0.BCOND_NOR2D  FLATHR|CUSTOM
BOUNDARY0.CUSTOM.ulav  uv_to_ulav 3D_velocity_data.nc
BOUNDARY0.BCOND_ELE    FLATHR|FILEIN|GRAVTY
BOUNDARY0.DATA         eta_data.nc
```

With additional conditions typically as:

```
BCOND_NOR      NOGRAD
BCOND_TAN      GRAVTY or NOGRAD
```

**SHOC only:** If normal depth averaged velocity and elevation data are unavailable, then a local solution (e.g. Palma and Matano (1998), p1340) may be used for velocity and elevation:

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```
BOUNDARY0.BCOND_NOR2D  FLATHR|LOCALN
BOUNDARY0.BCOND_ELE    FLATHR|LOCALE
BOUNDARY0.BCOND_TAN    LOCALT
```

This condition may be improved by using a radiation condition on elevation rather than the solution to the 1-dimensional continuity equation, e.g.

```
BOUNDARY0.BCOND_NOR2D  FLATHR|LOCALN
BOUNDARY0.BCOND_ELE    FLATHR|GRAVITY
BOUNDARY0.BCOND_TAN    LOCALT
```

If elevation data only is available, a linearized local solution may be used, retaining the elevation forcing; e.g.

```
BOUNDARY0.BCOND_NOR    LINEAR
BOUNDARY0.BCOND_NOR2D  FLATHR|LINEAR
BOUNDARY0.BCOND_ELE    FLATHR|FILEIN
BOUNDARY0.DATA         eta_data.nc
```

For SHOC/COMPAS, if the velocity and elevation data are required to be zero, then this may be accomplished by creating a file with zero values and using the `FILEIN` specification above, or using the `CLAMPD` condition:

```
BOUNDARY0.BCOND_NOR2D  FLATHR|CLAMPD
BOUNDARY0.BCOND_ELE    FLATHR|CLAMPD
```

In this case elevation will use a zero value in the Flather computation for normal velocity, and a zero value for the elevation condition. Generally, radiation conditions may be used to approximate the elevation and velocity data `<datain>`, e.g:

```
BOUNDARY0.BCOND_NOR2D  FLATHR|NOGRAD
BOUNDARY0.BCOND_ELE    FLATHR|MILLER
```

### 4.11.7 Custom Routines

Another mechanism for associating data with an open boundary is the `CUSTOM` parameter. A `CUSTOM` parameter may be defined for any variable by appending the variable name to the keyword with a fullstop (see below). Following the parameter, on the same line, are a sequence of space separated arguments. If the first argument is a numeric value or the string `default`, then the variable will be set to that fixed value on the boundary (default corresponding to the fill value for a tracer, or zero for `u1`, or `u2`). If the first argument is the name of a standard or custom function supported by the **SHOC/COMPAS** code, then the responsibility for evaluating the variable boundary value will be passed on to that function, along with the remaining arguments. These parameters are optional, and additional to the `DATA` parameter described above. If present, they override the `DATA` parameter for the variable concerned. For example:

```
# Set salinity to a constant value of 35.5 on this boundary
BOUNDARY0.CUSTOM.salt 35.5

# Set the tracer called contam to its default value
BOUNDARY0.CUSTOM.contam default

# Set surface elevation by calling the etabdry routine, and
# passing it the argument string "data.ts 280000 5700000"
BOUNDARY0.CUSTOM.eta etabdry data.ts 280000 5700000
```

For a given open boundary, it is not necessary to specify a `DATA` parameter if a `CUSTOM` parameter has been specified for every tracer and the appropriate dynamic variable (`u1`, or

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u2). The CUSTOM mechanism allows a high degree of flexibility in boundary specification, particularly when combined with custom subroutines.

### 4.11.8 River Flow Custom Routines

There exist several standard custom routines that allow a parabolic velocity profile to be imposed as the normal open boundary condition. This type of boundary forcing is designed to emulate a river inflow. Velocities decrease in a parabolic fashion from a maximum value at the surface to zero at a pre-defined depth such that the flow rate over the entire open boundary corresponds to a user specified rate (given in cumecs :  $\text{m}^3\text{s}^{-1}$ ). The syntax for this type of open boundary for a u1 boundary is as follows:

```
BOUNDARY0.BCOND_NOR      CUSTOM
BOUNDARY0.CUSTOM.u1      u1flowbdry
BOUNDARY0.U1_HC          -5.0
BOUNDARY0.U1_FLOW        <flowfile.ts> or flow_value
```

In this case a river flow boundary is set as the normal velocity condition on BOUNDARY0 and the parabolic profile exists from the surface to 5m depth. The flow rate can either be imposed in a time varying manner by specifying a time series file <flowfile.ts>, or can be set to a constant value by specifying the constant flow\_value. The flow rate should always be positive regardless of the orientation of the open boundary. Similarly, a river flow for a u2 boundary is specified via;

```
BOUNDARY0.BCOND_NOR      CUSTOM
BOUNDARY0.CUSTOM.u2      u2flowbdry
BOUNDARY0.U2_HC          -5.0
BOUNDARY0.U2_FLOW        <flowfile.ts> or flow_value
```

A simplified specification for rivers is input as follows:

```
BOUNDARY0.NAME      River1
BOUNDARY0.TYPE      u1
BOUNDARY0.BCOND0    RIVER flowfile.ts data_1.ts data_2.ts .... data_n.ts
```

where;

data\_<n>.ts = file containing temperature data (or other tracer data if the tracer OBC is active) at the cell centre. There must be at least one of these files listed.

flowfile.ts = file containing river flow.

In this case the depth over which the flow profile is distributed is the mean depth of the boundary, and salinity is input with a value of zero. If this is used a diagnostic tracer flow is generated which records the flow used in that river.

The halocline depth generally has to be set a priori, and is typically used as a tuneable parameter. This may not be desirable if many rivers exist. A dynamic pycnocline depth may be dynamically prescribed using:

```
BOUNDARY0.bcond_salt      TRCONC|CUSTOM
BOUNDARY0.CUSTOM.salt      0.0
BOUNDARY0.OPTIONS          DYNAMIC_HC NO_HDIFF
```

This can be further enhanced by computing the baroclinic landward flow in the salt wedge, and adjusting boundary 'ghost' cells using an upstream advection algorithm accordingly.

```
BOUNDARY0.OPTIONS          DYNAMIC_HC NO_HDIFF GEOSTR UPSTRM
```



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Note that the dynamic halocline depth is referenced to the free surface, and the absolute value will therefore change with the tide. Additional tracers are generated to report the depth the flow is distributed over (`flow_depth`) and the salinity of the flow (`flow_salt`).

If the salinity boundary condition is `TRCONC|CUSTOM` or `TRCONF|CUSTOM`, then a mass balance is performed to alter the salinity in the 'ghost' cell where;

$$\text{salinity} = [(\text{river salt mass}) + (\text{landward mass flux})] / [(\text{river flow}) + (\text{landward flow})]$$

If zero salinity is input to the river, then (`river salt mass`) is zero. This salt balance approximates mixing in a salt wedge estuary, where the up-estuary salt flux is entrained into the surface layer along the length of the salt wedge and mixed with the river outflow. For a tidally mixed estuary, an 'effective' river length can be specified, and the standing salt mass in the volume occupied by this river length is mixed with river inflow and landward salt wedge flow. A river length can be specified using:

```
BOUNDARY0.U1_LENGTH      10000.0
or
BOUNDARY0.U2_LENGTH      10000.0
```

Additional options are as follows:

`NO_SALT` : Do not adjust input 'ghost' cell salinity using the salt mass balance.

`FULL_DEPTH` : Use water depth rather than halocline to compute mean inflow velocity.

`FRESH_FLOW` : Surface density of 1000 is used in the internal wave speed calculation rather than actual surface density.

`TRUNC_LAYER` : Truncate halocline depth to next deepest layer.

`SCALE_MULT` : Use multiplicative scaling to inflow rather than additive scaling.

`YANKOVSKY` : Method of Yankovsky, A.E. (2000) The cyclonic turning and propagation of buoyant coastal discharge along the sheff. J. Mar. Res. 58, 585-607.

`NO_OUTFLOW` : River flow is delivered with the original unmodified parabolic profile.

`MACREADY` : Use the river mouth salinity approximation of MacCready and Geyer (2010) Annu. Rev. Mar. Sci., 2, 35-58, Eq. 19 and 16.

### 4.11.9 Forcing with Velocity

The standard custom routines may be used to force the open boundary with velocity profiles; e.g. saved from a coarser resolution simulation. Since this nesting approach usually uses large scale and fine scale grids having different orientation, any velocities saved on the coarse grid for nesting must first be rotated into east and north components (`u` & `v`). The point array (`parray`, Section 4.32.6) `netCDF` output option will automatically do this. These east and north velocity components must be saved on both normal and tangential open boundary faces on the fine scale grid. The latitude and longitude of these faces must be supplied in the `parray` specification, and may be retrieved from utilities such as `jvismeco` or `plum` (matlab package). Boundary location information may also be retrieved using the `WRITE_BDRY` function (Section 4.11.28). Once the normal and tangential (`u,v`) components are saved to file from the coarse scale grid, they may be re-read and rotated onto the fine scale boundaries using the custom routines, e.g. for a `u1` boundary;

```
BOUNDARY0.NAME           Offshore
BOUNDARY0.TYPE           u1
BOUNDARY0.BCOND_NOR     CUSTOM
BOUNDARY0.CUSTOM.u1     uv_to_u1  bdry_uv_nor.nc
BOUNDARY0.BCOND_TAN     CUSTOM
BOUNDARY0.CUSTOM.u2     uv_to_u2  bdry_uv_tan.nc
BOUNDARY0.ETA           NOTHIN
```

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Velocities from a standard netCDF file (see Section 4.32.6) may be rotated onto the grid using:

```
BOUNDARY0.CUSTOM.u1      hdstd_to_u1  bdry_std_nor.nc
```

**COMPAS only:** Since all boundaries are u1 boundaries in COMPAS, CUSTOM.u1 always refers to the normal boundary velocity and CUSTOM.u2 refers to tangential boundary velocity. If open boundary data is saved using the `sparse` format, then this may be read into the boundary arrays as a block (i.e. without spatial interpolation) using, e.g;

```
BOUNDARY0.OPTIONS      UGRID
BOUNDARY0.DATA          offshore.nc # for eta, T/S input
BOUNDARY0.CUSTOM.u1    ugrid_to_u1  offshore.mnc # velocity input
```

Additionally the frequency of update may be specified using, e.g;

```
BOUNDARY0.FILEIN_DT    2 minutes
```

Forcing with velocity is often prone to boundary over-specification issues which may lead to instability. These are harder to control than when forcing with elevation, where partially passive conditions may be used (see Section 4.11.8). Also, when using velocities interpolated from a coarse grid to a fine grid, there is no guarantee that the flux through the open boundary in the coarse and fine grid are identical (e.g. due to differences in bathymetry resolution, hence cross sectional area of the open boundary). This may lead to a gradual filling or emptying of the domain over time. To avoid this, the flux prescribed at the normal boundary face that is required to achieve a target elevation via the flux divergence may be inversely computed and added to the normal boundary velocity (see Herzfeld and Andrewartha, 2012 for details). In practice normal velocities are relaxed to this value over a timescale. This flux adjustment is invoked by specifying an elevation value in the `.DATA` boundary specification (e.g. derived from a coarse scale model) in conjunction with the `FILEIN` attribute, and the time-scale of the adjustment in the boundary list, e.g:

```
BOUNDARY0.ETA          NOTHIN|FILEIN
BOUNDARY0.ADJUST_FLUX  60 seconds
BOUNDARY0.DATA         data_ets.nc
```

A 'default' timescale may be specified by setting `ADJUST_FLUX < 0`; this default time-scale is given by (see Herzfeld and Andrewartha, 2012):

$$\tau_f = \frac{h}{\sqrt{gD_B}}$$

A dual time-scale may be implemented, where the tidal component is relaxed toward using a short time-scale, and the low frequency component using a longer time-scale (see Herzfeld and Gillibrand, 2015 for details). This is invoked using:

```
BOUNDARY0.ADJUST_FLUX  60 seconds # Long time-scale
BOUNDARY0.ADJUST_TIDE  2 seconds  # Short time-scale
```

Often the short time-scale is that of the barotropic time-step, and the long time-scale is the default time-scale.

The flux adjustment time-scale is relative to the 2D time-step, which is set by the fastest gravity wave in the domain, i.e. the deepest point in the domain. If this location is not on the open boundary, then the 'default' time-scale may become quite long relative to the 2D time-step, resulting in weak relaxation. Scaling can be applied to the flux-adjustment or dual adjustment time-scales so that the timescale becomes relative to the fastest gravity wave on the open boundary;

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```
BOUNDARY0.OPTIONS    SCALE_FA    # Scale the flux adjustment
BOUNDARY0.OPTIONS    SCALE_FAT   # Scale the dual flux adjustment
```

### COMPAS only

The flux adjustment timescale may be specified as a ratio applied to the 2D time-step, e.g:

```
BOUNDARY0.AJUST_RATIO 1.2
```

In this case the timescale is 1.2 x barotropic timestep, or  $(1.2 \times DT / IRATIO)$ . This is useful when time-steps are changed and the relative flux adjustment time-scale is desired to be retained.

The velocity forced boundary conditions may be specified in a simplified format;

```
BOUNDARY0.NAME      Offshore
BOUNDARY0.TYPE      u1
BOUNDARY0.BCOND0    NEST1WAY data_1.nc data_2.nc .... data_n.nc
                   bdry_uv_nor.nc bdry_uv_tan.nc
```

Where;

`data_<n>.nc` = file containing elevation, temperature and salinity data at the cell centre. Other tracer data is also required if the tracer OBC is active. There must be at least one of these files listed.

`bdry_uv_nor.nc` = file containing east and northward velocity components (u,v) at the normal velocity boundary face. This must be the second last file listed.

`bdry_uv_tan.nc` = file containing east and northward velocity components (u,v) at the tangential velocity boundary face. This must be the last file listed.

In this case the 'default' flux adjustment is used, and the boundary condition for temperature and salinity is `TRCONC` (Section 4.10.17). Any other tracers must be individually specified.

Versions prior to v1670 input the elevation via the `eta relaxation` file. This input method is backwards compatible using:

```
eta_relaxation_file    bdry_eta.nc
eta_relaxation_input_dt 20 minutes
COMPATIBLE             V1670
```

Note that the time scaling applied to the velocity increment is  $dt2d / dtr$ , where `dt2d` is the 2D time step, and `dtr` is the relaxation time-scale above. Therefore, if it is required that the flux be adjusted so that at every 3D time-step the boundary elevation becomes that in the `eta_relaxation_file`, then set `dtr = dt`, where here `dt` is the 3D time-step (note that the adjustment is done on the 2D time-step and  $dt = IRATIO \times dt2d$ ). If `FLUX_ADJUST` is specified in `RAMPVARS`, then the time scaling decreases from 1 year at the start of the ramp to the `ADJUST_FLUX` value at the end of the ramp. If `SCALE_ETA` is specified for the boundary, (Section 4.11.24) then the relaxation value is adjusted by the scale value before the inverse calculation. Note that if `FILEIN` is included in `RAMPVARS` and the initial condition for sea level is non-zero, then the sea level for flux adjustment will start from zero over the ramp which may cause instability. The `RAMPVARS` for this forcing is generally:

```
RAMPVARS    WIND CUSTOM TIDALH
```

Using forcing with velocity can lead to discontinuities in elevation (and tracers) on corners where there is boundary overlap, and elevation is solely determined by the forcing velocity data with no option for self-adjustment via interior velocities. In some cases this can lead to a constant drift in sea level, ultimately causing instability. Hard relaxation is imposed at these

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locations to attempt to mitigate this, however, if this fails then elevation and tracers may be over-ridden with a corner mean value using:

```
BOUNDARY0.OPTIONS          CORNER_MEANS
```

## 4.11.10 Tracer Equation OBCs

The standard custom routine `use_eqn` may be used to create an open boundary value for a particular tracer from an equation that has valid tracers as arguments, e.g;

```
BOUNDARY0.BCOND_NO3      CUSTOM
BOUNDARY0.CUSTOM.NO3     use_eqn '14.01*(neg(127.8562) - (0.8621*temp) +
(4.0403*salt))'
```

Where `neg` is the unary negative operator and `temp` and `salt` are valid model tracers. There is no binary operator precedence so parentheses must be used to enforce this, otherwise the equation is evaluated left to right. The current list of operators is:

```
*      Multiply
+      Addition
-      Subtraction
^      Power
exp    Exponential (unary)
neg    Negative (unary)
```

The unary operators must be enclosed by parenthesis (as in the above example) and spaces are allowed anywhere in the equation. Division is not supported as yet (use multiplication of the reciprocal). Any keywords in the equation that are not valid unary operators will be considered as a model tracer. An error will occur if any specified tracers are not found in the model.

## 4.11.11 Relaxation to Forced Data

Boundary data specified from a file may be combined with a radiation condition so that the transient response of the domain is transmitted through the boundary while allowing the boundary to respond to the prescribed forcing. This is accomplished by or-ing an active data forcing condition (`FILEIN` or `CUSTOM`) with a passive boundary condition. The time scale of relaxation is input via the keyword `RELAX_TIME`, and must be supplied for the following boundary conditions:

```
ORLANS | FILEIN
CAMOBR | FILEIN
MILLER | FILEIN
GRAVTY | FILEIN
NOGRAD | FILEIN
CLAMPD | FILEIN
LINEXT | FILEIN
POLEXT | FILEIN
```

Specifying `RELAX_TIME` assumes that incoming and outgoing waves are relaxed equally. Alternatively, relaxation may differ for incoming and outgoing waves by specifying:

```
BOUNDARY0.RELAX_IN      1 hour
BOUNDARY0.RELAX_OUT     30 days
```

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Long relaxation times are typically associated with outgoing waves so that the OBC behaves like a radiation condition, and short relaxation times are associated with incoming waves so that the OBC converges to the forcing data.

A boundary condition for relaxing surface elevation to observed data may appear as:

```
BOUNDARY0.TYPE u1
BOUNDARY0.NAME Offshore
BOUNDARY0.BCOND_NOR NOGRAD
BOUNDARY0.BCOND_TAN GRAVITY
BOUNDARY0.BCOND_ELE ORLANS|FILEIN
BOUNDARY0.RELAX_TIME 1 hour
BOUNDARY0.BCOND_TRA0 UPSTRM
BOUNDARY0.BCOND_TRA1 CLAMPD
BOUNDARY0.DATA offshore.nc
BOUNDARY0.RANGE (4,7) - (4,9)
```

### 4.11.12 Boundary Relaxation / Nudging

Elevation may be relaxed throughout a user defined zone with differing relaxation times on the inner and outer limits of the zone. Elevation relaxation is invoked via:

```
BOUNDARY0.RELAX_ELE r_width ts_b ts_i
```

where  $r\_width$  is the number of cells into the interior the relaxation zone extends,  $ts\_b$  is the relaxation time-scale on the boundary and  $ts\_i$  is the relaxation time-scale at the interior limit of the zone. It is permissible for  $ts\_b = ts\_i$ . The values of  $ts\_b$  and  $ts\_i$  are relative to the 2D time-step; i.e. the actual time-scale used for relaxation is  $ts\_b \times \Delta t_{2D}$  and  $ts\_i \times \Delta t_{2D}$ , where  $\Delta t_{2D}$  is the 2D time-step. For example, if the 2D time-step is 60 seconds, and the relaxation zone is defined as:

```
BOUNDARY0.RELAX_ELE 8 1 100
```

then a relaxation zone for elevation is created 8 cells into the interior, with a relaxation time-scale of 60 seconds on the boundary and 6000 seconds at the inner limit of the zone. Note that this option also requires an accompanying relaxation file to be specified, e.g.;

```
eta_relaxation_file bdry_eta.nc
eta_relaxation_input_dt 20 minutes
```

Temperature and salinity may be similarly nudged to data using:

```
BOUNDARY0.NUDGE_ZONE r_width ts_b ts_i
```

where  $r\_width$  is the width of the nudging zone in metres,  $ts\_b$  is the relaxation time-scale on the boundary and  $ts\_i$  is the relaxation time-scale at the interior limit of the zone. The values of  $ts\_b$  and  $ts\_i$  should have associated units; e.g.;

```
BOUNDARY0.NUDGE_ZONE 30000 1 day 5 day
```

Note that this option also requires an accompanying relaxation file to be specified in the tracer list for temperature and/or salinity:

```
TRACER1.relaxation_file temp_data.nc
TRACER1.relaxation_input_dt 3 hours
TRACER1.relaxation_time_constant obc
```

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Note that the `relaxation_time_constant` is specified as `obc` to designate boundary nudging.

## 4.11.13 Phase Speed Smoothing

The phase speed computed by the radiation schemes for elevation may be temporally smoothed using:

$$\tilde{c}^{t+1} = F\tilde{c}^t + (1-F)c^{t+1}$$

A typical value of  $F = 0.7$ . This smoothing assists in reducing numerical noise (e.g. MOM Users Guide). This smoothing is invoked using:

```
BOUNDARY0.SMOOTH_PHASE 0.7
```

## 4.11.14 Flow Relaxation Scheme

The flow relaxation scheme of Martinsen and Engedahl (1987) has been included to relax boundary data to interior data. This is accomplished over a region `NN` cells wide. The value of the prognostic values on the boundary ( $\eta$ ,  $u1$ ,  $u2$  or tracers) are given by any of the conditions outlined in Table 3.2.9.1; whatever is specified on the boundary is relaxed to the model-integrated values over `NN` cells. If the prognostic variable at the boundary is equal to zero then this flow relaxation scheme acts as a sponge type condition. This condition is invoked by adding the following flags for normal velocities, tangential velocities and elevation respectively, where `NN` is the number of cells the relaxation method is to act over (typically `NN=10`):

```
BOUNDARY0.RELAX_ZONE_NOR NN
BOUNDARY0.RELAX_ZONE_TAN NN
BOUNDARY0.RELAX_ZONE_ELE NN
```

For all tracers to have the same relaxation zone, include:

```
BOUNDARY0.RELAX_ZONE_ALL NN
```

For individual tracers use:

```
BOUNDARY0.RELAX_ZONE_TRAN n NN
BOUNDARY0.RELAX_ZONE_name n NN
```

where `n` is the tracer number and `name` is the tracer name.

## 4.11.15 Linear Conditions (SHOC only)

The advective and horizontal diffusive terms on the boundary may be omitted thus linearizing the boundary momentum balance. This is invoked via:

```
BOUNDARY0.BCOND_NOR LINEAR # Linear normal boundary velocity
BOUNDARY0.BCOND_TAN LINEAR # Linear tangential boundary velocity
```

For normal velocities on southern or western boundaries this is not particularly successful (see SHOC Science Manual, Section 4.5.6). A more successful linear strategy is to shift the stagger for normal velocities one cell into the interior and linearize the normal velocity at this location. This may be accomplished via:

```
BOUNDARY0.BCOND_NOR NOGRAD
```

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```
BOUNDARY0.LINEAR_ZONE_NOR      1
```

The linear zone make the momentum balance linear one cell into the interior of the model. This can be extended to any number of cells interior to the boundary, and may be applied to tangential components also;

```
BOUNDARY0.LINEAR_ZONE_NOR      n  # Linearize normal velocity n cells
                                # into the model interior. Typically
                                # n = 3.
BOUNDARY0.LINEAR_ZONE_TAN      n  # Linearize tangential velocity n
                                # cells into the model interior.
```

#### 4.11.16 **No Action Taken : NOTHIN**

The boundary condition `NOTHIN` will not alter the value of the prognostic value on the boundary. For example, if `BCOND_ELE = NOTHIN` the boundary value will assume that resulting from the solution to the continuity equation. This is useful if boundaries are forced with normal and tangential components of velocity, or the custom river OBC is imposed. The `NOTHIN` boundary condition may be combined with a radiation condition (e.g. `BCOND_ELE = NOTHIN|GRAVITY`), in which case the prognostic value on the boundary is relaxed to a radiation condition using the `RELAX_TIME` timescale. Alternatively, the prognostic value may be relaxed to data (`NOTHIN|FILEIN`) using the `RELAX_TIME` timescale.

#### 4.11.17 **Sponge Layers**

As a simple way of damping high frequency noise in the model (and sometimes to aid numerical stability), it is possible to apply a region of greatly increased horizontal viscosity just inside any type of open boundary. This is done by defining the parameter `NSPONGE_HORZ`, followed by the number of cells in from the boundary that the sponge will occupy.

##### SHOC only:

```
# Specifies that viscosity is greatly increased for 4 cells
# inside this open boundary.
BOUNDARY0.NSPONGE_HORZ 4
```

##### COMPAS only

```
# Specifies that viscosity is greatly increased for 20 km from
# the open boundary.
BOUNDARY0.NSPONGE_HORZ 20000
```

Within each sponge cell the horizontal viscosity is set near to the maximum numerically stable value for the particular grid and integration time step (default), or a multiple of the viscosity value at the boundary using, e.g;

```
# Set the maximum value of the sponge zone equal to 5 times the
boundary value.
BOUNDARY0.SPONGE_FACT      5
```

The alternate sponge formulation of Israeli and Orszag (1981) may be implemented where the coefficient of bottom friction is increased linearly to 4 times the interior value over a region `NN` cells wide. This sponge condition acts on 2D and 3D normal and tangential velocity components and is invoked by setting the following keyword for boundaries requiring a sponge:

```
BOUNDARY0.NSPONGE_VERT      NN
```

Where `NN` is the width of the sponge zone (typically `NN=10`).

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The sponges are applied to only the normal component of velocity. To generate sponge zones for normal and tangential components use;

```
BOUNDARY0.options          ISO_SPONGE
```

## 4.11.18 Atmospheric Pressure

If atmospheric pressure is specified as a model forcing input (see section 4.15), then, by default, elevation boundary conditions include an additional increment for the `eta` variable which is proportional to the difference between the specified pressure and a background ambient atmospheric pressure (the inverse barometer effect). This behaviour can be turned off for a particular boundary as follows:

```
# Turn of the inverse barometer boundary calculation.
# This is necessary where the specified eta values
# on the boundary already incorporate the effects of
# atmospheric pressure differences (nested grids can
# be an example of this).
BOUNDARY0.INVERSE_BAROMETER FALSE
or
BOUNDARY0.INV_BAR FALSE
```

## 4.11.19 Advection / flux conditions for tracers

A simple boundary condition for tracers is the upstream advection condition, `UPSTRM`. This condition is a 1-dimensional implementation of the upwind scheme discretized in advective form, and suffers the errors associated with this type of implementation, i.e. it is diffusive and non-conservative. Since the advective form only computes concentrations (as opposed to fluxes), it is uncertain as to what the actual flux of tracer entering the domain is when this condition is used. It is, however, easily implemented. The `UPSTRM` condition must be used in conjunction with another viable condition, e.g:

```
UPSTRM|CLAMPD
UPSTRM|NOGRAD
UPSTRM|LINEXT
UPSTRM|POLEXT
UPSTRM|CYCLIC
UPSTRM|FILEIN
UPSTRM|CUSTOM
```

In this case the value derived from the additional boundary condition is used in the upstream equation as the boundary value when flow is into the domain. The `UPSTRM|FILEIN` condition is used as the default if no additional boundary condition is specified (e.g. `BCOND_TRA_ALL=UPSTRM`), and this requires the user to supply a data file containing boundary values. Note that the `UPSTRM|CLAMPD` condition sets the boundary value to the water column fill value specified for that tracer when flow is into the domain.

The `UPSTRM` method effectively solves a one dimensional advection equation (Eqn. 4.8.1 Science Manual) and the location in the grid of the velocity used in this equation may influence the results depending on the type of forcing in effect. For example if low river flow is used as a boundary condition in conjunction with large tides in the model interior, then using a velocity located at one cell into the interior to the boundary in the `UPSTRM` condition will drag tracer into the domain whenever the tide flows in an outward direction from the boundary. The result is that too much tracer enters the model domain. If the velocity at the boundary cell is used then (river) velocity is always directed into the domain and the tracer in the boundary cell will converge to the data forced value, thus will not be influenced by flow into the cell from



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the model interior due to the tide. Again too much tracer enters the domain. Clearly neither of these scenarios are optimum and ideally a combination (adaptive method) of the two would yield the best result. The user has the ability to choose which velocity location is used in the equation to best suit the forcing conditions via:

```
UPSTRM_METHOD    FACE      # Use the face centered velocity at the
                  # boundary location.
                  INTERIOR # Use the velocity one cell into the
                  # interior of the boundary.
                  CENTER   # Use the mean of the boundary and
                  # interior velocities.
                  ADAPTIVE # Use the FACE velocity if the CENTER
                  # velocity is away (outward) from the
                  # boundary, and the INTERIOR velocity if
                  # the CENTER velocity is toward the
                  # boundary.
```

The default is INTERIOR.

A better method of implementing the tracer OBC is to use the advection scheme nominated by the user (e.g. VANLEER, QUICKEST etc; see Section 4.12) to solve the advection equation on the boundary. Using these higher order schemes ensures diffusion and dispersion errors are minimised, and since the flux form of the equation is solved the solution is conservative. This method is denoted TRCONC, and similar to the UPSTRM scheme, an additional boundary condition must be used to specify the value in this cell (see above). The default is TRCONC|FILEIN, where the user must supply a data file containing boundary values. If no data are available, passive conditions may be specified using e.g. TRCONC|NOGRAD. Note that conservation is only achieved, and reasonable values computed, if the volume is conserved in the boundary cell. This requires the velocity forced OBCs to be used (Section 4.10.7).

If the total flux of tracer entering the domain at the open boundary is precisely known, then this may be specified using the TRFLUX condition. Here the prescribed flux is used directly on the boundary face in the solution of the advection equation, and all other faces use the nominated advection scheme. The specified flux is uniformly distributed over all boundary cells. This approach may not be appropriate if the boundary cell becomes dominated by interior processes (i.e. the boundary cell must behave in a passive manner). Again an additional boundary condition must be used to specify the boundary flux and the default condition is TRFLUX|FILEIN, where the user must supply a data file containing boundary fluxes. Note that a positive specified flux implies tracer import, regardless of the edge the open boundary occupies.

If a concentration is known, then the flux and input method analogous to TRFLUX may be specified using TRCONF. In this case the supplied concentration is multiplied by the volume flux to get the tracer flux that is applied to the face. This may be useful for river inputs, if the river flow and inflow concentration of a tracer are known. The result will be identical to that using TRFLUX with the flux = concentration x flow, and is provided as an option for convenience.

The OVERWRITE option may be used with TRCONC, which will overwrite the data read from file into the boundary cell. This is equivalent to the FILEIN boundary condition, except that data is also written to the additional boundary ghost cells. This allows realistic values to be specified beyond the boundary for higher order advection schemes, rather than using a no-gradient condition which is effectively used when FILEIN is specified.

```
BOUNDARY0.OPTIONS    OVERWRITE
```

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## 4.11.20 Profile Methods for Tracers

The profile methods for tracers allow a depth dependent profile to be constructed given a surface and bottom measurement. The surface measurement may be spatially variable, and the bottom measurement should correspond to the deepest location on the boundary. The `DEPROF` method scales these measurements to the actual density profile predicted by the model a certain number of cells into the model interior (currently hardwired to 5 cells), whereas the `PROFIL` method constructs a synthetic profile consisting of surface mixed layer, pycnocline and bottom mixed layer. This synthetic profile is made by matching two exponential profiles at an inflection corresponding to the mixed layer depth. The `PROFIL` method therefore requires `MIX_LAYER = DENS_MIX` to be set so that a mixed layer depth is available. These methods are useful for forcing the model with surface and bottom data collected using moored instruments.

Both these methods require a netCDF file to be provided to SHOC/COMPAS containing the measured data. The data must be input at the exact geographic coordinates of the cell centers of the open boundaries. The surface measurements (which may vary spatially across the boundary) must be input at the surface (i.e. 0m) and the bottom measurement must be input at the layer in which the bottom is located for each cell comprising the boundary (i.e. the layer in which the bottom lies must be found for each cell and the same bottom measurement must be written to the netCDF file for that layer and geographic coordinates corresponding to that cell). This arrangement of the netCDF input file is necessary so that the profile method knows where to find surface and bottom measurements for each boundary cell. This means that netCDF files used for the profile methods are layer configuration and boundary location dependent (i.e. if the layer configuration or location of the boundary changes a new file must be created).

Profile methods are specified using:

```
BOUNDARY0.BCOND_TRA<n>  UPSTRM|FILEIN|PROFIL  # Synthetic profile for
# tracer <n>.
BOUNDARY0.BCOND_TRA<n>  UPSTRM|FILEIN|DEPROF  # Density profile for
# tracer <n>.
BOUNDARY0.DATA          input_file.nc        # netCDF input file
# containing measured
# data for tracer <n>.
```

Tracers may also be scaled to a normalized density profile that exists through the water column (i.e. at the deepest point in the domain). This ensures that the gradient of the tracer profile is some constant multiple of the density gradient, and therefore ensures that mixed layer depths are consistent between the tracer and density. This is invoked using:

```
BOUNDARY0.BCOND_<trname>      FILEIN|DESCAL
BOUNDARY0.SCALE_D.<trname>    v1 v2 <code>
```

Where `<trname>` is the name of the tracer, `v1` is the depth at which the tracer value is equal to that in `input_file.nc` at the same depth, and `v2` is a scaling factor for the profile (if `v2 < 0` the profile is inverted). Below depth `v1` the profile in any layer `k` is determined by adding `v2 x` (density gradient) to the concentration in the layer `k+1`. This is iteratively computed down through the water column. Above depth `v1` the profile in any layer `k` is determined by subtracting `v2 x` (density gradient) to the concentration in the layer `k-1`. This is iteratively computed up through the water column. If `<code> = c` then a copy of the values in `input_file.nc` is used for the profile below depth `v1`, and if `<code> = t` then the profile values are truncated to those in `input_file.nc` below the depth `v1` if the profile values become greater than those in `input_file.nc`.

## 4.11.21 Tidal Synthesis for Elevation

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The boundary condition `TIDEBC` will calculate the elevation on open boundaries from tidal constituent data supplied by the user. Data required are:

<code>T_CONSTITUENTS</code>	Number of tidal constituents to include
<code>T_NAME</code>	Name of the tidal constituent
<code>T_XLOCATION</code>	$i_c$ : the x location of the supplied tidal amplitude and period (m)
<code>T_YLOCATION</code>	$j_c$ : the y location of the supplied tidal amplitude and period (m)
<code>T_AMP</code>	$A$ : the tidal amplitude at location $(i_c, j_c)$ (m)
<code>T_PERIOD</code>	$P$ : the tidal period at location $(i_c, j_c)$ (hours)
<code>T_MOD_AMP</code>	$\alpha$ : the rate of modulation of tidal amplitude (cm/km)
<code>T_DIR_AMP</code>	$\theta$ : the direction towards which the tidal amplitude is progressing (i.e. direction of increasing $\alpha$ ) (degrees T)
<code>T_MOD_PSE</code>	$\beta$ : the rate of modulation of tidal phase (degrees/km)
<code>T_DIR_PSE</code>	$\phi$ : the direction towards which the tidal phase is progressing (i.e. direction of increasing $\beta$ ) (degrees T)

These data must be included for each tidal constituent on each boundary with the `TIDEBC` specification. An example of the domain forced with an M2 tide of amplitude 0.2m and an S1 tide of amplitude 0.1m is given below.

```
BOUNDARY0.T_CONSTITUENTS      2
BOUNDARY0.T_NAME              M2
BOUNDARY0.T_XLOCATION          641300
BOUNDARY0.T_YLOCATION          341707
BOUNDARY0.T_AMPLITUDE        0.2
BOUNDARY0.T_PERIOD            12.0
BOUNDARY0.T_MOD_AMP           0.0
BOUNDARY0.T_DIR_AMP           0.0
BOUNDARY0.T_MOD_PSE           0.0
BOUNDARY0.T_DIR_PSE           0.0

BOUNDARY0.T_NAME              S1
BOUNDARY0.T_XLOCATION          652000
BOUNDARY0.T_YLOCATION          341500
BOUNDARY0.T_AMPLITUDE        0.1
BOUNDARY0.T_PERIOD            24.0
BOUNDARY0.T_MOD_AMP           0.1
BOUNDARY0.T_DIR_AMP           350.0
BOUNDARY0.T_MOD_PSE           0.17
BOUNDARY0.T_DIR_PSE           55.0
```

### 4.11.22 Global Tidal Model

The global tide model of Cartwright and Ray (1990) may be applied to the open boundaries using:

```
BOUNDARY0.BCOND_ELE          TIDALH
```

This condition is described in Section 4.11 of the Science Manual. The tide may be directly imposed on the boundary as above, or may be superimposed on some low frequency sea level signal using:

```
BOUNDARY0.BCOND_ELE          FILEIN|TIDALH
BOUNDARY0.DATA                low_frequency.nc # netCDF file containing
                                     # low frequency sea level
                                     # data.
```

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The global tide model requires paths to the orthotide functions and nodal corrections to be present, e.g:

```
TIDE_CSR_CON_DIR      /tide/nodal      # Path to nodal
                        # correction directory.
TIDE_CSR_ORTHOWEIGHTS /tide/ortho_csr_4.0 # Orthotide functions.
```

## 4.11.23 Custom Tidal Constituents

Tidal constituents' amplitude and phase may be specified via file input. This allows the model to be boundary forced with spatially variable tidal phases and amplitudes of the user's choice. File formats may be netCDF for spatially variable, or ascii time series for non-spatially variable constituents. The custom tidal constituent prescription is specified using, e.g.:

```
BOUNDARY0.BCOND_ELE      TIDALC
BOUNDARY0.T_CONSTITUENTS M2 S2 K1 O1 # List of constituents
```

The TIDALC boundary condition may be used for elevation, normal and tangential 2D or 3D velocity.

The tide may be directly imposed on the boundary as above, or may be superimposed on some low frequency sea level signal using:

```
BOUNDARY0.BCOND_ELE      FILEIN|TIDALC
BOUNDARY0.T_CONSTITUENTS M2 S2 K1 O1 # List of constituents
BOUNDARY0.DATA           low_frequency.nc # netCDF file containing
                        # low frequency sea level
                        # data.
```

The global tide model requires paths to the file specifying constituent phases and amplitudes and the nodal correction directory to be present, e.g:

```
TIDE_CSR_CON_DIR      /tide/nodal      # Path to nodal
                        # correction directory.
TIDE_CONSTITUENTS     tide.nc          # Constituent file.
```

If this custom tide file contains velocity information (units  $\text{ms}^{-1}$ ), then velocity forcing may be applied on open boundaries. If transport information (velocity x depth; units  $\text{m}^2\text{s}^{-1}$ ) is contained in the file, this is first divided by local bathymetry before use. Compas will infer if the file contains velocity or transport by interrogating the units in the netCDF file. Alternatively, these may be explicitly specified via:

```
TIDE_CONSTITUENTS_VEL      tide.c # Velocity tidal constituents
TIDE_CONSTITUENTS_TRAN     tran.c # Transport tide constituents
```

### COMPAS only

Multiple tide files may be specified; where a model domain falls outside the bounds of the first supplied file, the second file is used. An option interpolation rule may be optionally supplied, e.g;

```
TIDE_CONSTITUENTS     tide1.nc tide2.nc i_rule
```

The optional interpolation rule, `i_rule`, may be `nearest`, `linear`, `cubic`, `nn_sibson`, `nn_non_sibson` or `quadratic`.

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The tidal velocity may be applied to 2D or 3D velocity; the 2D approach is more efficient. To prescribe tidal velocity forcing use:

```
BOUNDARY0.BCOND_NOR2D  VERTIN|TIDALC
BOUNDARY0.BCOND_TAN2D  VERTIN|TIDALC
```

If any of the constituents listed in the `BOUNDARY0.T_CONSTITUENTS` list cannot be found in the `TIDE_CONSTITUENTS` file, SHOC/COMPAS will terminate with an error. The list of constituents should be a subset of the following: if a constituent is not found in this subset it will be omitted from the forcing with an accompanying error.

Constituent Name	Doodson Number
long period	
LP	55.565
Sa	56.554
Ssa	57.555
TERa	58.554
Mm	65.455
Mf	75.555
TERm	85.455
93a	93.555
diurnal	
2Q1	125.755
Q1	135.655
O1	145.555
M1	155.655
P1	163.555
S1	164.556
K1	165.555
PHI1	167.555
J1	175.455
OO1	185.555
NU1	195.455
semi-diurnal	
227	227.655
2N2	235.755
MU2	237.555
N2	245.655
NU2	247.455
M2	255.555
L2	265.455
T2	272.556
S2	273.555
K2	275.555
285	285.455

Each constituent in the constituent file must be represented by an amplitude in 'metre' with '`_amp`' appended to the constituent name from the table above, and a phase in 'degrees' with '`_phase`' appended to the constituent name. For tidal velocities, the amplitude units must be `ms-1` and `_amp_u` and `amp_v` (or `phase_u` and `phase_v`) must be appended to constituent names for `u` (eastward) and `v` (northward) tidal velocities respectively. A time stamp must also exist in the file for compatibility with the time-series file reading libraries, although this time value may be anything since it is not used in computations (however, this does allow time dependent amplitudes and phases if required). However, the amplitudes and phases must be relative to the local time zone, not GMT. Note that the spatial extent of the

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tidal netCDF file must completely encompass the region defined by all cell centres of the model grid. An example of a netCDF header for the M2 constituent is given below:

```
netcdf tide {
dimensions:
    t = UNLIMITED ; // (1 currently)
    i_centre = 20 ;
    j_centre = 20 ;
variables:
    double t(t) ;
        t:units = "seconds since 2000-01-01 00:00:00 +08" ;
        t:coordinate_type = "time" ;
    double x_centre(j_centre, i_centre) ;
        x_centre:long_name = "Longitude at cell centre" ;
        x_centre:coordinate_type = "longitude" ;
        x_centre:units = "degrees_east" ;
        x_centre:projection = "geographic" ;
    double y_centre(j_centre, i_centre) ;
        y_centre:long_name = "Latitude at cell centre" ;
        y_centre:coordinate_type = "latitude" ;
        y_centre:units = "degrees_north" ;
        y_centre:projection = "geographic" ;

}
```

## 4.11.24 *Mixing coefficient boundary conditions*

Open boundary conditions can be imposed on the vertical mixing coefficients  $V_z$  and  $K_z$ . The same boundary conditions applicable to tracers may also be applied to  $V_z$  and  $K_z$  with the exception of `FILEIN` and `CUSTOM`. If the boundary condition type for mixing coefficients is unspecified then the default condition of `NOTHING` is imposed, which assigns the mixing values on the open boundaries via selected mixing scheme computations. Since these computations usually involve vertical velocity shear and density gradients on the open boundary, all of which use values derived from other open boundary conditions, it is possible that error is introduced into vertical mixing coefficients on the open boundary in this case. The velocity computations interior to the open boundary use the vertical viscosity on the open boundary hence it is possible for this error to propagate into the domain. Under these circumstances it is preferable to specify the mixing coefficients on the boundary via an open boundary condition.

## 4.11.25 *Split conditions for tracers*

A `NOGRAD` boundary condition may be applied above a certain depth for tracers and a `FILEIN` or `CUSTOM` condition below this depth. This is invoked by setting:

```
BOUNDARY0.BCOND_TRA<n>          FILEIN|NOGRAD   (or CUSTOM|NOGRAD)
BOUNDARY0.TRPC_TRA<n>           -50
```

Where `<n>` is the tracer number and in this case the depth above which the `NOGRAD` condition is applied is 50m. The depths should always be entered as a negative number.

## 4.11.26 *Constant boundary bathymetry*

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Bathymetry may be specified as constant adjacent to an open boundary via;

```
BOUNDARY0.BATHY_CON    n # Specify bathymetry constant for n cells
                        # into the model interior.
```

This is performed by finding the bathymetry n cells into the interior and setting the bathymetry at all cells between the boundary and this n<sup>th</sup> cell equal to this n<sup>th</sup> cell bathymetry value. Note that the input file must be re-created when the bathymetry is altered using this option.

Additionally, the boundary zone may be smoothed using:

```
BOUNDARY0.BATHY_SMOOTH  n # Specify bathymetry smoothing for n cells
                        # into the model interior.
```

## 4.11.27 Scaling

The values of the tracer values computed on the boundaries may be scaled by adding a constant or multiplying by a constant. Elevation values on the boundary may be scaled by adding a constant. This is useful for easily manipulating input data without creating a new input forcing file, for example when scaling is required to convert to the correct units for tracer input. The scaling may be either a constant specified value, or may be scaled by the value of a tracer existing in the tracer list. In the latter case the scaling may be temporally and spatially variable. To scale by a constant use:

```
# Add the value of one to the boundary value of eta
BOUNDARY0.SCALE_ETA    1
```

Multiplicative scaling on eta can be invoked using `'*' , e.g, multiply by 1.5;`

```
BOUNDARY0.SCALE_ETA    * 1.5
```

```
# Add the value of one to the boundary value of tracer with name <trname>
```

```
BOUNDARY0.SCALE_S.<trname>    1
```

```
# Multiply the boundary value of tracer with name <trname> by 0.9
```

```
BOUNDARY0.SCALE_P.<trname>    0.9
```

For example, to add 1°C to the temperature boundary value, use:

```
BOUNDARY0.SCALE_S.temp    1
```

A tracer may be set up where its value is updated using the `reset` function (Section 4.10.2). The tracer should not be advected, diffused and should not be a diagnostic. This tracers value will therefore be updated with data from a specified file at a specified time interval. The values of this tracer on the open boundary can then be used to scale elevation or a different tracer's boundary values. First define the scaling tracer in the tracer list, e.g;

```
TRACER2.name           scale_p
TRACER2.long_name      Scaling tracer product
TRACER2.units          fraction
TRACER2.fill_value     0.0
TRACER2.valid_range    0 10
TRACER2.advect         0
TRACER2.diffuse        0
TRACER2.diagn          0
TRACER2.reset_file     scale.nc
TRACER2.reset_dt       1 hour
```

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The values of this tracer will assume spatially interpolated values from the file 'scale.nc' at 1 hour intervals. The `reset_file` may be a netCDF or time-series file. Next, define different tracers to be scaled on each boundary by referencing to this tracer:

```
# Add the boundary values in tracer scale_p to the boundary value of eta (note the tracer
should have type = WC2D for elevation),
BOUNDARY0.SCALE_ETA          scale_p
```

```
# Add the boundary values in tracer scale_p to the boundary value of tracer with name
# <trname>.
BOUNDARY0.SCALE_S.<trname>   scale_p
```

```
# Multiply the boundary value of tracer with name <trname> by the boundary values in tracer
# scale_p,
BOUNDARY0.SCALE_P.<trname>   scale_p
```

For example, to add the boundary values in `scale_p` to the temperature boundary value, use:

```
BOUNDARY0.SCALE_S.temp       scale_p
```

## 4.11.28 *Boundary geographic location*

The latitude and longitude of the cell and face centres may be output to file using:

```
WRITE_BDRY          <bdry_file>
```

where `<bdry_file>` is the name of the file the information is written to. This file will contain the latitude and longitude of cell centres (for tracer / elevation), normal velocity face centres and tangential velocity face centres for every boundary present. The information is written in the point array output file format (Section 4.32.6), and may be directly pasted into a parameter file when outputting point array data for nested grids. The `WRITE_BDRY` option will only function when running the model under the `-p` or `-g` options.

## 4.11.29 *Standard boundary conditions*

A simplified format may be used to specify certain open boundary conditions. A list of these standard boundaries may be specified (currently the list size is 2) where boundaries may be re-configured to any in the list using run regulation (Section 4.31.1). The standard boundaries are specified using:

```
BCOND<n> type <data_1>....<data_n>
```

Where `n` is the list number (0 to 1), `type` is the `type` of the condition and `<data>` is a list of data required for the type. The `type` may be:

1. 1-way nesting (Section 4.10.7):

```
BOUNDARY0.BCOND0  NEST1WAY data_1.nc data_2.nc .... data_n.nc
bdry_uv_nor.nc bdry_uv_tan.nc
```

where `data_<n>.nc` = file containing elevation, temperature and salinity data at the cell centre. Other tracer data is also required if the tracer OBC is active. There must be at least one of these files listed.

`bdry_uv_nor.nc` = file containing east and northward velocity components (u,v) at the normal velocity boundary face.



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`bdry_uv_tan.nc` = file containing east and northward velocity components (u,v) at the tangential velocity boundary face.

In this case the 'default' flux adjustment is used, and the boundary condition for temperature and salinity is `TRCONC` (Section 4.10.17). Any other tracers must be individually specified.

## 2. 2-way nesting:

```
BOUNDARY0.BCOND0 NEST2WAY data_1.mpk data_2.mpk .... data_n.mpk
                    bdry_uv_nor.mpk bdry_uv_tan.mpk
```

where the format is the same as for 1-way nesting, except forcing files are memory packets.

## 3. Clamped nesting:

```
BOUNDARY0.BCOND0 NEST_CPD data_ets.mpk data_uv_nor.mpk
                    data_uv_tan.mpk
```

3D velocities are clamped, gravity wave radiation on sea level.

## 4. River boundaries (Section 4.10.6):

```
BOUNDARY0.BCOND0 RIVER flowfile.ts data_1.ts data_2.ts .... data_n.ts
```

Where `data_<n>.ts` = file containing temperature at the cell centre. Other tracer data is also required if the tracer OBC is active. There must be at least one of these files listed.

`flowfile.ts` = file containing river flow.

In this case the depth over which the flow profile is distributed is the mean depth of the boundary, and salinity is input with a value of zero.

## 5. No action taken:

```
BOUNDARY0.BCOND0 NOTHIN
```

Velocity, tracer and sea level open boundaries are set to `NOTHIN` (Section 4.10.14).

## 6. Emulate a solid wall:

```
BOUNDARY0.BCOND0 SOLID
```

This OBC is the same as No action taken, except normal velocities are clamped to zero such that a zero flux condition exists.

## 7. Flather radiation:

This OBC sets up a Flather radiation open boundary condition, and is invoked using:

```
BOUNDARY0.BCOND0 NEST_FLAT ts.nc eta.nc uvav_nor.nc uvav_tan.nc
```

Where `ts.nc` is a file containing temperature and salinity data, `eta.nc` is a file containing sea level data, `uvav_nor.nc` is a file containing normal depth averaged velocity data and `uvav_tan.nc` is a file containing tangential depth averaged velocity data. The Flather OBC conforms to the following specification:

```
BOUNDARY0.BCOND_ELE    FLATHR|FILEIN|GRAVTY
BOUNDARY0.BCOND_NOR    NOGRAD
BOUNDARY0.BCOND_NOR2D  FLATHR|CUSTOM
BOUNDARY0.BCOND_TAN    GRAVTY
BOUNDARY0.salt         FILEIN
BOUNDARY0.temp         FILEIN
```

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```
BOUNDARY0.STAGGER      INFACE
BOUNDARY0.custom.ulav  uvav_to_ulav  uvav_nor.nc # or .u2
BOUNDARY0.DATA         ts.nc eta.nc
```

A standard open boundary configuration may appear as:

```
BOUNDARY0.NAME      Offshore
BOUNDARY0.TYPE      u1
BOUNDARY0.BCOND0    NEST1WAY data_1.nc bdry_uv_nor.nc bdry_uv_tan.nc
BOUNDARY0.BCOND1    RIVER flowfile.ts data.ts
```

Any additional boundary specification (e.g. `INVERSE_BAROMETER`, `NSPONGE_HORZ`) is also applied to the standard boundary.

### 4.12 Advection Schemes

The specification of the advection scheme for tracers is set via the flag `TRA_SCHEME` in the parameter file. Current options are:

```
ORDER1              # 1st order upwind flux form
VANLEER             # Van Leer's scheme
ORDER2              # 2nd order flux form
ORDER2_UW           # 2nd order upwind flux form (stable for Courant < 2)
ORDER4              # 4th order flux form
QUICKEST            # QUICKEST, flux form, variable grid
QUICKEST_AD         # QUICKEST scheme, advective form
QUICKEST_CO         # QUICKEST, flux form, constant grid formulation
LAGRANGE            # Semi-Lagrange scheme
COMPAS only
ORDER3US            # 3rd order unstructured flux form (nonconservative)
ORDER4US            # 4th order unstructured flux form (nonconservative)
FCT|ORDER2          # 2nd order flux corrected transport (conservative)
FCT|ORDER3US        # 3rd order flux corrected transport (conservative)
FCT|ORDER4US        # 4th order flux corrected transport (conservative)
QUICKEST|US         # Unstructured QUICKEST
VANLEER|US          # Unstructured Van Leer
FFSL                # Flux form semi-Lagrange (see Section 9.4)
```

For details of these advection schemes see section 5, Herzfeld (2002).

The `ULTIMATE` limiter (Leonard, 1991) is invoked on the chosen scheme by setting the flag `UTLIMATE` in the parameter file. This limiter eliminates non-monotonic behaviour in the

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solutions and is generally only successful on the higher order advection schemes (i.e. 2<sup>nd</sup>, 4<sup>th</sup> order and QUICKEST). The ULTIMATE limiter is not invoked by default.

e.g.

```
ULTIMATE      YES    # invoke the ultimate limiter
ULTIMATE      NO     # no ultimate limiting
```

A choice of advection scheme is also available for momentum. This is set via the flag MOM\_SCHEME in the parameter file and the current options are:

### SHOC only:

```
ORDER1      # 1st order upwind scheme
ORDER2      # 2nd order scheme
VANLEER     # Van Leer's scheme
ANGULAR     # 2nd order flux form angular scheme for momentum
ANGULAR3D   # As for ANGULAR but applied to 3D momentum only
LAGRANGE    # Semi-Lagrange scheme
```

### COMPAS only

```
VECINVAR    # Vector invariant scheme. Note; an equivalent legacy
             # keyword of RINGLER was used in some older COMPAS
             # versions (pre v1.0 rev(5996)).
```

Several additional options may be appended to the MOM\_SCHEME definition:

```
WIMPLICIT   # Implicit vertical advection
```

### SHOC only:

```
ADVECT_FORM # Horizontal advection solved in the advection form
WTOP_O2     # 2nd order approximation for surface vertical velocity
WTOP_O4     # 4th order approximation for surface vertical velocity
ZERO_DRYK   # Velocity=0 for horizontal terms above free surface
SHAPIRO     # Use 1st order Shapiro filter on advection tendencies
```

The default approximation for surface vertical velocity is 4<sup>th</sup> order. Velocities used in the horizontal fluxes are set to zero above the free surface using ZERO\_DRYK, then set to a no-gradient for the vertical fluxes. The default is a no-gradient condition for horizontal and vertical fluxes. An example using these options may be:

```
MOM_SCHEME      ORDER2 ADVECT_FORM ZERO_DRYK
```

**COMPAS only:** In COMPAS the vertical momentum advection is always performed implicitly. Also, only 2<sup>nd</sup> order approximations are available for the surface vertical velocity. The default specification for momentum advection in COMPAS is therefore:

```
MOM_SCHEME      VECINVAR WTOP_O2 WIMPLICIT
```

The potential vorticity flux used in the nonlinear Coriolis term takes a default implementation of the energetically-neutral form (Eq. 49 Ringler et al., 2010), but the potential enstrophy conserving (Eq. 71 Ringler et al., 2010) or enstrophy dissipating (Eq. 73 Ringler et al., 2010) or anticipated potential vorticity method (Eq. 81 Ringler et al., 2010) form may also be invoked;

```
MOM_SCHEME VECINVAR WTOP_O2 WIMPLICIT NEUTRAL # Energy neutral
MOM_SCHEME VECINVAR WTOP_O2 WIMPLICIT CONSERVE # Enstrophy conserve
MOM_SCHEME VECINVAR WTOP_O2 WIMPLICIT DISSIPATE # Enstrophy dissipate
MOM_SCHEME VECINVAR WTOP_O2 WIMPLICIT APVM    # Anticipated
                                                # potential vorticity
                                                # method.
```

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Several methods exist to control spurious Rossby modes evident in COMPAS meshes (Weller, 2012). These methods use upwind techniques when interpolating potential vorticity from vertices to edge centres, and are included in the `MOM_SCHEME` specification (see above):

```
APVM      # Anticipated potential vorticity method
LUST      # Linear upwind stabilized transport
CLUST     # Continuous linear upwind stabilized transport
```

The kinetic energy formulations of Skamarock et al. (2012), Eq. 11-13 and Gassmann (2013), Appendix B are available. These formulations are designed to remove the Hollingsworth instability seen in meteorological models using TRiSK. The formulation of Yu et al. (2020) Section 4b, Eq. 12 is also available, which is reported to improve accuracy.

```
KINETIC    GASSMANN    # Gassman (2013) formulation
KINETIC    YU          # Yu (2020) formulation
```

## SHOC only:

The semi-Lagrangian scheme can be used with 1<sup>st</sup> to 4<sup>th</sup> order interpolations using:

```
ORDER_SL    n          # Order of scheme; n = 1, 2, 3 or 4.
```

The default is first order using a tri-linear interpolation. The scheme is also unconditionally stable and can therefore be used with any time-step. However, this scheme is only suitable to use with multiple windows if the CFL condition is satisfied (in practice the stencil of the higher order schemes ( $n > 1$ ) mean that insufficient partition transfers are available to provide an accurate solution). Therefore, these semi-Lagrangian approaches should only be safely used with `WINDOWS=1`. Using these schemes allows the possibility to operate the tracers on a longer time-step than momentum, which is achieved by setting the flag;

```
TRATIO      n
```

where `n` is the multiple of the 3D time-step the tracers are to operate on, e.g. if `n=4` and `dt=50` seconds then the tracers are updated every fourth 3D time step (every 200 seconds). Note that the Semi-Lagrangian scheme has conservation and numerical diffusion characteristics inferior to some of the other schemes available (semi-Lagrange characteristics improve with increasing Courant number), but if many tracers exist and speed is a priority, then this scheme may be attractive. Note that the effective upper limit of `TRATIO` may be determined by other events in the time scheduler's control. For this reason ideally the `TRATIO` time-step must be less than any other time IO interval used for output dumps, output timeseries or forcing data input.

## COMPAS only:

Using `TRATIO > 1` in conjunction with the `FFSL` advection scheme requires volume transports to be averaged over the longer time-step by using:

```
MEAN        TRANSPORT
```

Note that this precludes the use of the `MEAN` diagnostic with alternative values of `MEAN_DT`.

In transport mode, `TRATIO` may be  $0 < \text{TRATIO} < 1$ . This effectively reduces the time-step used with the transport model, and may be useful using the `FFSL` scheme if the `DT` time-step violates the stability criterion (Lipschitz stability – i.e. streamlines cannot cross). In this case a constant flux and linear elevation change is assumed over the interval `DT`, and at each substep `TRATIO × DT` the velocity profile is reconstructed according to these assumptions.

Due to the undesirable characteristics of the `LAGRANGE` scheme, it is possible to advect tracers temp and sal with a higher order scheme (`VANLEER`) and all remaining tracers with `LAGRANGE` using:

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```
TRA_SCHEME          LAGRANGE|VANLEER  # T/S = VANLEER,  
                    # other tracers = LAGRANGE
```

The `TRATIO` facility may be used in conjunction with these split schemes.

## COMPAS only:

A Runge-Kutta higher order time discretization has been included for tracers Shu and Osher (1998). Various schemes are also described in Gottlieb (2005). The 5 stage method is that of Spiteri and Ruuth (2002). This is specified via:

```
RUNGE_KUTTA        1      # 1 stage 1st order Euler forward integration  
RUNGE_KUTTA        2      # 2 stage 2nd order integration  
RUNGE_KUTTA        3      # 3 stage 3rd order integration  
RUNGE_KUTTA        5      # 5 stage 4th order integration
```

The default is `RUNGE_KUTTA=1`. Note that there is a computational cost if `RUNGE_KUTTA>1`.

## 4.13 Surface elevation and velocity

The initial condition for the surface elevation may be specified by input from file (netCDF or timeseries) or by direct input in the parameter file. The latter consists of specifying an `NCE1*NCE2` floating point array, so that it is possible to set a different value in every grid cell. However, for most applications where the grid geographical extent is not large, a uniform value can be used. Examples of surface initialisation are given below:

```
SURFACE            surface.nc  # Input eta from netCDF or timeseries file.
```

## COMPAS only

If an interpolation rule is appended to the netCDF file, then an unstructured interpolation is used (linear, cubic, `nn_sibson`, `nn_non_sibson`; see Section 4.9).

```
SURFACE            surface.nc nn_sibson  # netCDF interpolation using  
                                         # nn_sibson.
```

For SHOC/COMPAS elevation may be set uniformly over the entire grid:

```
SURFACE            2000          # Elevation set uniformly to 1m for a  
1.0                # hypothetical domain of size 40*50.
```

**SHOC only:** input may also be in  $(i, j)$  array format:

```
SURFACE            4              # Elevation set at each cell for a domain of  
0.1 0.2            # size 2*2.  
0.2 0.3
```

The surface elevation may be explicitly overwritten at a number of arbitrary cells using the `SURFACE_POINTS` list. This option is useful for quickly initialising barotropic relaxation experiments (e.g. tsunami modelling). The format is as follows:

## SHOC only

```
SURFACE_POINTS n          # n = number of points in the list  
i1 j1 val1            # (i,j) location and value for point 1  
i2 j2 val2            # (i,j) location and value for point 2  
.  
.  
in jn valn
```

## COMPAS only

```
SURFACE_POINTS n          # n = number of points in the list
```

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```
cc1 val1          # index location and value for point 1
cc2 val2          # index location and value for point 2
.
.
ccn valn
```

If file input is used for surface initialisation and this file doesn't contain an elevation dump at the time corresponding to the model start time, then linear interpolation of elevation to the start time is performed. Surface elevation initialisation using the above methods generates a surface field that is written to the input netCDF file, hence if any changes are made to the surface initialisation then a new input netCDF file must be generated using the `-g` option (see section 8). Changes to surface initialisation have no effect when running the model using the `-p` option.

Often sea level is initialised from output of a global general circulation model, and often these models do not include atmospheric pressure forcing (i.e. the inverse barometer effect). Both SHOC and COMPAS include this effect, and to impose an inverse barometer effect on the initial condition the following can be used:

```
SURFACE_INV_BAR      YES
```

Similarly, the surface velocity initial condition may be specified using:

```
VELOCITY      velocity.nc  # Input velocity from netCDF file.
```

The initial velocity field can be set to the geostrophic flow using:

```
VELOCITY      GEOSTROPHIC
```

### 4.13.1 Elevation (and velocity) relaxation

Surface elevation may be relaxed to a surface field supplied via a time series or netCDF file using:

```
eta_relaxation_file      infile.nc #  $\eta$  field to relax towards
eta_relaxation_input_dt  1 hour    # Time interval elevation is
                                # read from file.
eta_relaxation_time_constant # elevation relaxation time
                                # constant.
```

The elevation to relax towards is read from the file `infile.nc` at the time interval `eta_relaxation_input_dt`. Every 2D time-step the actual elevation is relaxed towards this value using a relaxation time constant of `eta_relaxation_time_constant`. The relaxation time constant is the time it takes for the elevation to converge to the elevation field in `infile.nc`, i.e. if the time constant is equivalent to the 2D time-step then elevation is reset to that found in `infile.nc` every 2D step.

If the `eta_relaxation_time_constant` is the name of a file (netCDF or ascii) then the units for the time constant in the file must be a date unit, e.g.

```
# Ascii relaxation file where relaxation is 48 hours at day 0 and 2
# hours at day 10. Note 'Time' is converted to the model units
# specified by TIMEUNIT.
## COLUMNS 2
##
## COLUMN1.name          Time
## COLUMN2.long_name     Time
## COLUMN1.units         days since 1990-01-01 00:00:00 +8
## COLUMN1.missing_value -999
```

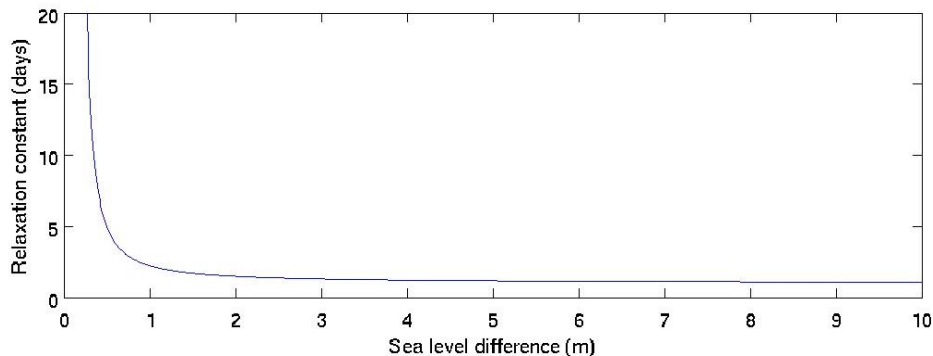
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```
## COLUMN1.fill_value      0.0
##
## COLUMN1.name            eta_relaxation_time_constant
## COLUMN2.long_name      Eta relaxation time constant
## COLUMN1.units          hours
## COLUMN1.missing_value  -999
## COLUMN1.fill_value     0.0
##
0 48
10 2
```

Adaptive relaxation can be invoked by specifying:

```
eta_relaxation_time_constant linear dv1 tc1 units1 dv2 tc2 units2
eta_relaxation_time_constant exponential dv1 tc1 units1
```

In the linear case, if the absolute difference between modelled eta and that read from `infile.nc` is  $dv_1$ , then a relaxation constant of  $tc_1$  `units1` is used and if the absolute difference is  $dv_2$ , then a relaxation constant of  $tc_2$  `units2` is used, with linear interpolation for other values of the absolute difference. For the exponential case, a function  $rate = \exp(\alpha |dv|)$  is used where  $dv$  is the difference between modelled eta and that read from `infile.nc` and  $\alpha = dv \ln(tc)$ . The relaxation constant will therefore vary spatially and temporally throughout the domain and simulation. An example is included below, where  $dv_1 = 0.5$  m and  $tc_1 = 5$  days.



A relaxation rate linear in time may be specified using:

```
eta_relaxation_time_constant temporal dv1 tc1 units1 dv2 tc2 units2
```

In this case the relaxation rate is  $tc_1$  `units1` at  $dv_1$  days (relative to the `TIMEUNIT`), changing linearly to  $tc_2$  `units2` at  $dv_2$  days, then thereafter capped at  $tc_2$  `units2`.

Depth based relaxation methods analogous to tracer relaxation (see Section 4.9.2) are also available. In these cases the sea level increment is saved to a 2D tracer `eta_inc`. These methods are invoked using:

```
eta_relaxation_time_constant depth dv1 tc1 units1 dv2 tc2 units2
eta_relaxation_time_constant exp_depth a0 tc1 units1 d1 tc2 units2
:
eta_relaxation_time_constant cos_depth d0 tc1 units1 d1 tc2 units2
```

Often the relaxation elevation does not contain tidal variation. If the model includes tidal forcing, this must be removed before relaxation can occur. This may be invoked using:

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```
TIDAL_REMOVAL CSR # Removal using tide computed from the CSR tide
                  # model.
                  MEAN # Use the long term eta mean as an approximation
                  # to the relaxation elevation. ETA must be
                  # included as a MEAN diagnostic (see Section
                  # 4.30.2) for this to operate, with a MEAN_DT
                  # equal to the length of the run.
```

**COMPAS only:** if the custom tide diagnostic is invoked (NUMBERS TPXO; Section 4.31.14) then sea level may be relaxed to this field using:

```
eta_relaxation file          TPXO
```

Velocity relaxation may be achieved with the same functionality as for elevation. In this case any 'eta\_' is replaced with 'vel\_' in the relaxation specification. Relaxation is performed every 3D time-step for the 3D mode, and 2D time-step for the 2D mode.

## 4.14 Wind

Wind forcing is specified by number of parameters which define an input time series of wind velocity components, and drag law coefficients. The model implements a general piece-wise linear surface drag coefficient (see, for example, Large and Pond, 1981). It has the form:

$$C_d = \begin{cases} C_{d0} & V \leq V_0 \\ C_{d0} + (C_{d1} - C_{d0}) \frac{(V - V_0)}{(V_1 - V_0)} & V_0 < V < V_1 \\ C_{d1} & V \geq V_1 \end{cases}$$

where  $C_d$  is the surface drag coefficient,  $V$  is the wind speed and  $C_{d0}$ ,  $C_{d1}$ ,  $V_0$  and  $V_1$  are specified parameters (described below). The surface stress  $\tau_{top}$  is then calculated as follows:

$$\tau_{top} = \rho_{air} C_d |\mathbf{V}| \mathbf{V}$$

where  $\rho_{air}$  is the air density (see section 4.5), and  $\mathbf{V}$  is the wind velocity vector. Note that the above formulation for  $C_d$  implies that the surface stress varies roughly as the cube of the wind speed for speeds between  $V_0$  and  $V_1$ . As a result, in some applications the model results can be very sensitive to the wind input data.

The drag parameterization may be alternatively specified using the following:

```
WIND_STRESS_FCTN L&P # Large and Pond (1982) scheme, (Eqn 21)
                  K/W # Kitaigorodskii et al (1973) scheme
                  B   # Bunker (1976) scheme
                  Ko  # Kondo (1975) scheme
```

These alternative schemes also require a reference height in metres to be supplied, corresponding to the height where measurements were made, e.g;

```
WIND_STRESS_REFH 10 # Reference height in (m)
```

For  $Ko$  the option exists to use the drag coefficient for neutral conditions:

```
WIND_STRESS_NEUTRAL YES # neutral drag coefficient
```



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At the start of a model run, wind forcing may be smoothly ramped up from zero over some specified period (see `RAMPSTART` and `RAMPEND` in section 4.3). This may help to avoid shocks or start-up transients in the model.

Wind inputs are specified as follows:

```
# A time series file containing wind East and North
# velocity components, which must be called 'u'; and 'v'
# respectively, and have units of ms-1.
WIND_TS                cyc_bobby95.nc
# How often to read data from the wind file and update
# the wind field in the model.
WIND_INPUT_DT          10 minutes
# Scale factor applied to the wind speed. This makes it
# easy to do experiments with different wind strengths
# without having to generate a new wind time series file.
WIND_SPEED_SCALE       1.0

# Drag law coefficients. Here they are as used by
# Large and Pond, (1981). V0 and V1 have units of m/s.
DRAG_LAW_V0            10.0
DRAG_LAW_V1            26.0
DRAG_LAW_CD0           0.00114
DRAG_LAW_CD1           0.00218
```

The wind speed components in the north and east directions must bear the names 'u' and 'v' in the wind input file (see Section 4.29). These wind components are then rotated onto the grid to conform to the grid e1 and e2 directions. If the wind components already conform to the grid orientation they may be directly applied without rotation by specifying the names 'wind\_e1' and 'wind\_e2' in the wind input file.

Wind stress may be directly applied to the grid by using the `WIND_TYPE` flag, eg.;

```
# Wind input file contains wind speed (ms-1) (used by default)
WIND_TYPE              SPEED
# Wind input file contains wind stress (Nm-2)
WIND_TYPE              STRESS
```

If the `WIND_TYPE` flag is absent the wind input file is assumed to contain wind speeds.

## 4.14.1 Generic Storm Systems (*SHOC only*)

Wind stress may be applied to the domain corresponding to the passage of generic cyclonic or anticyclonic synoptic weather systems. This is useful for performing idealized experiments or prescribing a realistic time and space dependent wind-field in the absence of measured data. These systems are defined by their (i,j) location in the grid relative to the grid origin, maximum pressure gradient, rotation to a latitude circle and eccentricity. Any number of these systems may be defined corresponding to certain times, and SHOC piecewise interpolates the defined systems to produce a wind pattern at any particular time during the simulation. The (i,j) location need not be defined within the dimensions of the domain but may assume any value ( $-\infty < i < \infty$ ,  $-\infty < j < \infty$ ). For this reason the locations must be supplied in terms of (i,j) rather than geographic coordinates, since there only exists a map between geographic coordinates and (i,j) locations within the confines of the domain. Generally the user must perform some type of extrapolation if the storm center is to be defined beyond the confines of the domain; this may not be trivial for curvilinear grids and some trial and error may be necessary. The storm systems are defined via:

```
NSTORM                n                # Number of storm systems to define
STORM_INPUT_DT        ? day            # Interval wind stress is updated
```

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```
ST0.stime      ? days      # Time this system is defined at
ST0.stype      HIPR or LOPR # High pressure or low pressure
systems
ST0.sp         ?           # Maximum pressure gradient (HPa/km)
ST0.ss         ?           # Radius (km)
ST0.si         i           # i location of system center
ST0.sj         j           # j location of system center
ST0.se         ?           # Eccentricity (0<e<1)
ST0.sr         ?           # Rotation (0<θ<360)
```

An example of a propagating storm system is given below:

```
NSTORM        3
STORM_INPUT_DT 1 day
ST0.stime      0 days
ST0.stype      HIPR
ST0.sp         7e-4
ST0.ss         3000
ST0.si         -20
ST0.sj         20
ST0.se         0
ST0.sr         0
```

```
ST0.stime      5 days
ST0.stype      HIPR
ST0.sp         1e-5
ST0.ss         2000
ST0.si         20
ST0.sj         20
ST0.se         .8
ST0.sr         90
```

```
ST0.stime      10 days
ST0.stype      HIPR
ST0.sp         7e-4
ST0.ss         3000
ST0.si         40
ST0.sj         20
ST0.se         0
ST0.sr         180
```

This system propagates through the domain along the  $\xi_1$  axis, centered on  $\xi_2=20$ . At day 0 it assumes the form of a circular anticyclone, at day 5 it strengthens, contracts in size and becomes elliptic with the major axis aligned in the north-south direction. By day 10 it has weakened and become larger again with a circular shape. The wind stress field is updated according to this progression at daily intervals.

If a wind file is specified in conjunction with the storm system specification then the wind and storm components are added to produce the wind stress vector.

### 4.15 Atmospheric pressure

A mandatory parameter sets the background air pressure, as follows:

```
# Background air pressure, in Pa
AMBIENT_AIR_PRESSURE 101000
```

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This value sets the air pressure throughout the model domain. Because this value is uniform, it is not dynamically significant unless time and space varying pressure forcing is also specified, as outlined below.

Models covering larger domains (or including phenomena such as severe storms) may require such atmospheric pressure inputs. These are specified by the following optional parameters:

```
# A time-series file containing the variable 'pressure' with
# units of Pa.
PRESSURE                cyc_bobby95.nc
# How often to read the file and update the pressure
# field in the model.
PRESSURE_INPUT_DT      10 minutes      # Update every 10 minutes.
```

In this case, horizontal gradients in atmospheric pressure are dynamically included in the model, and any difference between the pressure specified in the `PRESSURE` data file and the `AMBIENT_AIR_PRESSURE` value may cause an inverse barometer effect at elevation open boundaries (see section 4.11.18).

## 4.16 Rainfall

Rainfall can be included as a model forcing input by using the following optional parameters:

```
# A time-series file containing the variable 'precipitation'
# with units mm day-1 (the SI unit would be m s-1, but this
# results in ridiculously small values).
PRECIPITATION          rain.nc

# How often to read the precipitation data.
PRECIPITATION_INPUT_DT 10 minutes
```

Rainfall is assumed to be fresh (zero salinity), at ambient air temperature (see section 4.18), and have zero concentration of all other tracers. Rainfall increases the volume of water in the model, and so may directly affect the model surface elevation.

## 4.17 Evaporation

Evaporation can be included as a model forcing input by using the following optional parameters:

```
# A time-series file containing the variable 'evaporation'
# with units mm day-1.
EVAPORATION           evap.nc

# How often to read the evaporation data.
EVAPORATION_INPUT_DT 10 minutes
```

Evaporation removes fresh water from the model. Evaporation can cause numerical problems in the model if the surface layer is very thin, as tracer concentrations can increase without bound as the surface layer evaporates and the thickness approaches zero. This problem will be addressed in future model versions, but can usually be avoided by judicious choice of vertical grid geometry.

Note that evaporation rates are specified in an input time series file. This implies that the rates must be obtained by calculation or observation prior to the model run, so that the water

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temperature simulated by the run itself is not directly used as an input to the estimates of evaporation.

### 4.18 Surface heat flux

**SHOC** includes a variety of explicit heat flux parameterizations. The options for defining a heat flux are:

```
HEATFLUX    NONE           # No heat flux included
HEATFLUX    BULK           # Computed using bulk method
HEATFLUX    NET_HEAT       # Net heat flux supplied via timeseries
HEATFLUX    SURF_RELAX     # Surface layer temperature relaxation
HEATFLUX    GHRSSST        # Surface layer ghrsst SST relaxation
HEATFLUX    INVERSE        # Heat flux calculated inversely
HEATFLUX    COMP_HEAT      # Heat flux from RAMS components
HEATFLUX    COMP_HEAT_MOM  # Heat flux from MOM4 components
```

The least complex (and least realistic) surface heat flux mechanism is implemented by relaxation of the surface layer temperature to some prescribed, possibly time varying field using the `SURF_RELAX` option as follows:

```
# Time-series file specifying surface temperatures, containing
# the variable 'heatflux_temp' with units 'Degrees C'.
HEATFLUX_TEMP      temp.nc
HEATFLUX_TEMP_DT   1 day
# Relaxation time constant
HEATFLUX_TC        20 days
```

This mechanism is similar to the more general tracer relaxation mechanism described in section 4.10, except that it only operates on the surface layer of the model, rather than throughout the model.

If `HEATFLUX` is specified as `GHRSSST`, then SST is relaxed toward the `GHRSSST` SST values. In this case the `GHRSSST` diagnostic must also be invoked (see Section 4.31.20). Note that the heatflux may be specified as:

```
HEATFLUX    BULK    GHRSSST
```

In this case a bulk formulation is computed, and the surface temperature is additionally relaxed toward `GHRSSST` SST.

The `BULK` heat flux formulation uses a more complex bulk formulation and long wave parameterisation, in addition to calculating the short wave component rather than supplying a time-series file (see Herzfeld et al (2002), section 9.2). A number of input data sets are required, all of which are optional, as described below.

Sensible heat flux requires the specification of the air temperature (as well as wind inputs - see section 0). Air temperatures are specified as follows:

```
# Time-series file containing the variable 'air_temp' with
# units 'Degrees C'.
AIRTEMP      airtemp.nc

How often to read the air temperature file.
AIRTEMP_INPUT_DT  10 minutes
```

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The sensible heat flux is proportional to the product of the wind speed and the difference between the model surface layer temperature and the air temperature. The latent heat flux requires data to calculate specific humidity:

```
# Time-series file containing the variable 'wet_bulb' with
# units 'Degrees C'.
WET_BULB          wetbulb.nc
WET_BULB_INPUT_DT 10 minutes
```

In the absence of wet bulb measurements, the dew point temperature may be substituted;

```
# Time-series file containing the variable 'dew_point' with
# units 'degrees C'.
DEW_POINT         dewpoint.nc
DEW_POINT_INPUT_DT 10 minutes
```

If available, specific humidity may be supplied directly:

```
# Time-series file containing the variable 'rhumidity' with
# units 'kgkg-1'.
HUMIDITY          humidity.nc
HUMIDITY_INPUT_DT 10 minutes
```

Or as a last resort, relative humidity may be used:

```
# Time-series file containing the variable 'humidity' with
# units '%'.
HUMIDITY          humidity.nc
HUMIDITY_INPUT_DT 10 minutes
```

If available, a file containing short wave radiation may be supplied directly as below.

```
# Time-series file containing the variable 'swr' with
# units 'W m-2'.
RADIATION         swr.nc

# How often to read the solar radiation data
RADIATION_INPUT_DT 10 minutes

# Albedo of the surface
ALBEDO            0.2
```

If  $-1 < \text{ALBEDO} < 0$  then the albedo is computed as a function of cloud amount and hour angle (sect 9.1.1 Science Manual). In the absence of a CLOUD file, clear skies are assumed. There are five bulk schemes available to specify latent and sensible heat fluxes. These are specified via;

```
# Specify the bulk method
BULK_SCHEME      L&P # Large and Pond (1982) scheme
                  Ko  # Kondo (1975) scheme
                  B   # Bunker (1976) scheme
                  K/W # Kitaigorodskii et al (1973) scheme
                  M   # Masagutov (1981) scheme
```

These schemes are compared in Blanc (1985). The default is the scheme of Kondo (1975).

A ramp may be applied to the heatflux, where zero heatflux is applied before the time specified, e.g.

```
# Do not apply a heatflux before 10 days, relative to the TIMEUNIT
HEATFLUX_RAMP    10 days
```

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It is possible to distribute the short wave radiation throughout the water column by specifying an attenuation coefficient, `SWR_ATTENUATION`; if this is absent all short wave radiation is included in the surface boundary condition. It is possible to partition a fraction of the short wave radiation to be input as the surface boundary condition with the remainder distributed throughout the water column according to the attenuation coefficient. This is achieved by specifying a transmission coefficient, `SWR_TRANSMISSION`; if this is absent it is assumed all short wave radiation is depth distributed..

```
# Specify short wave radiation attenuation and transmission
# parameters.
SWR_ATTENUATION 0.2 # Attenuation
SWR_TRANSMISSION 0.5 # Fraction for depth distributed swr
```

Attenuation and transmission may be set to standard water classes according to Mellor (1992), e.g;

```
# Set the water type to Type II water
WATER_TYPE TYPE_II
```

Attenuation and transmission are set according to the table below:

Water Type	Attenuation	Transmission
I	0.037	0.32
IA	0.042	0.31
IB	0.056	0.29
II	0.073	0.26
III	0.127	0.24

Note that `SWR_TRANSMISSION = 1` means that all shortwave radiation is depth distributed. Alternatively the dual extinction parameterization may be used where separate extinction coefficients are used for the surface and deeper layers. A fraction determines the partitioning between surface and deep attenuation.

```
# Specify dual short wave radiation attenuation parameters.
SWR_ATTENUATION 2.8 # Surface attenuation
SWR_ATTENUATION_DEEP 0.04 # Deep attenuation
SWR_FRACTION 0.58 # Fraction for surface attenuation
```

Where short wave radiation penetrates to the bottom, it is assumed that all surplus radiation below the sea floor is absorbed into the sea bed with no additional heating of the bottom layer. This may be altered using the `SWR_BOT_ABSORB` flag, where a (default) value of 1 assumes the above, while a value of 0 assumes all surplus short wave radiation is input into the bottom layer. The reality is that bottom reflectance would supply some heat to the bottom layer and the value `SWR_BOT_ABSORB` of would be somewhere between 0 and 1. This flag may be used as a tuning parameter, e.g.

```
# Specify fraction of surplus radiation input into bottom layer.
SWR_BOT_ABSORB 0.5 # Bottom absorbtion
```

The short wave parameters may be input as a 2-D spatially varying field by supplying a netCDF file as input, e.g.

```
SWR_BOT_ABSORB babs.nc # 2D varying bottom absorbtion
```

Or a list of ascii values in the parameter file, e.g. for a 2 x 2 grid:

```
SWR_BOT_ABSORB 4 # 2 x 2 = 4 values
0.9 0.8 0.0 0.5 # List of values.
```

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In these cases a new input file must be created using the `-g` option so that short wave parameters are correctly initialized. Finally, the `swr_attenuation` may be specified by specifying a tracer name in the tracer list, e.g.

```
SWR_ATTENUATION <trname> # Uses the values in tracer 'trname'
```

If the tracer specified uses the reset function (Section 4.9.3), then this allows a temporally and spatially varying attenuation to be used. Note that these short wave parameters are 2D tracers; it is possible to specify short wave attenuation only as a 3D field using:

```
SWR_ATTENUATION3D 0.5 # Constant value
SWR_ATTENUATION3D attn.nc # Initial value (create using -g)
SWR_ATTENUATION3D <trname> # 3D tracer value
```

**If a 3D tracer name is used as the short wave attenuation, then create an input file (`-g`) using a constant or initial value, then change the attenuation to a tracer when performing the run (`-p`).**

The short wave radiation parameters (attenuation and transmission) may be estimated from the best fit within an ensemble if required. To invoke this use:

```
swr_regions regions.bnc # A subdivision of the domain using regions
                ONE      # Only one profile in the domain is used
                ALL      # Parameters are estimated at every grid
swr_dt          1 hour   # The time interval parameters are estimated
swr_data        GHRSSST  # Data SST is compared to for optimization
```

The principle of this method is that at a certain time interval (`swr_dt`) and at a given water column location (e.g. within each region specified in a `.bnc` region file; see Section 4.31.21 for creation of region files) an ensemble of attenuation (0.03 to 0.137 in increments of 0.01; spanning all Jerlov classes) and transmission (0 to 1 in increments of 0.1) is created, and the column is subject to vertical diffusion using the vertical diffusion coefficient and short wave radiation in effect at that time. An ensemble of SST solutions results, and the optimum attenuation and transmission is chosen as that which produces the lowest RMS error against provided observations. These observations may be GHRSSST SST (see Section 4.31.20 for importing GHRSSST data) or a 2D tracer in the tracer list (see `copy_layer` in Section 13 to extract a surface layer from a 3D dataset, e.g. global data). The GHRSSST option is set by default, and in this case the user must also specify GHRSSST data import.

Note that `SWR_ATTENUATION` and `SWR_TRANSMISSION` need not be specified using this option. If one of these parameters are specified, the ensemble is generated using the specified fixed value, and the unspecified variable range and resolution is increased. For example if `SWR_TRANSMISSION` is specified with a value of 0.59433, then the ensemble is built using this value and `SWR_ATTENUATION` takes on 100 values between 0.03 and 0.137 in increments of 0.001.

If regions are specified using a `.bnc` file, then the mean SST data (e.g. GHRSSST) in each region is computed, and the column used to create the ensemble in each region is that which has a model surface temperature closest to that of the regional mean. A 2D tracer `swrms`, written to output file, is created which shows the location of the columns in the grid used for optimisation, and the value of the optimised RMSE at those locations. The column optimised value of attenuation and transmission are then used for that entire region. Note that if `NWINDOWS > 1`, then each region is further subdivided into regional partitions in each window (i.e. the overall partitioning is more than that specified in the region file). If `ONE` is specified, the same approach is used for the entire domain. This is the least computationally expensive approach. If `ALL` is used, every grid cell is optimised for attenuation and transmission; this is the most computationally expensive, but most accurate approach. A 2D tracer `swreg`, written to output files, is created which shows the partitioning for swr estimation used.

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The model will create a running mean of optimized attenuation (stored in `attn_mean`) and transmission (stored in `tran_mean`) which are used for the model timestep update of vertical mixing in preference to the optimised values. When `swr` is zero (i.e. at night) the parameter estimation is not performed.

Note that if `swr_dt` is short, then insufficient heat may be input/lost over the time interval to reach the target temperature, and `swr` parameters tend to converge to the extremes of the ensemble. If `swr_dt` is too long, then the assumptions that vertical mixing and `swr` input are constant over the interval may not hold.

**COMPAS only:** The ensemble size may be specified using COMPAS with:

```
SWR_ENSEMBLE      attn_s attn_e tran_s tran_e
```

Where `attn_s` is the start attenuation value of the ensemble, `attn_e` is the end attenuation value of the ensemble, with the attenuation increment then  $(attn_e - attn_s) / 10$ . Also, `tran_s` is the start transmission value of the ensemble, `tran_e` is the end transmission value of the ensemble, with the transmission increment then  $(tran_e - atran_s) / 10$ .

If measurements of shortwave radiation are not available, then this parameter may be calculated. This requires the specification cloud cover as follows:

```
# Time-series file containing the 'cloud' with units 'oktas'.
CLOUD                cloudiness.nc
CLOUD_INPUT_DT      10 minutes
```

ALBEDO must not be present if short wave radiation is to be computed by the model.

Note that if the ecology module is invoked then short wave radiation is input via the `LIGHT` and `ALBEDO_LIGHT` parameters which differ from the `RADIATION` parameters in that the ecology module requires a daily mean short wave radiation, which is inadequate for the heat flux calculation.

Longwave downwelling radiation may be specified independently using the `BULK` method, such that total longwave is the sum of this component and the blackbody longwave output at the sea surface. To specify longwave downwelling radiance, use;

```
# Time-series file containing the variable 'lwr_in' with
# units 'W m-2'.
LONGWAVE_IN          longwave.nc
LONGWAVE_INPUT_DT   10 minutes
```

The bulk parameters are usually specified at a standard height of 10m. If the wet and dry bulb temperatures (and wind) are not measured at this standard height, then the bulk parameters must be scaled from the standard height to the reference height the measurements were taken at. The user should therefore supply the reference height of measurements via:

```
# Reference height of meteorological measurements, units 'm'.
HEATFLUX_REFH       5.0
```

If the reference height is absent a height of 10m is assumed. A larger reference height results in larger bulk fluxes.

The sensible heat flux uses a gradient between the air temperature and SST. The SST used in this calculation is that predicted by the model. The user may submit an alternate file (e.g. of field measured SST) from which the sensible heat is computed. In this case a `HEATFLUX_TEMP` file (see above) containing sea surface temperature must be supplied.

Correcting air temperature and humidity for advection effects (see section 9.3 Herzfeld et al 2002) is invoked via:



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```
# Include the correction to air temperature and humidity due to
# advective effects.
```

```
HEATFLUX_ADVECT          YES
```

Note that the advection correction uses a calculation of fetch from 8 compass points; if all these directions are not required then the array `mask[]` in `init_fetch()` in the module `forcings/heatflux.c` may be modified (zero values omit the corresponding wind directions in the advection calculation).

The `NET_HEAT` option imposes a net heat flux directly from time-series input as the surface boundary condition for temperature and requires the following:

```
# Time-series file containing the variable 'heatflux' with
# units 'W m-2'.
HEATFLUX_FILE            heatflux.nc
HEATFLUX_DT              1 day
```

Note that a positive flux indicates heat input into the ocean. Short wave radiation may be input separately and distributed with depth as per the `BULK` option above. In this case the net heat flux corresponds to the sum of long wave radiation, sensible and latent heat fluxes.

Finally the `INVERSE` option calculates a heat flux inversely based on a time-series of surface water temperatures (see Herzfeld et al 2002, section 9.4 for details). In the absence of any heat flux information this constitutes a helpful first estimate of heat input. This option requires a timeseries of SST observation, input in the same manner as relaxation to the surface; i.e.

```
# Time-series file specifying surface temperatures, containing
# the variable 'heatflux_temp' with units 'Degrees C'.
HEATFLUX_TEMP           temp.nc

# Time constant
HEATFLUX_TC             20 days
```

In this case the time constant determines the time-scale over which the SST will change due to the applied heatflux, i.e. the shorter the time constant the larger the estimated fluxes. Generally the time constant should be of the order of the frequency of observations.

The heat flux generated with the `BULK` and `INVERSE` methods (and heat flux components) are saved as tracers which may be viewed in the model output. If the `BULK` option is invoked, the heat flux components are written to the time series files.

The atmospheric model RAMS (Pielke et. al., 1992) can output heatflux components that may be assembled to generate a net heat flux comprising of sensible, latent and longwave fluxes, and a short wave component that is depth distributed as above. Note that this formulation the longwave radiation is replaced with analytical blackbody outgoing radiation and clear sky longwave input, since this seems to generate heatfluxes that balance (i.e. do not excessively heat or cool the ocean) in the long term, hence producing better results. Also, RAMS may produce latent heat > 0 when it is raining, hence the latent heat imposed using this option has a maximum of zero. This option is invoked, for example, via:

```
# Impose RAMS heat flux components
HEATFLUX                COMP_HEAT
HEATFLUX_FILE           RAMS.nc
HEATFLUX_DT             30 minutes
```

In this case the file `RAMS.nc` must contain variables with names `swr` (short wave radiation), `lwr_in` (downward long wave radiation), `lwr` (outward long wave radiation), `sensible`

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(sensible heat flux) and `latent` (latent heat flux). See Section 7 for more detail on `COMP_HEAT`.

Heatflux components used in the global ocean model MOM4 may also be assembled in a similar manner. In this case the short wave radiation is provided as a mean over some fraction of a day defined by `HEATFLUX_DT`. The daily profile is reconstructed from these means using the methodology of Schiller and Godfrey, 2003. Also, latent heat is provided as an evaporation rate in units of  $\text{kgm}^{-2}\text{s}^{-1}$ , which is converted to  $\text{Wm}^{-2}$  by multiplication by the latent heat of evaporation ( $L_v = 2.5 \times 10^6$ ). This option is invoked, for example, via:

```
# Impose MOM4 heat flux components
HEATFLUX          COMP_HEAT_MOM
HEATFLUX_FILE     MOM.nc
HEATFLUX_DT       30 minutes
```

In this case the file `MOM.nc` must contain variables with names `swr` (short wave radiation), `lwr` (outward long wave radiation), `sensible` (sensible heat flux) and `latent` (latent heat flux). These variables usually require the use of variable substitution, since they typically have the following MOM names:

```
swr = sw_flux
lwr = lw_flux
sensible = t_flux
latent = q_flux
```

## 4.19 Surface salt flux

A surface salt (or freshwater) flux may be included to account for the effect of water fluxes on salinity. This can be specified via the flag:

```
SALTFLUX    NONE          # No salt flux included
SALTFLUX    ORIGINAL      # Salt fluxes from file
SALTFLUX    BULK          # Salt flux partially determined using bulk
                          # schemes.
```

The `BULK` method requires `PRECIPITATION` and `EVAPORATION` time-series files to be defined (sections 4.16 and 4.17) from which the surface salt flux is calculated and applied as a surface boundary condition for the vertical diffusion of salinity (see Herzfeld et al (2002), section 9.4). Evaporation is difficult to measure over water, and the latent heat of evaporation may be used to estimate this parameter (Herzfeld et al (2002), section 9.4) when the `BULK` method is invoked. Since this bulk flux is used, the `BULK` method will only function if the `HEATFLUX` flag is set to `BULK` so that latent heat of evaporation is calculated. If a `PRECIPITATION` time-series file is present then the effect of rain is added to the calculated evaporation.

## 4.20 Bottom friction

Bottom friction in the model is implemented as a combination of a linear and quadratic drag law. The bottom stress  $\tau_{bot}$  is calculated as follows:

$$\tau_{bot} = \rho C_d U m a(|U|, U_f)$$

where  $\rho$  is the water density,  $U$  is the bottom velocity, and  $U_f$  is a small background friction velocity, below which the friction law changes from quadratic to linear (with an effective drag coefficient of  $C_d U_f$ ).

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The bottom drag coefficient  $C_d$  is calculated using a bottom roughness length  $z_0$  (which may vary spatially), as follows:

$$C_d = \max\left(\sqrt{\frac{1}{K} \ln\left(\frac{z+z_0}{x_0}\right)}, C_{d\min}\right)$$

Here,  $K$  is the von Karman constant (0.4), and  $z$  is the height of the nearest velocity point above the sea bed.  $C_{d\min}$  is a parameter, typically between 0.002 and 0.003, which places a lower limit on the value of  $C_d$  when the velocity point is a long way from the bottom.

The model parameters associated with the formulations described above are specified as follows:

```
# Minimum bottom drag coefficient. If QBFC < 0, then this value is
# used directly for the bottom drag.
QBFC                0.0025

# Background friction velocity (ms-1)
UF                  0.01

# Bottom roughness (values in metres).
Z0                  0.001
```

**COMPAS only:** if  $QBFC < 0$  in 2D mode, then the Manning friction coefficient is computed for the drag coefficient, where:

$$C_D = \frac{gn^2}{D^{1/3}}$$

with  $n$  = Mannings coefficient ( $s.m^{-1/3}$ ) and  $D$  = depth (m) (see [http://www.marinespecies.org/introduced/wiki/Bed\\_roughness\\_and\\_friction\\_factors\\_in\\_estuaries](http://www.marinespecies.org/introduced/wiki/Bed_roughness_and_friction_factors_in_estuaries)).

For COMPAS the  $QBFC$  coefficient may be interpolated onto the mesh from file or specified using region files, e.g;

```
QBFC drag_file.nc # netCDF file input
QBFC region drag.bncc 0:0.01 1:0.022 2:0.05 # Region input
```

### 4.21 Waves

Waves are primarily used in SHOC/COMPAS in conjunction with sediment transport libraries so that bottom friction may be enhanced by wave action to result in increased resuspension. This requires that wave period, wave amplitude, wave direction and orbital velocity are supplied or computed. These quantities may be supplied via file input using:

```
WAVE_VARS wave.nc # Wave time series file
WAVE_VARS_INPUT_DT 2 hours # How often to read the wave data
```

Alternatively, the wave variables may be created by SHOC/COMPAS and provided with values via the wave library (see below) using:

```
WAVE_VARS YES
```

If a `WAVE_VARS = YES` or a file is specified, then SHOC will automatically create 2D tracers for the wave variables. This is done even if the input file does not contain data for the wave

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variables (e.g. an empty file). The wave variables created by SHOC are (see Section 4.31.15):

Tracer name	Variable name in input file	Description
wave_amp	amplitude	wave amplitude (m)
wave_period	period	wave period (s)
wave_dir	direction	wave direction (deg T)
wave_ub	ub	bottom orbital velocity (ms <sup>-1</sup> )
ustrcw	-	wave current friction
wave_Fx	force_x / force_e1	x Radiation stress (Nm <sup>-2</sup> )
wave_Fy	force_y / force_e2	y Radiation stress (Nm <sup>-2</sup> )
wave_ste1	stokes_x / stokes_e1	x Stokes drift velocity (ms <sup>-1</sup> )
wave_ste2	stokes_y / stokes_e2	y Stokes drift velocity (ms <sup>-1</sup> )

The influence of wave action on the hydrodynamics is controlled by the parameter WAVES. Currently, feedback of wave enhanced bottom friction to the hydrodynamics and the influence of waves on currents due to radiation stresses is supported. The wave options are invoked by listing the following:

```

WAVES      BOT_STRESS      # Allow feedback of wave bottom
              # friction.
              TAN_RADIATION # Include tangential radiation
              # stresses.
              WAVE_FORCING  # Include 2D wave forcing using
              # radiation stresses read from
              # file.
              STOKES        # Include Stokes drift velocity:
              # Stokes Coriolis, Stokes vortex,
              # enhanced vertical mixing and
              # wave-to-ocean impacts.
              STOKES_DRIFT  # Include Stokes drift velocity:
              # Stokes Coriolis, Stokes vortex.
              STOKES_MIX    # Include Stokes drift velocity:
              # enhanced vertical mixing.
              STOKES_WIND   # Include Stokes drift velocity:
              # wave-to-ocean impacts.
              VERT_MIX      # Wave amplitude used for surface
              # length scale in vertical
              # mixing.
              NONE          # No wave options invoked.

```

The default is NONE. Note that multiple options may be invoked in the list, e.g:

```

# Allow wave enhanced bottom friction and radiation stresses
WAVES      BOT_STRESS TAN_RADIATION

```

SHOC/COMPAS will automatically create the following 2D tracers if these conditions are invoked:

```

wave_Cd      # Wave enhanced bottom drag for BOT_STRESS
wave_Sxy     # Tangential radiation stresses (m2s-2) for
wave_Syx     # TAN_RADIATION.
wave_Fx, wave_Fy # Radiation stresses (Nm-2) for WAVE_FORCING.
wave_ste1, wave_ste2 # Stokes drift velocity (ms-1) for STOKES.

```

If wave enhanced mixing is invoked, several methods are available for the k-ε and k-ω mixing schemes only:

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**MIX\_JONES** : The method outlined in Jones, N.L. and Monismith, S.G. (2008). Modelling the influence of wave-enhanced turbulence in a shallow tide- and wind-driven water column. JGR, 113, C03009. This method allows for the constant  $\alpha$  to be altered via `WAVE_ALPHA` (default is 100).

**MIX\_WOM** : The wave orbital method, Babanin and Haus, (2009), On the existence of water turbulence induced by non-breaking surface waves JPO, Notes and Correspondence, 39, 2675 – 2679. This method allows for the constant  $b_1$  to be altered via `WAVE_B1` (default is 0.0014).

**MIX\_BVM** : The wave induced mixing coefficient,  $B_v$  method for monochromatic waves, Qiao, F., Yuan, Y., Ezer, T., Xia, C., Yang, Y., Lu, X., Song, Z., (2010) A three dimensional surface wave-ocean circulation coupled model and its initial testing, Ocean Dynamics, 60, 1339 – 1355. This method allows for the constant  $\alpha$  to be altered via `WAVE_ALPHA` (default is 100 as per the **MIX\_JONES** method, and should be changed to 1 or 4.).

Radiation stresses may be read from file (i.e. a file is provided to `WAVE_VARS`), as provided by a wave model (SWAN, WWIII etc). These variables may be aligned with the grid or have components in the east/north direction, and have units of  $\text{Nm}^{-2}$ . In this case the depth averaged velocity is augmented to reflect the forcing due to these radiation stresses. To invoke this forcing, the `WAVE_FORCING` keyword should be specified. If the `MOM_TEND` flag is true, then tangential radiation stress tendencies ( $\text{ms}^{-1}$ ) are added to the tracer list.

**SHOC only:** If `WAVE_VARS = YES` and `WAVES = TAN_RADIATION`, then the radiation stresses may be applied to the 2D mode following the implementation of Bye (1977a).

For SHOC/COMPAS, the Stokes drift velocity may be aligned with the grid or east/north, and have units of  $\text{ms}^{-1}$ . In this case the drift velocity is added to the 3D and 2D Coriolis terms. To invoke this forcing, the `STOKES` keyword should be specified. The Stokes Coriolis and vortex forces are applied according to Moon (2005), Eq. 14.

A wave library exists which is responsible for the calculation of wave variables (period, amplitude, direction, orbital velocity, bottom stress, enhanced bottom drag and tangential radiation stresses). If this library is to be invoked, then the following parameters are set:

```
DO_WAVES      YES          # Invoke the waves library
WAVES_DT      1 hour      # Time interval which waves are invoked
```

The wave variables are computed according to the amount of information supplied in the `WAVE_VARS` file. If `WAVE_VARS = YES`, or the `WAVE_VARS` file doesn't contain any of the wave variables, then the waves are assumed to be wind waves and are estimated using Eqns. 10.9, 10.11 and 10.14 in the Science Manual. Wave direction is assumed to be the same as the wind direction.

**SHOC only:** Alternatively, Eqns. 10.12 and 10.13 may be used to estimate wave amplitude and period. This choice is controlled by the flag:

```
WIND_WAVE     TOBA # Use eqns. 10.9 and 10.11
               USAC # Use eqns. 10.12 and 10.13
```

The fetch is required when estimating wind waves using these methods. This is automatically created by SHOC when using `DO_WAVES`. The fetch at the limits of the model domain (open boundaries) may be specified via spatially variable netCDF or spatially constant .ts file input:

```
FETCH         fetch_OBC.nc # Boundary values for fetch
```

For SHOC/COMPAS, if the wave period only is supplied in the `WAVE_VARS` file, then wind wave amplitudes are estimated using the simpler formulation of Eqn. 10.8 (Science Manual) which does not use the fetch. If all the wave variables are included in the `WAVE_VARS` file, then waves are assumed to be swell waves and the values retrieved from file are used for wave amplitude, period and direction.

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A Grant-Madsen style bottom boundary layer (see Grant and Madsen, 1986 or Madsen, 1994) is used to compute wave enhanced bottom friction. In this case, the bottom roughness, `Z0`, is replaced by a time and space varying apparent bottom roughness, calculated according to specified wave input data. The bottom friction model parameters are still required, with `Z0` becoming the bottom roughness value in the absence of waves.

## 4.21.1 SWAN 2-way coupling (COMPAS only)

COMPAS may be 2-way coupled with the SWAN spectral wave model, v41.31 available from <http://swanmodel.sourceforge.net/download/download.htm>. This model is built as a library function within EMS and called by the wave libraries as a subroutine, with information transferred between SWAN and COMPAS via pointers. This coupling can only be performed on meshes using Voronoi diagrams (i.e. not quadrilateral grids) in COMPAS. When compiling EMS, the `-enable-swan` compile derivative must be used to access this coupling option. In COMPAS, the wave coupling method is more explicit using the following:

```
DO_WAVES      NONE    # No wave coupling
                FILE    # Read wave variables from file
                COMP    # Compute wave variables
                SWAN    # Couple with SWAN (master scheduled)
                SWAN_W  # Couple with SWAN (windows)
```

If wave coupling is not equal to `NONE`, then the wave time-step must be specified:

```
WAVES_DT      2 hours    # How often to couple to waves
```

The wave coupling specification described above (Section 4.21) then apply. If `COMP` wave coupling is specified, then the `WAVE_VARS` keyword need not be present.

The first step in coupling to SWAN is to create ascii files that contain information about the numerical mesh that SWAN will use, and bathymetry for that mesh. These are created during the `-g` option using:

```
SWAN_CONVERT      YES
```

If this is invoked, then the following are created:

```
<infile>.node    # Locations of the mesh nodes
<infile>.ele     # Triangle connectivity
<infile>.bth     # Bathymetry at the nodes
```

Where `<infile>` is the name of the `INPUT_FILE` file specified, without the `.nc` appended (e.g. if `INPUT_FILE = test.nc`, then a file `test.node` is created).

SWAN will then use these files when COMPAS is run using the `-p` mode. When using the `-g` mode, two identical additional files are created, `<infile>.swn` and `INPUT`, which contain the input parameterisation for SWAN. These may be manually edited to change the SWAN configuration, e.g. adding additional output or spectral parameterisation. When using the `-p` mode, only the `<infile>.swn` file is created, containing the current parameterisation information (e.g. restarts), some of which may be required to be copied to `INPUT`. The reason `INPUT` is unaltered using the `-p` option is that the user may have modified the SWAN physics in this file to tune the wave simulation, and this tuning should not be over-written. SWAN runtime information is written to the file `PRINT` during execution.

When coupling to SWAN, the `wave_amp`, `wave_period`, `wave_dir` and `wave_ub` (see above) variables are automatically created by COMPAS. These variables are the variables computed by SWAN and passed back to COMPAS, and will be present in any COMPAS output. The surface elevation, currents and wind computed by COMPAS are passed to SWAN at every coupling interval in return. Additionally, if coupling processes are invoked

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using the WAVES specification (see above), then those variables computed by SWAN (e.g. Stokes drift, radiation stress) are also present in COMPAS output.

Open boundary information is also passed to SWAN by COMPAS. Any boundary intended to be forced with wave information should have the following:

```
BOUNDARY#.OPTIONS WAVES # Specify wave forcing at this boundary
```

Wave forcing data in netCDF or timeseries files, containing wave amplitude, period and direction, should then be included in the DATA for those boundaries, e.g;

```
BOUNDARY#.DATA wave_bdry.nc # Wave forcing data
```

Note that it is not necessary to edit the SWAN INPUT parameter file to specify the boundaries; COMPAS automatically creates and pass all boundary information to SWAN. If a restart file is specified in the COMPAS parameter file, then a RESTART file is also specified in INPUT. Since this is only dumped within SWAN, it is helpful if the restart\_dt is the same as waves\_dt. If the -restart option is invoked, then SWAN will initialize using INITIAL HOTSTART '<swan\_restart\_file>'. Note that this will only be updated in the file <infile>.swn (see above), and is required to be copied to the INPUT file using the -p -restart option.

The SWAN library exists in /main/ext/swan/lib, with source code in /main/ext/swan/src. To re-compile this library, use;

```
make clobber
make com
```

## 4.22 Vertical mixing

SHOC currently supports seven vertical mixing schemes, one of which must be specified for any model run. For more details on these mixing scheme formulations, see section 6, Herzfeld et al (2002). Mixing schemes can be specified by one of the following:

```
# Mixing scheme types
MIXING_SCHEME constant
MIXING_SCHEME csanady
MIXING_SCHEME mellor_yamada_2_0
MIXING_SCHEME mellor_yamada_2_0_estuarine
MIXING_SCHEME mellor_yamada_2_5
MIXING_SCHEME k-e
MIXING_SCHEME k-w
MIXING_SCHEME W88
```

### 4.22.1 Constant

The first scheme simply specifies constant values for the vertical diffusivities for momentum and mass, as follows:

```
# Use the constant mixing scheme
MIXING_SCHEME constant

# Vertical eddy diffusivity
VZ0 0.001

# Vertical diffusivity for tracers
KZ0 0.001
```

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## 4.22.2 Csanady

The vertical momentum diffusion coefficient  $V_z$  and vertical tracer diffusion coefficient  $K_z$  are calculated using a formulation along the lines described in Csanady (1982), equation 6.22b, with modification due to stratification as described by Bowden and Hamilton (1975):

$$V_z = V_{z0} + \alpha_V \mu_* H (1 + 10 R_\eta)^{-1/2}$$
$$K_z = K_{z0} + \alpha_K \mu_* H (1 + 33 R_\eta)^{-3/2}$$

where  $\mu_*$  is the maximum of the surface and bottom friction velocities (to account for both tidal and wind mixing),  $H$  is the depth of water,  $V_{z0}$ ,  $K_{z0}$ ,  $\alpha_V$  and  $\alpha_K$  are constants, and  $R_\eta$  is a Richardson number, dependent on the vertical stratification and vertical velocity shear. The constants  $V_{z0}$  and  $K_{z0}$  specify small background mixing values. This scheme is specified as follows:

```
# Use the Csanady mixing scheme
MIXING_SCHEME    csanady
VZ0              0.00001 # Background viscosity (m2s-1)
VZ_ALPHA        0.0625  # Viscosity coefficient
KZ0              0.00001 # Background diffusivity (m2s-1)
KZ_ALPHA        0.03    # Diffusivity coefficient
```

Csanady (1982) suggests a value of 1/16 (0.0625) for  $\alpha_V$ .

## 4.22.3 Mellor-Yamada 2.0

The Mellor/Yamada level 2 scheme is described (Mellor and Yamada, 1982). This is specified as follows:

```
# Use the Mellor-Yamada level 2 scheme
MIXING_SCHEME    mellor_yamada_2_0
VZ0              1e-5   # Background viscosity
KZ0              1e-5   # Background diffusivity
ZS               0.3    # Surface length scale
```

The Richardson number criterion in this scheme can create grid point noise when background mixing coefficients are imposed due to the flux Richardson number being greater than the critical Richardson number. This can create grid point noise in the temperature solution if a heatflux is imposed. A Shuman filter may be applied to the mixing coefficients to remove this noise by setting:

```
# Smooth Vz and Kz using a Shuman filter
SMOOTH_VzKz      YES
```

## 4.22.4 Mellor-Yamada 2.0 Estuarine

This scheme uses an alternate mixing length parameterisation for the Mellor-Yamada 2.0 mixing scheme (Burchard et al, 1999; Eifler and Schimpf, 1992; Demirov et al., 1998). This is based on a three layer system where surface and bottom mixed layers are intersected by a stably stratified interior layer.



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Required parameters to invoke this mixing scheme are given below.

```
# Use the modified Mellor-Yamada level 2 scheme
MIXING_SCHEME mellor_yamada_2_0_estuarine # scheme type
ZS            0.6             # surface length offset
LMIN         0.01            # Minimum stratified length scale
E            1                # Mixed layer tuning parameter
VZ0          0.001           # Background viscosity
KZ0          0.000001        # Background diffusivity
```

This type of scheme displays better results than Mellor-Yamada-2.0 or  $k-\varepsilon$  for estuarine applications where a three layer system commonly exists. A large degree of flexibility exists in tuning this mixing model, where changes to ZS, LMIN, E, VZ0, KZ0 and density gradient threshold (hardwired as variable `thr` in routine `mld()` in `MY2-0.c`) may affect the solution. The bottom roughness, Z0, also influences the mixing length scale in the bottom mixed layer (ZS is analogous to Z0 for the surface layer). Solutions may be particularly sensitive to the background viscosity and diffusivity. If the mixed layer interfaces are required to be identified using turbulent kinetic energy rather than the density gradient, then the routine `mld()` must be changed to `mldk()` in `MY2_VzKz_mod()` in `mixing/MY2-0.c`. The threshold is given by the variable `thr` in `mldk()` in the same module. Finally, the mixing length scale may be modified by the local turbulent kinetic energy in the mixed layers (Blackadar, 1962) via the flag `lof` in the routine `get_Lscale()` in `mixing/MY2-0.c`. This option is switch off by default (`lof=0`) and can be included by hardwiring `lof=1`. Accounting for local turbulent kinetic energy in the mixed layers generally decreases the mixing length scale in those regions. These hardwire options can generally be left unaltered unless complex tuning of the mixing scheme is required.

## 4.22.5 Mellor-Yamada 2.5

Finally the Mellor-Yamada 2.5 (or `kkl`) scheme (Mellor and Yamada, 1982) includes the transport of turbulence kinetic intensity and turbulence length, and requires four additional tracers. Note length scale and turbulence mixing are diagnostic tracers and do not undergo advection and diffusion.

```
# Use the Mellor-Yamada 2.5 scheme
MIXING_SCHEME mellor_yamada_2_5
VZ0           1e-5           # Background viscosity
KZ0           1e-5           # Background diffusivity
ZS            0.3            # Surface length scale
MIN_TKE       1e-8           # Optional - minimum TKE
MIN_DISS      1e-12          # Optional - minimum dissipation
LMIN          0.17           # Optional - minimum length scale
```

This scheme requires four additional tracers corresponding to turbulent kinetic intensity (`tki`), turbulent kinetic intensity length scale (`tki_l`), turbulence length scale (`lscale`) and turbulence diffusion (`Kq`). These tracers are automatically generated by **SHOC/COMPAS** when the `mellor_yamada_2_5` scheme is chosen, but may be over-riden by manually specifying the following tracers in the parameter file:

```
# Q2 tracer
TRACER2.name      tki
TRACER2.long_name Turbulent Kinetic Intensity
TRACER2.units     m2s-2
TRACER2.fill_value 2.0e-8
TRACER2.valid_range 0 1

# Q2L tracer
TRACER3.name      tki_l
```

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```
TRACER3.long_name   Turbulent Kinetic Intensity Length Scale
TRACER3.units       m2s-1
TRACER3.fill_value  3.4e-9
TRACER3.valid_range 0 1

# Length scale tracer
TRACER4.name        lscale
TRACER4.long_name   Turbulence length scale
TRACER4.units       m
TRACER4.fill_value  0.17
TRACER4.valid_range 0 1e4
TRACER4.advect      0
TRACER4.diffuse     0
TRACER4.diagn       1

# Turbulence mixing tracer
TRACER5.name        Kq
TRACER5.long_name   Turbulence Mixing
TRACER5.units       m2s-1
TRACER5.fill_value  1e-5
TRACER5.valid_range 0 1
TRACER5.advect      0
TRACER5.diffuse     0
TRACER5.diagn       1
```

### 4.22.6 **Harcourt 2015**

The scheme of Harcourt 2015 (Harcourt, 2015) is essentially the same as the Mellor-Yamada 2.5 model but with improvements in the upper ocean to account for the effects of waves via Langmuir turbulence. In particular, it uses different stability functions to the MY2.5 scheme. The Harcourt scheme is invoked the same as for Mellor-Yamada 2.5 except use:

```
MIXING_SCHEME      harcourt
```

### 4.22.7 **k- $\epsilon$**

The k- $\epsilon$  scheme is described by Burchard *et al.* (1998). The specification for this scheme is shown below.

```
# Use the k-e scheme
MIXING_SCHEME      k-e           # scheme type
VZ0                1e-5          # Background viscosity
KZ0                1e-5          # Background diffusivity
MIN_TKE            7.6e-6        # Optional - minimum TKE
MIN_DISS           5.0e-10       # Optional - minimum dissipation
WAVE_ALPHA         100           # Optional - wave a parameter,
                                # Craig & Banner (1994).
```

This scheme requires two additional tracers corresponding to turbulent kinetic energy (tke) and dissipation (diss). These tracers are automatically generated by **SHOC/COMPAS** when the k- $\epsilon$  scheme is chosen, but may be over-ridden by manually specifying the following tracers (e.g. to change fill values or valid ranges) in the parameter file:

```
# tke tracer
TRACER2.name       tke
TRACER2.long_name  Turbulent Kinetic Energy
TRACER2.units      m2s-2
TRACER2.fill_value 7.6e-6
TRACER2.valid_range 0 1
```

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```
# diss tracer
TRACER3.name      diss
TRACER3.long_name Dissipation
TRACER3.units     m2s-3
TRACER3.fill_value 5e-10
TRACER3.valid_range 0 1
```

### 4.22.8 $k-\omega$

The  $k-\omega$  scheme is similar to  $k-\varepsilon$  except it solves for turbulence frequency rather than dissipation (Umlauf et al 2003).

```
# Use the k-w scheme
MIXING_SCHEME      k-w
VZ0                1e-5      # Background viscosity
KZ0                1e-5      # Background diffusivity
ZS                 0.3       # Surface length scale
MIN_TKE            7.6e-6    # Optional - minimum TKE
MIN_DISS           7.27e-19 # Optional - minimum dissipation
```

This scheme requires two additional tracers corresponding to turbulent kinetic energy (tke) and turbulence frequency (omega). These tracers are automatically generated by **SHOC/COMPAS** when the  $k-\omega$  scheme is chosen, but may be over-ridden by manually specifying the following tracers in the parameter file:

```
# tke tracer
TRACER2.name      tke
TRACER2.long_name Turbulent Kinetic Energy
TRACER2.units     m2s-2
TRACER2.fill_value 7.6e-6
TRACER2.valid_range 0 1

# diss tracer
TRACER3.name      omega
TRACER3.long_name Turbulence frequency
TRACER3.units     s-1
TRACER3.fill_value 1.0e-12
TRACER3.valid_range 0 1
```

**COMPAS only:** the functions  $f_{cu}$  and  $f_{cw}$  (see Science Manual, Section 6.8) are currently not implemented in the  $k-\omega$  model, and are assumed to equal 1. This effectively reduces the  $k-\omega$  model to that of W88 (see below).

### 4.22.9 W88

The W88 model of Wilcox (1988) is the same as the  $k-\omega$  model, but using  $f_{cu} = f_{cw} = 1.0$

```
# Use the k-w scheme
MIXING_SCHEME      W88
```

Additional parameters required for the W88 scheme are identical to the  $k-\omega$  scheme.

### 4.22.10 Stability functions.

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The stability function used in the turbulence closure schemes for  $k$ - $\epsilon$ ,  $k$ - $\omega$  and MY2.5 may be specified using `STABILITY_FUNC`. The stability functions available are:

```
STABILITY_FUNC  CANUTO_A  # Canuto et. al. (2001) model A
STABILITY_FUNC  CANUTO_B  # Canuto et. al. (2001) model B
STABILITY_FUNC  GALPERIN  # Galperin et. al. (1988)
STABILITY_FUNC  KANTHA&CLAYSON # Kantha and Clayson (1994)
STABILITY_FUNC  POM       # Mellor (1992)
STABILITY_FUNC  MUNK&ANDERSON # Munk and Anderson (1948)
STABILITY_FUNC  EIFLER&SCHRIMPF # Eifler and Schrimpf (1992)
STABILITY_FUNC  SCHUMANN&GERZ # Schumann and Gerz (1995)
```

## 4.22.11 Waves

The effects of waves can be included in the  $k$ - $\epsilon$ ,  $k$ - $\omega$  and W88 models. This requires the `DO_WAVES` flag to be invoked (see Section 4.23) with feedback to vertical mixing, i.e;

```
WAVES          VERT_MIX          # Wave amplitude used for surface
                                     # length scale in vertical
```

The impact of waves on vertical mixing of momentum follows the Craig and Banner (1994) approach, where the constant  $\alpha$  and scaling factor for significant wave height are set according to:

```
WAVE_ALPHA      100  # Wave factor  $\alpha$ 
WAVE_HEIGHT_FACT 1    # Scaling for significant wave height
```

The default values are those listed above. See Jones and Monosmith (2008) for alternative values.

## 4.23 Horizontal mixing

**SHOC/COMPAS** includes horizontal mixing of momentum and tracers, by specifying a viscosity and diffusivity value respectively. This term is usually included in the momentum equations for stability reasons. The parameters are specified as follows:

```
# Horizontal viscosities are specified separately for the u1
# and u2 momentum equations, but except under special
# circumstances, both values should be the same.
#
# Horizontal viscosity in u1 equation
U1VH          1.0

# Horizontal viscosity in u2 equation (SHOC only)
U2VH          1.0
```

Horizontal diffusion for tracers is also included and is invoked by specifying the diffusivities in the x and y directions in the parameter file via:

```
# Horizontal diffusivity in the x direction ( $\text{m}^2\text{s}^{-1}$ )
U1KH          100
# Horizontal diffusivity in the y direction ( $\text{m}^2\text{s}^{-1}$ ) SHOC only
U2KH          100
```

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Note that since COMPAS only contains one component of velocity applied to all faces, there is no requirement to supply coefficients in the e2 direction.

The horizontal mixing coefficients may be scaled according to the grid size at each cell. This allows reasonable values to be specified for curvilinear grids which encompass a large range of resolutions. Scaling of horizontal mixing coefficients is specified by the parameter `DIFF_SCALE` and may take on the following forms, where  $\Delta x$  is the grid size and  $\Delta x_m$  is the mean grid size (mean grid area for **COMPAS**) :

```
DIFF_SCALE      NONE          # No scaling performed
DIFF_SCALE      LINEAR        # Linear scaling by  $\Delta x / \Delta x_m$ 
DIFF_SCALE      NONLIN        # Non-linear scaling by  $(\Delta x)^2 / (\Delta x_m)^2$ 
DIFF_SCALE      AUTO          # Grid optimized: mixing =  $0.1 \Delta x^2 / \Delta t$ 
DIFF_SCALE      SMAG          # Sets smagorinsky = 0.1 (see below)
```

### COMPAS only:

```
DIFF_SCALE      CUBIC         # Non-linear scaling by  $(\Delta x)^3 / (\Delta x_m)^3$ 
DIFF_SCALE      SCALE2D       # Scale U1VH by IRATIO for 2D mode
DIFF_SCALE      SCALEBI       # Scale U1VH by  $\Delta x^2/8$  for biharmonic
```

The default scaling is `DIFF_SCALE = LINEAR`. If scaling is performed, the value set in the parameter file is relative to the mean grid spacing in the e1 and e2 directions (mean grid spacing is output in the file `setup.txt`).

### COMPAS only:

Both Laplacian (default) and biharmonic momentum mixing are available in COMPAS. These are invoked by:

```
VISC_METHOD     US_LAPLACIAN  # Laplacian viscosity
VISC_METHOD     US_BIHARMONIC # Biharmonic viscosity
```

The relationship between Laplacian viscosity ( $L$ ,  $m^2s^{-1}$ ) and biharmonic ( $B$ ,  $m^4s^{-1}$ ) is  $B = L\Delta^2/8$  (Griffies and Hallberg, 2000) where here we use the edge length squared for  $\Delta^2$ . Biharmonic viscosity can be specified explicitly, or can be a Laplacian value in conjunction with `SCALEBI`, in which case the above scaling is performed internally. For explicit specification, `DIFF_SCALE=CUBIC` is recommended, whereas for Laplacian conversion `DIFF_SCALE=NONLIN SCALEBI`. A combination of Laplacian and bi-harmonic mixing may be specified using:

```
VISC_METHOD     US_LAPLACIAN US_BIHARMONIC frac
```

where `frac` is the fraction ( $0 \leq frac \leq 1$ ) of mixing attributed to the Laplacian scheme and  $(1-frac)$  is the fraction attributed to bi-harmonic mixing. This is applied to viscosity only (an analogous approach for diffusivity is described in Delhez and Deleersnijder, 2007)).

The Smagorinsky diffusion coefficients can be independently invoked on any component of viscosity or diffusivity by setting:

```
SMAGORINSKY     c
```

Where `c` is the value of the constant above (typically `c=0.1`), and any combination of `U1VH`, `U2VH`, `U1KH`, `U2KH` is negative. For example, if the y component of horizontal diffusivity is to be calculated using Smagorinsky diffusion then set;

```
SMAGORINSKY     0.1
U2KH             -100.0
```

Different empirical constants for horizontal viscosity and diffusivity in e1 and e2 directions can be specified using:

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## SHOC only:

```
SMAGORINSKY      v1 v2 k1 k2
```

## COMPAS only:

```
SMAGORINSKY      v1 k1
```

Where  $v_1$  and  $v_2$  are horizontal viscosity coefficients in the  $e_1$  and  $e_2$  directions respectively, and  $k_1$  and  $k_2$  are horizontal diffusion coefficients in the  $e_1$  and  $e_2$  directions respectively. Note that coefficients must be supplied for all components irrespective of whether  $U_{1VH}$ ,  $U_{2VH}$ ,  $U_{1KH}$ ,  $U_{2KH}$  are negative. A base mixing coefficient may also be prescribed using:

## SHOC only:

```
SMAGORINSKY      bv1.v1 bv2.v2 bk1.k1 bk2.k2
```

## COMPAS only:

```
SMAGORINSKY      bv1.v1 bk1.k1
```

Where  $bv_1$ ,  $bv_2$ ,  $bk_1$  and  $bk_2$  are base rates for  $U_{1VH}$ ,  $U_{2VH}$ ,  $U_{1KH}$ , and  $U_{2KH}$  respectively. The fractional part of the number supplied, (e.g.  $v_1$ ,  $v_2$ ,  $k_1$ ,  $k_2$ ) are the Smagorinsky coefficients, where the total mixing is the sum of the base rate and Smagorinsky component, e.g (for SHOC).

```
U1VH              -100.0
U2VH              -100.0
U1KH              -100.0
U2KH              100.0
SMAGORINSKY       100.1 50.2 0.1 0.0
```

In this case  $U_{1VH}$  uses a Smagorinsky coefficient of 0.1 with a base viscosity of  $100 \text{ m}^2\text{s}^{-1}$ ,  $U_{2VH}$  uses a Smagorinsky coefficient of 0.2 with a base viscosity of  $50 \text{ m}^2\text{s}^{-1}$ ,  $U_{1KH}$  uses a Smagorinsky coefficient of 0.1 and  $U_{2KH}$  uses a constant diffusivity of  $100 \text{ m}^2\text{s}^{-1}$ .

If `DIFF_SCALE = SMAG` then Smagorinsky diffusion is set for all horizontal mixing coefficients using a constant `smagorinsky = 0.1`. This constant may be over-ridden if the `SMAGORINSKY` constant is explicitly defined.

If Smagorinsky diffusion is to be used, then an extra tracer is required, which stores the value of the diffusion coefficient. This tracers is automatically generated by SHOC when the smagorinsky diffusion is invoked, but may be over-ridden by manually specifying the following in the parameter file:

```
TRACERn.name      smag
TRACERn.long_name Smagorinsky
TRACERn.units     m2s-1
TRACERn.diagn     1
TRACERn.advect    0
TRACERn.diffuse   0
TRACERn.decay     0.0
TRACERn.svel      0.0
TRACERn.fill_value 0.0
TRACERn.valid_range 0 10000
```

The Smagorinsky distribution can be limited and smoothed prior to use any number of times,  $n$ , using:

```
SMAG_SMOOTH      n
```

The Smagorinsky coefficient is clipped to  $|U_{1VH}|$  for vorticity and  $|U_{1KH}|$  for diffusivity before application.

## SHOC only:

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Note that the horizontal mixing of momentum in **SHOC** follows the full formulation (Herzfeld et al, 2002, section 2.4). A simple formulation exists (e.g. Apel, 1987, p99, Eqn (3.61)) where metric terms are omitted and incompressibility assumptions are made; these can be controlled by the `VISC_METHOD` flag:

```
VISC_METHOD      NONE          # No horizontal viscosity
                  LAPLACIAN     # Full formulation (default)
                  SIMPLE        # Simple formulation
```

The horizontal viscosity routine executed is controlled by function pointers, allowing relatively straightforward inclusion of biharmonic viscosity if required.

## COMPAS only:

The horizontal mixing may be regionalised in COMPAS using:

```
U1VH      region box.bncc 0:v1 1:v2 2:v3..... n:vn
```

where `box.bncc` is a region file with  $n$  regions, and  $v_1$  to  $v_n$  are the viscosity values applied to each region. If one of these values is negative, then Smagorinsky mixing is invoked for that region, where for example a value of -100.1 uses a base rate of 100 and a Smagorinsky constant of 0.1. If the `DIFF_SCALE` is `AUTO`, then  $v_1$  to  $v_n$  are percentages of the optimal value applied to the region; e.g. a value of 50 will use half the optimised value. Examples are:

```
U1VH      region box4.bncc 0:1000 1:-200.1 2:3000 3:500
DIFF_SCALE AREA
```

```
U1KH      region box3.bncc 0:10 1:-50.1 2:10
DIFF_SCALE AUTO
```

## 4.24 Point sources/sinks

A **SHOC** implementation can include an arbitrary number of point sources (or sinks) of water and tracers. These allow the representation of minor inputs of fresh water, or perhaps nutrients, for example. Associated with each point source (or sink) is a time series file (see section 11.1) which specifies inputs in one of two ways. If flows of water are associated with the point source, then the file must specify time varying flow rates ( $\text{m}^3 \text{s}^{-1}$ ), and tracer concentrations ( $\text{kg m}^{-3}$ ). If no water is associated with the point source, then the file specifies tracer input rates (i.e loads or fluxes in  $\text{kg s}^{-1}$ ) only. The file need not specify concentrations or fluxes for all model tracers. Values for those tracers not mentioned in the file are assumed to be zero; the exception is temperature and salinity which are assumed to be equal to the receiving water values if not specified.

Sources of momentum may also be directly input as the source/sink; in this case the `u1` or `u2` velocity (in  $\text{ms}^{-1}$ ) is directly read from file. If flows of water are associated with the point source (i.e. flow rates are specified in the time series file), then the rate of momentum input is:

$$P_i = \rho_i Q v / \rho V \quad (\text{ms}^{-2})$$

where  $\rho_i$  = density of the inflow ( $\text{kg m}^{-3}$ ); if temperature and salinity are associated with the source in the time series file, then the inflow density is computed using the equation of state. If no temperature and salinity are specified, the inflow density is assumed to be equal to the receiving water.  $Q$  is the flow rate ( $\text{m}^3 \text{s}^{-1}$ ) and  $V$  is the velocity associated with the inflow (`u1` or `u2` velocity in  $\text{ms}^{-1}$ ), both specified in the time series file.  $\rho$  is the density of the receiving water and  $V$  is the cell volume, where the vertical depth distribution of the source is used to compute this volume if specified (see below).

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Point source/sinks are specified as follows:

```
# Number of point source/sinks
npointss      2

# Parameters for each point source/sink
pss0.name     Nasty stuff           # Point source/sink name
pss0.location 447174 5442668 0      # Location (X Y Z)
pss0.reference surface             # reference level
pss0.data     nasty.ts              # Time-series file

pss1.name     Nice stuff
pss1.location 450477 5446628 -10
pss1.data     nice.ts
```

The z location (i.e. depth) of the source/sink input may encompass a depth range, with the deepest limit entered first and depths below the surface entered as negative. The tracer input values are equally distributed over the depth range, e.g. for tracers to be distributed between -5m and -10m;

```
pss0.location 147.31 -43.06 -10 -5 # Source between -10 and -5m
```

The (X Y Z) locations may be entered as a time series file and be allowed to vary with time. In this case `pss0.location` contains the name of the time series file and the file must contain the variables X (or x), Y (or y), `z_low` and `z_high`, e.g:

```
pss0.location input_location.ts    # Time dependent input
```

The time series file has variables:

```
## COLUMNS 5
##
## COLUMN1.name time
## COLUMN1.long_name Time
## COLUMN1.units days since 1990-01-01 00:00:00 +10
## COLUMN1.missing_value -99999999
##
## COLUMN2.name X
## COLUMN2.long_name Longitude
## COLUMN2.units Degrees
##
## COLUMN3.name Y
## COLUMN3.long_name Latitude
## COLUMN3.units Degrees
##
## COLUMN4.name z_low
## COLUMN4.long_name Lower depth range
## COLUMN4.units m
##
## COLUMN5.name z_high
## COLUMN5.long_name Upper depth range
## COLUMN5.units m
4382 147.31 -43.06 -10 -5
4392 147.31 -43.06 -20 -15
```

The source/sink may be distributed over multiple cells horizontally and a depth range using (e.g. for SHOC or COMPAS quad meshes):

```
pss0.location -200 -100           # Depth range
pss0.ncells   3                   # Number of entries
```



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```
12 25          #1: (i,j) location
(2,5)-(10,11) #2: (i,j) range
24 27          #3: (i,j) location
```

The indices prescribed for these ranges or locations should conform to the conventions described in Section 4.7.6 for structured and unstructured grids. If a range is given, SHOC/COMPAS will determine only those cells within the range that are wet. Therefore, for example, if a flux were to be input in the bottom layer over the whole domain (approximating a groundwater flux) then (assuming the grid size is 100x100) one would use;

```
pss0.reference  bottom
pss0.location   -1 0
pss0.ncells     1
(0,0)-(100,100)
```

The source/sink may also be distributed over multiple cells horizontally and a depth range using a region file (see Section 4.31.21), where the flux can be specified over one or multiple regions:

```
pss0.location   -200 -100          # Depth range
pss0.region     region.bnc 3 4 ... n # Region file and numbers
```

The flux may be scaled according to:

```
pss0.flag      AREA_WEIGHTED      # Input flux scaled by cell area
pss0.flag      VOL_WEIGHTED        # Input flux scaled by volume of the
                                   # cell mass is delivered into.
```

The reference level is determined by the following (msl by default):

```
pss0.reference  surface          # referenced to the free surface
pss0.reference  msl              # referenced to mean sea level
pss0.reference  bottom           # referenced to the bottom
```

Major inflows or outflows of water (which carry significant momentum) should not be specified in this way, as the point source/sink code ignores momentum input considerations. Such inputs can be specified at open boundaries (see section 4.10.6).

Sometimes the mapping of the point source location from geographic space (lat, long) to index space (i, j) is unsuccessful for the slaves. This is because sometimes custom curvilinear grids have land or outside cells that are not associated with valid coordinate values in the parameter file, and cannot be assigned geographic locations. Also, the precision of the inverse tetragonal bilinear texture map that performs this mapping is sometimes not sufficient to discriminate cell indices for point sources close to cell faces. If the code exits with the warning 'Mismatch between point sourcesinks on master and slave' then refer to the runlog to identify the point source that could not be successfully mapped and redefine its geographic location. Placing point source locations at the cell centre, and avoiding open boundary locations will rectify this problem.

An automated option exists for specifying point sources:

```
pss lon1 lat1 bot1 top1 ..... lonn latn botn topn
```

where lon is the longitude of the source, lat is the latitude of the source, bot is the lower limit in the water column and top is the upper limit for distribution of the input. In this case a tracer passive (kgm-3) is automatically generated and a flux of 1 kgs-1 is input at the location and depth range specified for the duration of the simulation. Multiple locations may be input by including multiple (lon lat bot top) specifications. An example for input of two locations is:

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pss 147.1156 -43.2861 -1 0 147.3715 -43.0141 -10 -5

## 4.24.1 Steady State Approximation

The steady state concentration resulting from a point source input into a grid cell is dependent on the grid size, and can be approximated via the following. Assume a flux  $F_{in}$  ( $gs^{-1}$ ) is input into a cell with dimensions  $(\Delta x, \Delta y, \Delta z)$  in the  $(e_1, e_2, z)$  directions. The  $e_1$  direction only is considered, it is assumed that a constant  $e_1$  velocity of  $u$  ( $ms^{-1}$ ) exists, and the horizontal diffusion is  $A_H$  ( $m^2s^{-1}$ ). The concentration of tracer,  $c$  ( $kgm^{-3}$ ), at time  $t+1$  can be written in terms of mass as:

$$Vc^{t+1} = Vc^t + (\text{source input}) - (\text{mass advected out}) + (\text{mass advected in}) - (\text{mass diffused out})$$

where  $V = \Delta x \Delta y \Delta z$ . Over a time-step  $\Delta t$ , this is equivalent to:

$$c^{t+1}V = c^tV + F_{in}\Delta t - c^{t+1}\Delta y\Delta z u\Delta t + 0\Delta y\Delta z u\Delta t - \Delta y\Delta z A_H \frac{c_i^{t+1} - c_{i-1}^{t+1}}{\Delta x} \Delta t$$

It is assumed that the concentration of tracer advected in ( $c_{i-1}^t$ ) is zero, and that a zero gradient of tracer exists down-current from the source ( $c_{i+1}^t = c_i^t$ ). This is simplified to:

$$V \frac{c^{t+1} - c^t}{\Delta t} = V \frac{\partial c}{\partial t} = +F_{in} - c^{t+1}\Delta y\Delta z u - \frac{\Delta y\Delta z}{\Delta x} A_H c_i^{t+1}$$

At steady state,  $\partial c / \partial t = 0$ , thus steady state concentration,  $c_s$ , is;

$$F_{in} = c_s \Delta y \Delta z u + \frac{\Delta y \Delta z}{\Delta x} A_H c_s$$

or;

$$c_s = \frac{F_{in}}{\Delta y \Delta z u + \Delta y \Delta z A_H / \Delta x}$$

For uniform grid size ( $\Delta x = \Delta y$ ), this reduces to:

$$c_s = \frac{F_{in}}{\Delta x (\Delta y u + A_H)}$$

Therefore, as the horizontal grid size decreases, then the steady state concentration will increase to a limit where horizontal diffusive process dominate.

## 4.25 2D Mode

**SHOC/COMPAS** can be operated in the capacity of a 2D depth integrated model. This is achieved by setting:

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2D-MODE YES

The default is 2D-MODE=NO. The 3D currents are not calculated in this case, resulting in large increases in execution time. The initial tracer distribution is vertically averaged and tracers are subsequently advected using the 2D current (i.e. the water column is assumed to be well mixed). Note that using vertically averaged tracer initial conditions may result in tracer gradients over steep bathymetry, which can in turn lead to spurious baroclinic currents. It is often desirable to use constant temperature and salinity in 2D mode and turn advection and diffusion of these tracers off.

## 4.26 Sigma vertical coordinates

**SHOC/COMPAS** can be configured to use sigma coordinates in the vertical. The formulation follows that of Blumberg and Herring (1987), for curvilinear coordinates. Sigma coordinates are invoked by setting the flag:

SIGMA YES

The default value is SIGMA = NO. In the sigma case, the value of LAYERFACES is equal to the number of sigma levels the model uses, and the distribution of these layers is generated by **SHOC/COMPAS** such that a logarithmic distribution exists at the surface and bottom and a linear distribution in the interior. The input netCDF file for sigma coordinates is the same as that used for 'z' coordinates. **SHOC/COMPAS** linearly interpolates the initial condition for tracers onto the sigma grid (then also applies a smoothing filter in the vertical). The bathymetry is checked to ensure no extreme gradients are encountered; if the bottom slope becomes greater than 0.07 then the bathymetry is smoothed (up to a maximum of 5 passes) until the gradient becomes less than 0.07. The bathymetry may be optionally smoothed n times by setting the flag:

SMOOTHING n

The sigma layers converge at the coast, and this can lead to small vertical grid spacing, which in turn may lead to vertical velocity stability violations. To avoid program termination due to this violation, the sigma system should always be used with STABILITY = SUB-STEP or STABILITY = SUB-STEP-TRACER. Note also that the minimum depth at the coast may need to be increased to maintain stability when using sigma coordinates.

It is recommended to use Smagorinsky diffusivity when using the sigma system so that mixing along sigma surfaces over steep bathymetry does not lead to cross-isobaric exchange in the absence of any motion.

## 4.27 Stability sub-stepping

**SHOC/COMPAS** can invoke several methods to ensure the model remains stable if there exist local violations of the advection scheme stability criteria (which may occur, for example, if the forcing becomes locally large for a short period of time). The advective terms (for 2D, 3D momentum and tracers) are calculated using a sub-timestep based on the maximum Courant number in the grid, and the remaining terms in the model equations are calculated using the original time-step. Note that the original time-step must still obey the CFL condition so as fast moving gravity and internal waves are adequately resolved.

To invoke the sub-time stepping the parameter STABILITY is set in the parameter file as follows;

```
STABILITY SUB-STEP # Sub-stepping stability adjustment
STABILITY SUB-STEP-NOSURF # As for SUB-STEP but excluding
```

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```
                                # the surface layer.
STABILITY  SUB-STEP-TRACER  # Only sub-step for tracers
STABILITY  NONE              # No stability compensation
```

The default option is NONE.

If `STABILITY = SUB-STEP-NOSURF` then the vertical velocity in the surface layer is not included in the maximum sub-step calculation. This is consistent with the original MECO formulation. This option avoids sub-stepping when the surface elevation is only slightly greater than a layer level (the surface layer is thin) and moderately large vertical velocities exist. This condition may occur often and increase the run time ratio due to frequent sub-stepping. However, the model may go unstable in the surface layer in this case, and `HMIN` may need to be increased to maintain stability in the surface layer.

## 4.28 Thin layers

In order to maintain stability when layers become very thin, an option exists whereby if a layer becomes thinner than the parameter `HMIN`, then that layer is merged with the layer below prior to the calculation of the advective terms. The velocity of the merged layer is set to the layer weighted mean of the two layers merged. It is assumed that the velocity is uniform throughout the merged layer, and subsequent to the calculation of the advective terms the merged layer is split back to the original thin layer and associated layer beneath and the thin layer is assigned the updated velocity. This option is initiated via the flag;

```
# Invoke thin layer merging
MERGE_THIN  YES
HMIN        0.05
```

The default is `MERGE_THIN = NO`. The implementation of the thin layer code effectively decreases the `k` coordinate of the surface and resets the velocity of the layer to the mean when thin layers are encountered. The optimum value of `HMIN` generally needs to be derived on a trial and error basis, but generally 2–3% of the surface layer thickness is a good initial estimation.

## 4.29 Particle tracking

Particle tracking is supported in **SHOC/COMPAS**. If an input particle file is specified, then the domain will be seeded with an initial distribution of particles. Particles will be advected and diffused according to parameters defined below. Particles may be reset to their initial locations periodically if requested. If desired, particles can also display a specific vertical movement prescribed within a time series file. This file should contain the vertical velocity as a function of time and space, allowing particle 'swimming behaviour'. Mortality or the loss of a percentage of the remaining particles at every time step can also be prescribed with a time series file. Output files will contain the variable 'ptconc' if particle tracking is invoked; this variable indicates the concentration of particles ( $\text{kgm}^3$ ) for each cell over time. For `ptconc` to be computed the particle mass has to be given as non-zero.

Particle tracking will only occur if an input file is specified. Following is an example particle tracking specification:

```
# Defines the input particle input file. This is a netCDF
# time-series containing the variables 't', 'x', 'y' and 'z'
# for a specified number of particles ('n').
PT_InputFile      pt/pt50000.nc # 50000 particle file.
PT_InputRecord    0             # Dump number to use for initial
                                # particle distribution.

# The output file where the position of all active particles
# will be written.
```

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```
PT_OutputFile      pt.nc

PT_StartTime       1580 days # Start time for PT.
PT_StopTime        1612 days # Stop time.
PT_OutputStep      1 hours   # Output interval.
PT_TimeStep        10 minutes # Update period for recal.
                    # particle positions.
PT_ResetStep       100 days  # How often to reset particles
                    # to the original locations.
PT_KH              1         # Horizontal diffusion coeff.
PT_KZ_MULT         1         # Vertical diffusion coeff.
                    # multiplier
PT_Mass            1         # Particle mass (kg).
PT_Restart         yes      # Interpolate particle positions
                    # from the InputFile onto the grid.

# If true then the particles are not lost when they move
# outside the model domain, instead they 'stick' to the
# boundary and are released when the current changes direction.
PT_StickyBoundary FALSE

# A continuous source of particles along a line is specified
# by a rate of release and the start/end positions of the line.
# These parameters are not mandatory, and multiple sources
# are permitted.
PT_NSource 1
PT_Source0.Rate      20      # Number of particles/second.
PT_Source0.ColourBit 2       # The bit to set in the flag
                    # array when the particle is
                    # seeded. Valid range 2-15.
PT_Source0.StartLocation 280000 7000000 -15 # XYZ of start
                    # position.
PT_Source0.EndLocation 280000 7020000 -25 # XYZ of start
                    # position.
```

An automated option exists for specifying particle tracking:

```
particles lon1 lat1 bot1 top1 ..... lonn latn botn topn
PT_InputFile      pt.nc
```

where *lon* is the longitude of the source, *lat* is the latitude of the source, *bot* is the lower limit in the water column and *top* is the upper limit for distribution of the input. In this case particles are released from that location with a rate of 2 particles / hour for the duration of the simulation. The attributes for the particle source are the same as those listed above.

Multiple locations may be input by including multiple (*lon lat bot top*) specifications. An example for input of two locations is:

```
particles 147.1156 -43.2861 -1 0 147.3715 -43.0141 -10 -5
```

### 4.29.1 Particle Status

The status of a particle may be active / inactive and unlost / lost. Active, unlost particles are the particles that appear in the domain. If a particle exits through a non-sticky boundary then it becomes lost and returns to the inactive pool of particles available to be released at each source. A particle may become lost by moving through an open boundary, or by failing to reach a solid boundary within a certain number of sub-steps (currently hardwired to 110). The

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latter case arises if a large velocity,  $v$ , is normal to a solid boundary which advects the particle into the boundary. The model will attempt to calculate the particles position at a future time by adding the distance,  $s$ , the particle moves over a time interval  $\Delta t$  where  $s = v\Delta t$ . If  $v$  is large then the model successively reduces  $\Delta t$  to resolve the particles position near the boundary. If the position cannot be resolved after 110 reductions of  $\Delta t$  it is assumed the particle has moved through the boundary and becomes lost. An example of this may be a particle settling into the sediments. If settling of a particle is invoked and a particle is attempted to be advected through the bottom, then the vertical diffusion is modified to counteract such effect. Consequently these particles are not lost but remain close to the bottom.

## 4.29.2 Source Colour

Individual sources can be identified by the `ColourBit` parameter, with valid ranges between 2 and 15 (the colourbit values 0 and 1 are used to flag inactive and lost particles). These data are written to the output file making it possible to display particles from multiple sources and identify each individual source by colour.

## 4.29.3 Age

The age of each particle since the release time may be computed. When a particle becomes lost the age is reset to zero. In order to minimise output file size the age of particles are stored as unsigned bytes with values ranging from 0 to 255. The actual age in floating point precision is scaled to this output range via the parameter `AgeLimit`, e.g:

```
PT_AgeLimit          20 days
```

If the `AgeLimit` parameter is present then the age is calculated and scaled age is included in the output file. Scaling is performed linearly such that an age of 0 is scaled to zero, and an age of `AgeLimit` is scaled to 255. Typically `AgeLimit` is the flushing time of the water body. Particles older than `AgeLimit` remain scaled to 255. These scaled ages may be plotted as a colour spectrum for all sources.

A histogram of the distribution of ages in bin sizes of 1 day can be produced. This is in the form of a time series file named 'part\_hist.ts', with the histogram output at a specified interval, e.g;

```
PT_Histogram_DT      1 hour # Output the histogram at 1
                        # hour intervals to the file
                        # part_hist.ts.
```

A region file (see Section 4.31.21) may be used to specify a subsection of the domain within which the mean age of particles is reported:

```
PT_age_region        region.bnc 3
```

In the above case the mean age region will comprise regions 3 of the region file `region.bnc`.

## 4.29.4 Size

A size of particles released from each source may be prescribed using;

```
PT_Source0.Size      1e-4 # Size in m
```

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A growth or decay rate may also be specified for the source and the particle will decay to zero or double in size on this timescale, e.g;

```
PT_Source0.Decay    10 days # Size decreases to zero in 10 days
PT_Source0.Growth   10 days # Size doubles in 10 days
```

When a particle becomes lost the size is reset to `PT_Source0.Size`. A particle threshold size of  $10^{-10}$  is hardwired so that if particles decay to sizes less than this threshold they are flagged as lost. In order to minimise output file size the age of particles are stored as unsigned bytes with values ranging from 0 to 255. The actual size in floating point precision is scaled to this output range via the parameter `SizeLimit`, e.g:

```
PT_SizeLimit        1e-3
```

If the `SizeLimit` parameter is present then the size is calculated and scaled size is included in the output file. For decaying particles scaling is performed linearly such that a size of `SizeLimit` is scaled to 255, and a size of zero is scaled to zero. For growing particles a size of `PT_Source0.Size` is scaled to zero, and a size of `SizeLimit` is scaled to 255. These scaled sizes may be plotted as a colour spectrum for all sources. Particle sizes are only invoked if `SizeLimit` is present, regardless if sizes are set for individual sources. If `SizeLimit` is present and sizes for individual sources are not, then the particle size for each source defaults to zero. In this case all particles will always be flagged as lost, since the particle size is below the threshold of  $10^{-10}$  (see above).

## 4.29.5 Settling

Particles may be prescribed settling velocities as a function of the source, or as a function of position when an initial particle distribution is prescribed (i.e. no sources). For the former, different types of settling behaviour for particles released from each source may be prescribed using:

```
PT_Source0.Stype  NONE      # No settling imposed
                  CONSTANT   # Particles from this source settle with
                              # a constant settling velocity.
                  STOKES     # The stokes settling formula is used to
                              # compute the settling velocity. This is
                              # a function of particle size, density
                              # and water density.
                  DIURNAL    # A periodic settling velocity is used
                              # where the amplitude and period are
                              # prescribed.
                  FILEIN     # Velocity is read from file.
```

For all particles, a negative settling velocity means the particle will sink and a positive velocity will result in a buoyant particle. The `CONSTANT` settling velocity for particles released from each source may be prescribed using:

```
PT_Source0.Svel  1e-3      # velocity in ms-1
```

The `STOKES` settling velocity may be computed using Stokes settling formula:

$$v = \frac{g(\rho_w - \rho_p)d^2}{18\mu} \quad 3.27.1$$

where  $g = 9.81 \text{ (m}^2\text{s}^{-1}\text{)}$  is the acceleration due to gravity,  $\rho_w \text{ (kgm}^{-3}\text{)}$  is the density of surrounding water,  $\rho_p \text{ (kgm}^{-3}\text{)}$  is the density of the particle,  $d \text{ (m)}$  is the particle diameter (size in this case) and  $\mu = 1.4\text{e-3 (kgm}^{-1}\text{s}^{-1}\text{)}$  is the viscosity of water at 20°C. This settling velocity is

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calculated and applied to each particle if the particle size is set (see Section 4.29.4) and the particle density is prescribed:

```
PT_Source0.Dens      1030 # Density in kgm-3
```

Hence if a growth rate is also prescribed, then as the particle grows its diameter increases and therefore settles faster.

The DIURNAL settling velocity is computed using the formula:

$$v = -svel \cos\left(\frac{t}{sper} - \frac{f \cos(t/sper)}{f \cos(t/sper)}\right) \quad 3.27.2$$

where svel is the maximum vertical velocity (ms<sup>-1</sup>) at which the particle will move, t is time and sper is the periodicity of the cosine function, e.g.

```
PT_Source0.Svel  1e-3 # Velocity in ms-1
PT_Source0.Sper  1 day # Periodicity
```

The FILEIN settling velocity is prescribed using an ASCII or netCDF time series file.

```
PT_Source0.File svel.ts # Time series file containing
                        # variable and 'wpt' (ms-1).
```

The settling velocity variable in the file must be named 'wpt'. The settling velocity in the file may be a function of time or space (or both). The spatial coordinates of the source (i.e. StartLocation and EndLocation) are used to interpolate from the file onto the source location if spatial information is contained in the file.

Additionally, particles released from an initial distribution (i.e. without sources specified) may undergo settling as a function of their position in time and space as read from file. This is specified using:

```
PT_w_file   svel.nc # File containing settling variable 'wpt'.
```

The settling velocity variable in the file must be named 'wpt', and the velocity may be a function of time, space or both. Spatially dependent velocities interpolate the settling velocity onto cell centres of the grid, and all particles within a particular cell will adopt that corresponding settling velocity.

NOTE: The differences between invoking PT\_Source0.Svel settling velocity type and the PT\_w\_file are that the former is used for particles released from sources; in which case a continuous source of particles along a line is specified by a rate of release and the start/end positions of the line. Each source must have their own time series file. The second from is used for a release of particles determined with the particle input file, in which case the domain is seeded with an initial distribution of particles. In this case, the settling velocity can vary as a function of time t and space .

### 4.29.6 Swimming

Similar to the settling for particles released from an initial distribution, particles may be assigned horizontal swimming velocities applicable to an initial release. This swimming is read from netCDF file as a function of time and space and is specified via:

```
PT_uv_file  vel.nc # File containing settling variable 'upt'
              # for swimming in the x (east-west)
              # direction and 'vpt' for swimming in the y
              # (north-south) direction.
```



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Note that  $u_{pt}$  and  $v_{pt}$  are velocities are relative to the east-west / north-south axis rather than the numerical grid, and must generally undergo rotation (within the particle tracking code) to be transformed onto the grid.

## 4.29.7 Mortality

Mortality, or the loss of particles expressed as a percentage of active, unlost, particles at every time step, can be prescribed with a time series file (note: this input is not spatially dependent), e.g:

```
PT_mortality_file mp.ts # mortality percentage file
```

The mortality percentage variable in the file must be named 'mpt'.

## 4.30 Grid Refinement

Grid refinement is implemented for **SHOC only**. The concept of this type of refinement is not applicable to unstructured meshes, where equivalent refinement is achieved through use of the weighting function.

Grid refinement, or two-way nesting, allows a fine resolution grid (FRG) to be embedded within a coarse resolution grid (CRG) so that increased resolution is achievable in a sub-region of the whole domain. Although the time-step for the simulation is determined by the smallest grid, savings in computer time is generally achieved by not highly resolving the whole domain. The method used for grid refinement is detailed in Section 14 of the Science Manual.

There must exist at least 2 windows for grid refinement to operate. A grid must be constructed where the number of fine grid cells that comprise one coarse grid cell (i.e. the zoom factor,  $z_f$ ) is an odd number so that cell faces and centers in the coarse grid are coincident with fine grid locations at the coarse-fine boundary. The user must therefore choose a zoom factor and provide a list of the (i,j) locations of the centers of the coarse grid. An example of invoking grid refinement is given below.

```
WINDOWS          2 # At least 2 windows are necessary
GRID_REFINEMENT YES # Turn on grid refinement
ZOOM_FACTOR      3 # Use a zoom factor of 3 so that 3 x 3
                  # = 9 fine grids comprise 1 coarse grid.
ZOOM_POINTS      28 # List the (i,j) locations of the cell
17 9              # centers of the coarse grid. There are
20 9              # 28 (i,j) locations in the list.
23 9
26 9
29 9
32 9
35 9
17 12
20 12
23 12
26 12
29 12
32 12
35 12
17 15
20 15
23 15
```

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```
26 15
29 15
32 15
35 15
17 18
20 18
23 18
26 18
29 18
32 18
35 18
```

The resulting grid for a closed basin test domain is illustrated in Figure 4.29.1.

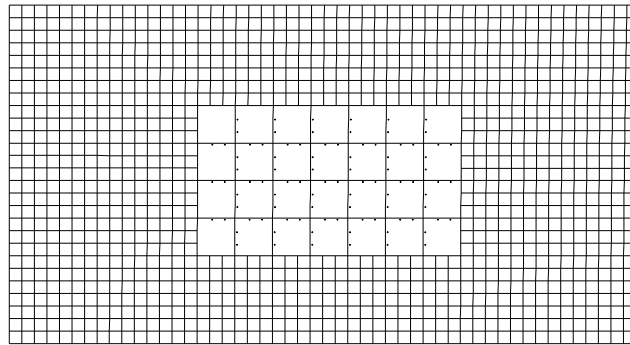


Figure 4.29.1 : Grid refinement example

A section of the grid can be retained at high resolution, or a coarse resolution section can be created using:

```
ZOOM_HR_ZONE      (17,9)-(35,18)    # Set a high resolution zone
or
ZOOM_CR_ZONE      (17,9)-(35,18)    # Set a coarse resolution zone
```

Grid refinement may be turned off using `GRID_REFINEMENT NO`. The default is for no grid refinement. Note that the bathymetry is averaged over the coarse grid cells, hence a new netcdf input file must be created when grid refinement is invoked.

Anisotropic grid refinement may be invoked using:

```
ZOOM_FACTOR_E1    3      # Use a zoom factor of 3 in the e1
                    # direction only.
or
ZOOM_FACTOR_E2    5      # Use a zoom factor of 5 in the e2
                    # direction only.
```

It is possible to construct a grid which has refinement in one direction, e.g. Figure 4.29.2 has a refinement of factor 3 in the e1 direction. This grid may be reverted to a uniform grid using the `PRECONDITIONED` grid refinement option;

```
GRID_REFINEMENT   YES PRECONDITIONED
ZOOM_FACTOR_E1    3
```

This option is useful for reverting a portion of the grid to a uniform grid, while increasing the resolution of another part of the grid (e.g. an upstream river section). In the example below the river section that is three cells wide may be retained at this resolution while the remainder reverted to uniform. Note that the `ZOOM_POINTS` of the cell centres required to be reverted must also be supplied.

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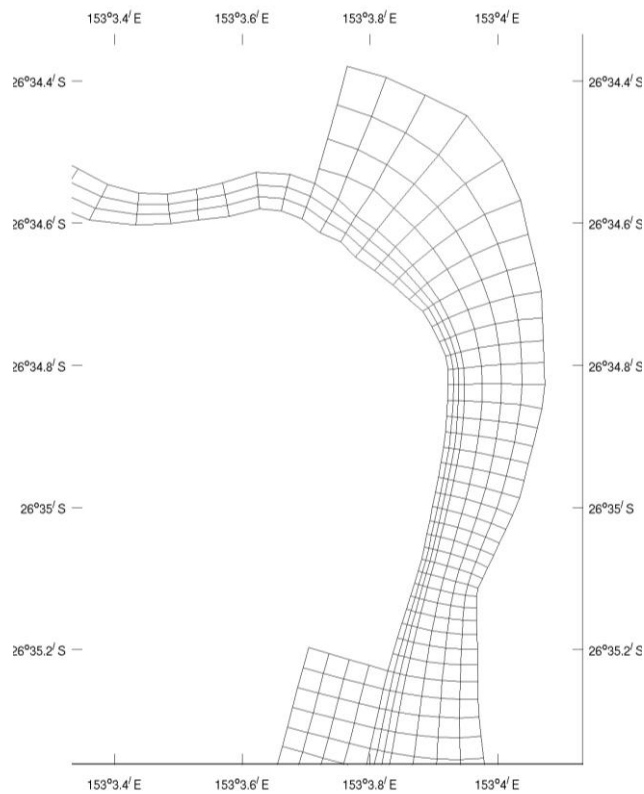


Figure 4.29.2. Grid example with refinement of factor 3 through the river section in the e1 direction.

Usually time-steps are compromised when resolution is increased laterally in a river section of the grid. A grid section where variables are linearly blended can be useful to overcome this. In the case of a river, if variables are blended laterally across the entire width of the river then there will be no transverse flow since the lateral boundary conditions prohibit flow through the solid boundaries. This makes flow along-river only, and the cross-river direction is irrelevant in terms of determining the time-steps for stability. The river effectively consists of a number of independent channels stacked side by side. Tracer exchange between the channels may exist via horizontal mixing. Such a configuration has the benefit of allowing increased resolution of the bathymetric cross section of the river, and aids in constructing river branches. Blending is invoked using:

```
NE1_BLEND 1 # Number of blend areas in the e1 direction
E1_BLEND0 e1s e1e e2s e2e # Start & end e1 coordinates (e1s and
# e1e) and start & end e2 coordinates
# (e2s and e2e) for blend area 0.
```

Or

```
NE2_BLEND 1 # Number of blend areas in the e2 direction
E2_BLEND0 e2s e2e e1s e1e # Start & end e2 coordinates (e2s and
# e2e) and start & end e1 coordinates
# (e1s and e1e) for blend area 0.
```

Examples may be:

```
NE1_BLEND 2
E1_BLEND0 45 47 241 255
E1_BLEND1 45 47 260 298
```

```
NE2_BLEND 1
E2_BLEND0 18 22 100 110
```

## 4.31 Tracer diagnostics

There exist several options for SHOC/COMPAS to generate diagnostics of interest which are subsequently saved to 2D or 3D tracers. These tracers then appear in any specified netCDF output files or timeseries files. Currently these diagnostic tracers include mixed layer depth, heat flux (described in section 4.18), steric height, vorticity, mixing length scale, flushing time, CFL time-steps, tracer fluxes, mean velocity or mean tracer flux and tendencies in the momentum balance. Specification of these diagnostics is described below.

### 4.31.1 Tracer Fluxes

The advective and vertical diffusive flux of a specified tracer may be calculated. The flux calculation of a tracer is invoked by specifying a tracer name, e.g;

```
CALC_FLUXES          salt      # Name of tracer for flux calculation
```

#### COMPAS only:

For COMPAS, the directions through cell faces vary according to the shape of the polygon (rectangular, hexagonal etc), hence the face directions must be additionally supplied:

```
CALC_FLUXES      salt  1 3  # salt fluxes through faces 1 and 3 of
                        # the cell polygon.
```

To disable the flux diagnostic, set the flux diagnostic to `NONE`. This diagnostic requires the specification of tracers representing the advective fluxes in `e1`, `e2` and `z` directions, and a diffusive flux in the `z` direction. These tracers are automatically generated by SHOC/COMPAS when the `CALC_FLUXES` flag is invoked, but may be over-ridden by manually specifying any of the following tracers in the parameter file:

```
TRACER?.name          flux_e1
TRACER?.long_name     Advective flux e1
TRACER?.units         kgs-1
TRACER?.diagn         1

TRACER?.name          flux_e2
TRACER?.long_name     Advective flux e2
TRACER?.units         kgs-1
TRACER?.diagn         1

TRACER?.name          flux_w
TRACER?.long_name     Vertical advective flux
TRACER?.units         kgs-1
TRACER?.diagn         1

TRACER?.name          flux_kz
TRACER?.long_name     Vertical diffusive flux
TRACER?.units         kgs-1
TRACER?.diagn         1
```

Fluxes are calculated at each grid cell via:

$$\begin{aligned} flux\_e1 &= u_1 T N_2 \Delta x \\ flux\_e2 &= u_2 T N_1 \Delta x \\ flux\_w &= w T N_1 \Delta z \end{aligned}$$

$$flux_{kz} = K_z \frac{\partial T}{\partial z} \Delta h_1 \Delta h_2$$

where  $u_1$  and  $u_2$  are the velocities in the  $e_1$  and  $e_2$  directions respectively (form compas only the  $e_1$  direction exists, and is non-directional),  $T$  is the tracer concentration at the cell face,  $\Delta h_1$  and  $\Delta h_2$  are the grid metrics at the cell faces and  $\Delta z$  is the layer thickness.

#### 4.31.2 Means

The cumulative moving mean of certain variables may be calculated via the flag `MEAN`. Options are:

```

MEAN      NONE      # No mean velocity calculation
MEAN      VEL3D     # Mean 3D velocity calculation
MEAN      VEL2D     # Mean 2D velocity calculation
MEAN      ETA       # Mean sea level calculation
MEAN      TS        # Mean temperature and salt
MEAN      KZ        # Mean vertical diffusivity calculation
MEAN      WIND      # Mean wind calculation
MEAN      VOLFLUX   # Mean volume flux calculation
MEAN      TENDENCY  # Mean momentum tendencies
MEAN      FLUX      # Mean tracer flux calculation
MEAN      TIDAL     # Means calculated over a tidal cycle
MEAN      TRANSPORT # Tracers advected with mean velocities
MEAN      <trname> # Mean of 2D or 3D tracer in the tracer list
MEAN_DT   1 day    # Averaging period
    
```

A `MEAN_DT` value of `SEASONAL`, `MONTHLY` or `DAILY` is also supported for seasonal, monthly or daily means respectively. These quantities may be written to file using the `SEASONAL`, `MONTHLY` or `DAILY` netCDF file output time increments (see Section 4.32.6); here the mean dumped at the start of the season corresponds to the mean computed over the previous season (ditto for months, e.g. output on 1 March corresponds to a mean computed over the previous summer for `SEASONAL` means and means computed over February for `MONTHLY` means). Additionally, if `SEASONAL` `MONTHLY` or `DAILY` means are written to netCDF file at the same interval as `MEAN_DT` (e.g. `file0.tinc = SEASONAL` with `MEAN_DT = SEASONAL`) then the mean will be cumulative over the season for successive years (e.g. for a multi-year run, the mean dumped to file on 1 March will be that of all previous summers for `SEASONAL` means, that of all previous Februaries for `MONTHLY` means and that of the same day for `DAILY` means). If the mean is not desired to be cumulative in this fashion, then the mean for each season of each year should be saved using `MONTHLY` dumps for `SEASONAL` means.

The means computed are cumulative running means, where the value present in the output file is the mean from the start of the computation period to that point in time. When the `MEAN_DT` time is reached, the mean values are reset to zero and the running mean begins again. If a restart is performed, the running mean values are correctly populated from the restart file, and the time counter for the means is read from the global attributes of the netCDF file containing the means. Note: *if the INPUT\_FILE contains a global attribute `mean_c` that is not consistent with the mean calculation, the mean quantities may be compromised.* The time counter can also be explicitly set using:

```

MEANS_OFFSET <time> # e.g. <time> = 10 days is the time
                # since the last reset occurred.
    
```

The default is no calculation of mean quantities. If the `VEL3D` flag is invoked, then three additional tracers corresponding to the mean 3D velocity in the  $e_1$ ,  $e_2$  and  $z$  directions must exist. These tracers are automatically generated by SHOC/COMPAS when the `MEAN` flag is

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invoked, but may be over-ridden by manually specifying any of the following tracers in the parameter file:

```
TRACER?.name          ulmean
TRACER?.long_name     Mean u1 velocity
TRACER?.units         ms-1
TRACER?.diagn        0
```

```
TRACER?.name          u2mean
TRACER?.long_name     Mean u2 velocity
TRACER?.units         ms-1
TRACER?.diagn        0
```

```
TRACER?.name          wmean
TRACER?.long_name     Mean w velocity
TRACER?.units         ms-1
TRACER?.diagn        0
```

If the `FLUX` flag is invoked then the mean values of the tracer fluxes (section 4.31.1) are calculated for the respective flux tracers, hence additional flux tracers must also be specified. If the `TENDENCY` flag is set then the contributions to the momentum balance are averaged for the respective tendency tracers (see section 4.31.11). The `VEL2D` and `WIND` flags generate means of the 2D velocity and wind-field respectively. These averages are stored in 2D tracer arrays which are automatically created by SHOC/COMPAS when these flags are invoked.

If the `TIDAL` flag is present then the mean values are calculated over a tidal period. To do this SHOC/COMPAS attempts to find the maximum sea level in a 24 hour period at each point in the grid, then proceeds to average until the next maximum sea level is encountered at that point. Note that this may result in the exact averaging period differing throughout the grid (e.g. if a modulation of tidal phase exists across the grid). After each output dump event the mean arrays are reset. When invoking this option, the file output interval should be set to around 3 times the dominant tidal period (i.e. 3 days for diurnal tides) since **SHOC/COMPAS** may require up to 1 tidal period to locate the start of the averaging period, 1 tidal period to calculate the mean and 1 tidal period for safety to avoid any overlap of the tidal averaging into the next cycle.

The `TRANSPORT` flag allows tracers to be advected using the mean 3D velocity field. If the averaging period is set so as to filter out higher frequency oscillation (e.g. the tide) then these velocities represent the residual current field which may be much smaller than the instantaneous current. In these cases the time-step for tracers may be dramatically increased, resulting in an improvement in execution speed.

The mean fields appear in the output file and time-series files as an additional tracer. Note that if tracers are set as diagnostic tracers (`TRACER?.diagn = 1`) then SHOC/COMPAS initializes the tracer to zero every time the tracer is dumped to file. Since mean tracers sum contributions over the averaging period, always set `TRACER?.diagn = 0` when manually defining mean tracers.

### 4.31.3 *Mixed Layer Depth*

The mixed layer depth may be computed using a threshold on the vertical density profile (currently hardwired to  $-0.01 \text{ kgm}^{-2}$  in the routine `mld()`) or threshold on the turbulent kinetic energy (hardwired to  $10^{-5} \text{ Wkg}^{-1}$  in the routine `mldk()`; see Burchard et al (1999), p26). Obviously the latter will only function if the mixing scheme calculates TKE (e.g. Mellor-Yamada 2.5,  $k-\epsilon$ ,  $k-\omega$ ). Finally, the mixed layer may be computed as the level where water temperature attains a value of  $0.1 \times \text{SST}$ . The mixed layer option is invoked by setting the flag:

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```
MIX_LAYER    NONE          # Default : no mixed layer calculation
MIX_LAYER    DENS_MIX     # Density gradient computation
MIX_LAYER    TKE_MIX      # TKE threshold computation
MIX_LAYER    TEMP_MIX     # Temperature (0.1 x SST) computation
```

The default is no mixed layer calculation. If this flag is invoked, then a 2D tracer is automatically created to store the mixed layer depth in units of metres.

## 4.31.4 Flushing Time

The time required to flush a sub-region of the model domain may be calculated using the flushing diagnostic. The flushing time is defined as the time for the total mass in the sub-region to decrease by a factor of 1/e (~38%, i.e. the e-folding time). This representation of the flushing time assumes that tracer is well mixed in the sub-region and the total mass is assumed to decrease exponentially according to:

$$M(t) = M_0 e^{-t/\tau}$$

where  $M_0$  is the initial mass and  $\tau$  is the flushing time scale (Tartinville et al, 1997). When  $M = M_0/e$  then  $t = \tau$ , hence the flushing time can be recovered. This diagnostic is invoked by specifying the tracer number of a flushing tracer, e.g.

```
FLUSHING_TR          YES          # Invoke flushing diagnostic
FLUSHING_DT          30 minutes   # Output interval.
FLUSHING_PTS         3            # Grid cells defining the
15 5                  # flushing region.
16 5
17 6
```

The flushing region may also be distributed over multiple cells horizontally using blocks (see Section 4.7.6 for structured / unstructured indexing conventions), e.g. for a structured grid:

```
FLUSHING_BLOCKS      3            # Number of entries
12 25                #1: (i,j) location
(2,5)-(10,11)        #2: (i,j) range
24 27                #3: (i,j) location
```

If a range is given, SHOC will determine only those cells within the range that are wet. A region file (see Section 4.31.21) may also be used to specify the flushing region:

```
FLUSHING_REGION      region.bnc 3 4 ... n # Region file and numbers
```

Invoking the flushing tracer diagnostic will automatically create a tracer named 'flush' with the following attributes:

```
TRACER5.name         flush
TRACER5.long_name    Flushing tracer
TRACER5.units        mgL-1
TRACER5.fill_value   0.0
TRACER5.valid_range  0 1
TRACER5.diagn        0
TRACER5.advect       1
TRACER5.diffuse      1
```

The flushing tracer concentration is automatically initialised to 1.0 within the flushing region and zero elsewhere during startup. The flushing region is defined by listing a series of index locations, whose total number is `FLUSHING_PTS`. The index locations of any sub-region of the structured domain may be retrieved using the 'marked' facility in `jvismeco`. The total

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mass in the flushing region is printed to the time-series file 'flushing.ts' at the time interval `FLUSHING_DT`. This time-series file contains the total mass in the flushing region, the normalised mass (i.e. the ratio of total mass : total initial mass) and the flushing time. The flushing (e-folding) time can be calculated from this output, i.e. the time when the normalised mass falls below  $1/e$ . When this occurs the flushing time variable in the time-series file will assume this time value. Subsequent to this flushing time being reached, the initial concentration is re-set after a further two flushing times.

### 4.31.5 Age tracer

An age tracer may be specified, where the value of the age tracer is indicative of the time the tracer has spent in a defined region. The region may be defined using a list of points, blocks or a region. If the tracer lies within the specified region, it is incremented at a rate of  $1 \text{ day}^{-1}$ , and outside the specified region it is not incremented. To specify the region using a list of points use:

```
AGE_TR          3      # Number of points in the list
18 5            # Points list.
19 5
20 6
```

Blocks can also be used to specify the region (see Section 4.7.6 for structured / unstructured indexing conventions), e.g. for a structured grid;

```
AGE_TR          3      # Number of points in the list
12 25           #1: (i,j) location
(2,5)-(10,11)   #2: (i,j) range
24 27           #3: (i,j) location
```

To specify the region using a region file (see Section 4.31.21);

```
AGE_TR  region.bnc 3 4 ... n # Region file and numbers
```

In the above case the age region will comprise regions 3 4 ... n of the region file `region.bnc`.

A depth range for the age region may be specified using:

```
AGE_RANGE  top_depth  bot_depth
```

If this is absent, the region encompasses the whole water column. The age tracer is named 'age' in output files and is generated automatically. Alternatively the age tracer may be manually specified in the tracer list.

### 4.31.6 Steric Height

The steric height within a domain can be calculated by specifying the flag:

```
STERIC_HEIGHT          lnm # Level of no motion
```

Where `lnm` is a number corresponding to the level of no motion used in the steric height calculation. If this flag is set, a 2D tracer is automatically created to store the steric height output with units of metres. Steric height is defined as the geopotential anomaly divided by the acceleration due to gravity (e.g. Godfrey and Ridgeway, 1985). Geopotential anomaly is defined as:



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$$\Delta\Phi = \int_{p_1}^{p_2} \delta l$$

where  $p_1 > p_2$  are any pressure levels and  $\delta$  is the anomaly of specific volume where:

$$\delta = \alpha(S, T, p) - \alpha(S_0, p)$$

with  $\alpha = 1/\rho$  = the specific volume,  $S$ =salinity,  $T$ =temperature and  $p$ =pressure. For the steric height diagnostic the pressure  $p_1$  is taken as the pressure at the level of no motion ( $l_{nm}$  where it is assumed velocity=0) and  $p_2$  is taken as the sea surface.

The geostrophic current relative to the level of no motion in the  $e_1$  direction is then given by:

$$u_g = \frac{g}{f} \frac{\partial s_h}{\partial e_1}$$

where  $s_h$  is the steric height (m) and  $f$  is the Coriolis parameter. The gradient of steric height in the  $e_2$  direction gives geostrophic velocity in the  $e_2$  direction. If  $l_{nm} = 0$  then the steric height diagnostic is not calculated.

### 4.31.7 Vorticity

The vorticity may be calculated and stored in 2-D tracer diagnostic variables by invoking the flag:

VORTICITY <string>

Where <string> is a string containing ABSOLUTE, RELATIVE, POTENTIAL, TENDENCY or NONE, with;

```
ABSOLUTE # absolute vorticity saved to tracer 'abs_vor' (s-1)
RELATIVE # relative vorticity saved to tracer 'rel_vor' (s-1)
POTENTIAL # potential vorticity saved to tracer 'pot_vor' (m-1s-1)
TENDENCY # barotropic tendency terms saved to tracers (see below)
NONE # no vorticity calculations performed
```

Relative vorticity is defined as:

$$\zeta = \frac{1}{h_1} \frac{\partial h_2}{\partial e_1} - \frac{1}{h_2} \frac{\partial h_1}{\partial e_2}$$

and absolute vorticity =  $\zeta + f$  where  $f$  is the Coriolis parameter (equivalent to planetary vorticity). Potential vorticity is then defined as (Gill, 1982, p232):

$$\Pi = \frac{f + \zeta}{H + \eta} = \text{constant}$$

i.e. potential vorticity is equal to absolute vorticity divided by water depth and is conserved following the flow. Relative vorticity is calculated using the depth averaged velocity to provide a 2-dimensional vorticity diagnostics which are saved to the 2D tracers `abs_vor`, `rel_vor` and `pot_vor`.

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The 2D relative vorticity equation is described in the SHOC Science Manual. The contributing terms to this balance are automatically generated and saved as 2D tracers if `TENDENCY` is specified. These tracers have the following attributes:

<code>rv_drvdt</code>	Temporal rate of change of relative vorticity (production of relative vorticity) ( $s^{-2}$ ).
<code>rv_nonlin</code>	Nonlinear contribution to relative vorticity. Includes advection, metric terms and diffusion ( $s^{-2}$ ).
<code>rv_beta</code>	Transport across contours of constant planetary vorticity ( $s^{-2}$ ).
<code>rv_strch</code>	Vortex stretching, i.e. transport across $f/H$ contours ( $s^{-2}$ ).
<code>rv_jebar</code>	Joint Effect of Baroclinicity And Relief ; the contribution of the mass field to vorticity production ( $s^{-2}$ ).
<code>rv_wsc</code>	Production of vorticity due to wind stress curl and the interaction of the wind stress with the gradient of topography ( $s^{-2}$ ).
<code>rv_bsc</code>	Dissipation of vorticity due to bottom stress curl and the interaction of the bottom stress with the gradient of topography ( $s^{-2}$ ).

### 4.31.8 *Mixing Length Scale*

The mixing length scale is saved to the diagnostic tracer `lscale` if this tracer is defined, e.g. if :

```
TRACER?.name          lscale
TRACER?.long_name     Mixing length scale
TRACER?.units         m
TRACER?.fill_value    0.0
TRACER?.valid_range   0 100
TRACER?.diagn         1
TRACER?.advect        0
TRACER?.diffuse       0
```

is defined then this tracer will be populated with the mixing length scale calculated in the Mellor-Yamada 2.0  $k-\epsilon$  or  $k-\omega$  mixing schemes.

### 4.31.9 *CFL Time-steps*

The Courant-Friedrichs-Levy stability time-step (see section 2.7 Herzfeld et al, 2002) for barotropic and baroclinic modes, the Courant and Lipschitz stability criterion and horizontal diffusion stability limit may be calculated at every grid point and time-step. The CFL time-steps are saved to 2D diagnostic tracers in units of seconds. This is useful to precisely set the time-steps used by the model. An option exists to include the vertical advection Courant constraint (i.e.  $w\Delta t/\Delta z < 1$ ) The minimum time-step for the simulation is printed to the diagnostic file 'diag.txt' (section 4.33). Options exist to adaptively alter the time-step used by the model to the CFL condition. This process is performed for a user defined time period. The CFL diagnostics are invoked via:

```
CFL    PASSIVE          # CFL calculated and output to tracers

      ACTIVE           # 2D and 3D time-steps are set to the minimum
CFL_DT <x> days      # CFL time-steps at x days

      ACTIVE3D        # 3D time-step is set to CFL step whenever
CFL_DT <x> days      # the CFL step becomes less than the 3D step
                    # and the simulation time is less than x
                    # days.
      |WVEL           # By or-ing WVEL to the above flags the
                    # vertical advection stability constraint
```

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# (i.e. Courant number < 1) is included in  
# the stability calculation.

An example of the CFL stability diagnostic is:

```
CFL          AVTIVE3D|WVEL
CFL_DT       20 days
```

Tracer names in output files for these stability limits are:

```
cfl12d      # 2D CFL stability time-step
cfl13d      # 2D CFL stability time-step
courant      # Courant stability time-step
courant_no  # Courant number
lipschitz   # Lipschitz stability time-step
diffstab    # Horizontal diffusion stability time-step
```

## 4.31.10 Heat Flux Diagnostics

If the heat flux is calculated (see section 4.18) then the components of the heat flux are automatically written to 2D diagnostic tracers. The attributes of these tracers are listed below.

Heat Flux Diagnostic Attributes

2D Tracer Name	Description	Units
swr	Short wave radiation	Wm <sup>-2</sup>
lwr	Long wave radiation	Wm <sup>-2</sup>
shf	Sensible heat flux	Wm <sup>-2</sup>
lhf	Latent heat flux	Wm <sup>-2</sup>
nhf	Net heat flux	Wm <sup>-2</sup>

## 4.31.11 Momentum Balance Tendencies

The contribution to each of the terms in the 3D momentum balance may be saved to 3D diagnostic tracers. These variables will then appear in any specified output netCDF and time-series files. These diagnostics are invoked by invoking the flag:

```
MOM_TEND     YES
```

This diagnostic automatically generates the following tracers (with units ms<sup>-1</sup>) representing the momentum tendencies when the MOM\_TEND flag is invoked

```
u1_adv       u1 advective tendency
u1_hdif      u1 horizontal diffusion tendency
u1_vdif      u1 vertical diffusion tendency
u1_btp       u1 barotropic pressure gradient tendency
u1_bcp       u1 baroclinic pressure gradient tendency
u1_cor       u1 Coriolis tendency
u1_sto       u1 Stokes Coriolis and vortex forces

u2_adv       u2 advective tendency
u2_hdif      u2 horizontal diffusion tendency
u2_vdif      u2 vertical diffusion tendency
u2_btp       u2 barotropic pressure gradient tendency
u2_bcp       u2 baroclinic pressure gradient tendency
u2_cor       u2 Coriolis tendency
u2_sto       u1 Stokes Coriolis and vortex forces
```

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## COMPAS only:

The `u1_` and `u2_` components of the momentum balance for COMPAS represent tendencies in the east (u) and north(v) directions.

The Stokes tendencies are only generated for `waves = STOKES` (see Section 4.20).

```
mom_balance A code representing the maximum term in the momentum
              balance, where the code:
              1 = advection
              2 = horizontal diffusion
              4 = vertical diffusion
              8 = Coriolis
              16 = barotropic pressure
              32 = baroclinic pressure
```

The sum of the momentum diagnostic tracers for `u1/u` or `u2/v` velocity is equal to the total change in velocity over the time-step. If the `MOM_TEND` flag is set to `NO` but any of the above tracers are included in the parameter file, then the momentum tendency corresponding to just that tracer will be calculated. This diagnostic will not work in the 2D mode.

### 4.31.12 Tracer Tendencies

Tracer tendencies can be saved to 3D diagnostic tracers using:

```
TRA_TEND <tr_name>
```

where `<tr_name>` is the name of a tracer in the tracer list for which the tendencies are to be computed. The units of the tendencies are the same as that of the nominated tracer, and the following diagnostic tracers are automatically generated;

```
<tr_name>_adv          advective and horizontal diffusive tendency
<tr_name>_vdif         vertical diffusive tendency
<tr_name>_ncon         non-conservative tendency
```

### 4.31.13 Selective Momentum Calculations

The terms in the 2D and 3D momentum balance (i.e. advection, horizontal diffusion, vertical diffusion, barotropic pressure gradients, baroclinic pressure gradients and Coriolis) may be selectively omitted from the momentum calculation via the flags:

```
U1_OMIT <string>
U2_OMIT <string>
U1AV_OMIT <string>
U2AV_OMIT <string>
```

## COMPAS only:

Only the `U1_OMIT` or `U1AV_OMIT` flags are required for COMPAS.

Where `<string>` is a string containing `ADVECT`, `HDIFF`, `VDIFF`, `PRESS_BT`, `PRESS_BC` or `CORIOLIS`. This facility is useful for diagnosing the source of instability in the model. The baroclinic contribution is only omitted from the 2D mode if it is also omitted from the 3D mode.

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## 4.31.14 Diagnostic numbers

A variety of diagnostic numbers can be computed at every time-step. These are invoked via the NUMBERS diagnostic as follows:

NUMBERS <string>

Where <string> is a string containing BRUNT, INT\_WAVE, RICHARDSON\_GR, RICHARDSON\_FL, REYNOLDS, FROUDE, ROSSBY\_IN, ROSSBY\_EX, SOUND, SHEAR\_V, BUOY\_PROD, SHEAR\_PROD, SPEED\_2D, SPEED\_3D, SPEED\_SQ, SIGMA\_T, UNIT, EKMAN\_PUMP, CONTINUITY or ALL\_NUMBERS. These diagnostics are computed as follows:

BRUNT : Brunt-Vaisala (buoyancy) frequency (s<sup>-1</sup>), N, where;

$$N^2 = -\frac{g}{\rho_0} \frac{\partial \rho_0}{\partial z} \quad (\text{Gill, 1982, eqn 6.4.9}).$$

INT\_WAVE : Internal wave speed (ms<sup>-1</sup>). For constant N the n<sup>th</sup> mode long wave phase speed is approximated by:

$$c_n = \frac{NH}{n\pi} \quad (\text{Gill, 1982, eqn 6.11.1})$$

where H is the water depth. Mode 1 internal waves are produced as this diagnostic.

RICHARDSON\_GR : Gradient Richardson number (dimensionless), where;

$$Ri = \frac{N^2}{(\partial u / \partial z)^2} \quad (\text{Dyer, 1997, eqn 4.2})$$

If Ri > 0 flow is stable

Ri = 0 flow is neutral

Ri < 0 flow is unstable

RICHARDSON\_FL : Flux Richardson number (dimensionless), where;

$$Rf = \frac{K_z Ri}{V_z} \quad (\text{Dyer, 1997, p54})$$

REYNOLDS : Reynolds number (dimensionless), where;

$$Re = \frac{uL}{\nu} \quad (\text{Dyer, 1997, eqn 4.1})$$

The diagnostic produced uses layer thickness for D and vertical eddy viscosity, V<sub>z</sub>, for the kinematic viscosity, ν.

FROUDE : Interfacial Froude number (dimensionless) where;

$$Fr = \frac{u^2}{c_n^2} \quad (\text{Dyer, 1997, p42})$$

The internal wave speed used is that from the INT\_WAVE diagnostic.

If Fr < 1 flow is sub-critical

Fr = 1 flow is critical

Fr > 1 flow is super-critical.

Note, Dyer (1997, p43) states critical flow occurs at Fr = 0.33 for continuous stratification.

ROSSBY\_IN : Internal Rossby radius (m), where:

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$$R\phi = \frac{c_n}{|f|} \quad n = 1, 2, 3, \dots \quad (\text{Gill, 1982, eqn 7.5.4})$$

The mode 1 internal Rossby radius is supplied as the diagnostic.

ROSSBY\_EX : External Rossby radius (m), where:

$$R\phi = \frac{\sqrt{gH}}{|f|} \quad (\text{Gill, 1982, p 207})$$

SOUND : Speed of sound given by:

$$c = c(S, T, Z) = c_o + \alpha_o(T - 10) + \beta_o(T - 10)^2 + \gamma_o(T - 18)^2 + \delta_o(S - 35) + \varepsilon_o(T - 18)(S - 35) + \zeta_o |z| \quad (\text{Apel, 1887, eqn 7.19})$$

where  $c_o = 1493.0$ ,  $\alpha_o = 3.0$ ,  $\beta_o = -0.006$ ,  $\gamma_o = -0.04$ ,  $\delta_o = 1.2$ ,  $\varepsilon_o = -0.01$  and  $\zeta_o = 0.0164$ . This equation is believed to be accurate to within  $\pm 0.2 \text{ ms}^{-1}$ . Sound channels are defined as the depth where a change of sign in the sound speed gradient occurs, i.e. where the curvature of the sound profile is equal to zero. The vertical representation of all variables in SHOC occupies discrete vertical layers arranged at variable depths, usually with higher resolution at the surface (and being dependent on maximum water depth). Therefore, the speed of sound is also only provided at discrete depths. In SHOC the sound channels are simply computed from a linear interpolation between two layers where the gradient of sound speed changes. The gradient of sound speed is computed with a 4<sup>th</sup> order approximation:

$$\frac{\partial c}{\partial z} \sim \frac{dc}{dk} = \frac{4c_{k+1}^t - c_{k-1}^t}{3 \cdot 2h} - \frac{1c_{k+2}^t - c_{k-2}^t}{3 \cdot 4h}$$

Where  $C$  is the sound speed,  $k$  is the vertical index and  $h$  is the layer thickness. Layers  $k$  and  $k-1$  are identified where  $\frac{dc}{dk} / \frac{dc}{dk-1} < 0$ , and the sound channel depth,  $D_k$ , is then given by:

$$D_k = d_k - \frac{dc}{dk} (d_{k-1} - d_k) / \left( \frac{dc}{dk-1} - \frac{dc}{dk} \right)$$

where  $d_k$  is the depth of layer  $k$ . Sonic depth and sound channel depths are provided along with the speed of sound when this diagnostic is invoked.

SHEAR\_V : The vertical velocity shear magnitude ( $\text{s}^{-1}$ ), defined by:

$$\left| \frac{\partial v}{\partial z} \right| = \sqrt{\left( \frac{\partial u_1}{\partial z} \right)^2 + \left( \frac{\partial u_2}{\partial z} \right)^2}$$

BUOY\_PROD and SHEAR\_PROD : These diagnostics are assigned from the closure scheme used, where buoyancy production,  $B$  ( $\text{m}^2\text{s}^{-2}$ ), and shear production,  $P$  ( $\text{m}^2\text{s}^{-2}$ ), are defined by (e.g. Burchard et al, 1998, eqn. 9):

$$P = V_z \left[ \left( \frac{\partial u_1}{\partial z} \right)^2 + \left( \frac{\partial u_2}{\partial z} \right)^2 \right]$$

$$B = K_z N^2$$

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where  $N^2$  is the Brunt-Vaisala frequency (see above). Note that these diagnostics are extracted directly from the mixing scheme used, and may differ for different schemes (e.g. some schemes add a correction for internal wave shear to P).

SPEED\_2D : Depth averaged current speed ( $\text{ms}^{-1}$ ), given by:

$$|U| = \sqrt{U_1^2 + U_2^2}$$

Current direction is also supplied.

SPEED\_3D : Three dimensional current speed ( $\text{ms}^{-1}$ ), given by:

$$|u| = \sqrt{u_1^2 + v_1^2 + u_2^2 + v_2^2}$$

SPEED\_SQ : Three dimensional current speed squared ( $\text{m}^2\text{s}^{-2}$ ), given by:

$$u^2 = u_1^2 + v_1^2 + u_2^2 + v_2^2$$

Current direction is also supplied.

WIND\_CD : The momentum drag coefficient given by the function in Section 4.14.

OBC\_PHASE : Open boundary phase speed for elevation, as given by radiation conditions in Science Manual Section 4.6. The phase speed is bounded by the CFL condition ( $0 \leq \text{phase} \leq 1$ ); if waves are incoming then the phase is negative, hence bounded to zero. Out-going waves have the phase  $> 0$ .

SIGMA\_T :  $\sigma_T$  ( $\text{kgm}^{-3}$ ) is output as `dens_0 - 1000`.

ENERGY : Mechanical energy ( $\text{Jm}^{-3}$ ) given by (Kowalik and Murty (1993), eqn. 1.24):

$$E_T = E_k + E_p = \frac{1}{2} \rho (u_1^2 + u_2^2 + w^2) + \rho g \eta$$

KINETIC : Kinetic energy ( $\text{Jm}^{-3}$ ) given by (Kowalik and Murty (1993), eqn. 1.24):

$$E_k = \frac{1}{2} \rho (u_1^2 + u_2^2 + w^2)$$

SLOPE : Computes the surface slope in the e1 and e2 directions, stored in `surf_slope_x` and `surf_slope_y` respectively. **COMPAS only**: the slope is the mean slope of all face directions.

SURF\_LAYER : The k index of the surface layer is stored in the 2d array `surf_layer`.

BOTSTRESS : Bottom stress in e1 and e2 directions, and bottom stress magnitude.

WET\_CELLS : A diagnostic to show wet and dry water columns. Water columns are assigned the percentage of water they contain relative to being dry; i.e. a dry water column is assigned 100%, cell with sea level at msl is assigned 0 and when sea level rises above msl the percent dry is negative. If sea level falls to half the water depth, the cell is 50% dry. Note that a cell is considered dry when the water falls below `DRY_FRAC * HMIN`, where `DRY_FRAC` is currently hardwired to 0.05 and `HMIN` is defined in Section 4.4; e.g. if `HMIN = 0.07` m, then cells dry when the sea level gets within 3.5 mm of the bottom.

EKMAN\_PUMP : Computes surface and bottom Ekman pumping ( $\text{ms}^{-1}$ ) via:

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$$w_E = \text{cur}_z(\tau_s) / \rho_f \quad (\text{surface})$$
$$w_{EB} = \text{cur}_z(\tau_b) / \rho_f \quad (\text{bottom})$$

Where  $\tau_s$  is the surface wind stress and  $\tau_b$  is the bottom stress.

**UNIT** : A passive tracer with an initial value of 1. Good for testing the constancy condition in transport models.

**GLIDER** : A passive tracer is created to store cell averaged density from glider observations.

**RESOLUTION (COMPAS only)**: The mesh resolution, defined by the mean of distance between faces of all faces of each cell. Also output is the square root of cell area and edge area.

**U1VH (COMPAS only)**: The cell centered horizontal viscosity is output. Note: horizontal viscosity is an edge centered variable in COMPAS.

**TPXO (COMPAS only)**: If a custom tide file is specified using `TIDE_CONSTITUENTS` (Section 4.11.23) then a diagnostic field of the tidal elevation may be generated using `TPXO`. Furthermore, if this custom tide file contains velocity information, the cell centered velocity field (units  $\text{ms}^{-1}$ ) may be generated using `TPXO_VEL`, or cell centered transport field (velocity x depth; units  $\text{m}^2\text{s}^{-1}$ ) with `TPXO_TRAN`.

**CONTINUITY (COMPAS only)**: Checks the volume continuity balance. The change in volume in each cell over the time-step should equal the sum of incoming and outgoing volume fluxes (note: only the surface cell generally has changes in volume). Output is in  $\text{m}^3$  and should be  $\sim 1 \times 10^{-10}$ .

**DUMMIES** : Three generic 3D dummy variables (`dum1`, `dum2` and `dum3`) are created for hardwiring debugging diagnostics internally in the code.

`ALL_NUMBERS` Invokes all the diagnostic numbers.

### 4.31.15 Degree heating weeks

Thermal exposure computed using the NOAA degree heating week algorithm (<http://coralreefwatch.noaa.gov/satellite/methodology/methodology.php#dhw>) is invoked via:

```
NDHW n # Number of DHW diagnostics
DHW0 <climatology_0> <dhd_file_0>
DHW0.text CARS climatology # Optional descriptive text for DHW 0
DHW1 <climatology_1> <dhd_file_1>
DHW1.text NOAA climatology # Optional descriptive text for DHW 1
.
.
DHWn <climatology_n> <dhd_file_n>
```

Note that several parameterisations of DHWs can be prescribed in a run (e.g. using different climatologies). This algorithm outputs the degree heating week 'dhw' ( $^{\circ}\text{C}$ -week); values over 4  $^{\circ}\text{C}$ -weeks have been shown to cause significant coral bleaching. In this specification, `<climatology>` is a file containing the maximum of the monthly mean (MMM, not time dependent) with name 'dhwc', and `<dhd_file>` is a file containing degree heating day (DHD) values, having a name 'dhd'. This latter file should be the same as one in the dumpfile list containing the variable 'dhd', i.e. this value is read from a file produced by the same run that is computing the DHW. The NOAA algorithm computes the DHW value from the previous



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12 weeks of HotSpots (difference between SST and MMM), in their case as a twice weekly satellite derived estimate. The HotSpot is only accumulated when  $SST > MMM + 1^{\circ}C$  threshold; i.e. the HotSpot is  $\geq 1.0$ . The model computes the Hotspot at every time-step and saves the daily accumulation of these in the variable 'dhd'. These DHDs should be written to file, and in order to retrieve a 12 week sum of these (i.e. the DHW) a DHD value is read from this file, <dhd\_file>, 12 weeks prior to the current model time and subtracted from the DHW, then the current day's DHD is added to the DHW.

The DHD may be computed using a (daily mean of temperature) – [MMM] (as opposed to the daily mean of (temp – [MMM]) using:

```
DHW0 <climatology_0> <dhd_file_0> mean
```

Finally, the DHD may be computed using a snapshot temperature at <hrs> hours (0-24) using:

```
DHW0 <climatology_1> <dhd_file_1> <hrs>
```

e.g. if the algorithm is to emulate the DHD using a 5am satellite pass, then use;

```
DHW0 <climatology_0> <dhd_file_0> 5
```

Note that the hour is relative to the time zone in TIMEUNIT.

### 4.31.16 Tracer percentiles

The tracer percentile diagnostic calculates the spatial distributions of percentiles of a snapshot of a given tracer distribution, i.e. it shows the spatial position of the percentile values of a given tracer at a particular time. This diagnostic is useful for determining the position in a domain where e.g. a median, 95 %ile or 5%ile tracer concentration may be found. This diagnostic is time dependent, but if a mean is created using the `tracerstats` library, then the position in the domain where the average of a particular percentile (e.g. average median over a simulation) may be determined. The percentile calculation of tracer is invoked by specifying a tracer name, e.g;

```
CALC_PERCS      salt      # Name of tracer for percentile calculation
```

The region tracer percentiles is computed over may be specified via ranges or blocks (see Section 4.7.6 for structured and unstructured indexing conventions), e.g:

```
PERC_REGION      3          # Number of entries
12 25            #1: (i,j) location
(2,5)-(10,11)    #2: (i,j) range
24 27            #3: (i,j) location
```

If a range is given, SHOC will determine only those cells within the range that are wet. A region file (see Section 4.31.21) may also be used to specify the percentile region:

```
PERC_REGION      region.bnc 3 4 ... n # Region file and numbers
```

Finally, a vertical range the percentiles are computed over may be specified using:

```
PERC_REGION      -100 -50    # Between 100 and 50 m depth
```

or

```
PERC_REGION      surf      # Surface only
```

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A 3D tracer containing the specified tracer percentiles is automatically created with the tracer name appended to 'percentile\_' e.g. in this case 'percentile\_salt'.

## 4.31.17 Alerts

The alert diagnostic attempts to detect early signs of instability by monitoring maximum absolute velocities, divergences and, if invoked, maximum absolute momentum tendencies. These maximums are written to an alert diagnostic file every time-step, along with the maximums encountered during the whole simulation. A time series file containing the history of the maximum values is also created. To invoke alert tracking in passive mode:

```
ALERT          PASSIVE <alert_file>
ALERT_DT      1 hour
```

Where <alert\_file> is an optional filename to write the maximum value information to. This file name is appended with '.txt'. If <alert\_file> is absent then output is written to the file 'alert.txt' by default. If ALERT\_DT is present then a time series file is created with the alert filename appended with '.ts', and maximum values are output at the specified time interval. The maximum values printed to file are absolute maximum values. Note that maximum tendencies are only printed if the MOM\_TEND flag is invoked. The mechanical energy, excess mass (mean sea level) and boundary energy flux are defined according to Palma and Matano (1998) and are useful for diagnosing the stability of a domain;

$$\text{Mechanical Energy} = \frac{1}{A} \left[ \int_A \rho g \eta^2 dA + \int_A 0.5 \rho D (U_1^2 + U_2^2) dA \right] \quad (\text{Jm}^{-2})$$

$$\text{Excess Mass} = \frac{1}{A} \int_A \eta dA \quad (\text{m})$$

$$\text{OBC Energy Flux} = \frac{1}{W} \int_W D U (g \eta + 0.5 U_2^2) \Delta y \quad (\text{m}^4 \text{s}^{-3})$$

Where A = domain area, W = OBC width (the energy flux is for a u1 boundary in this case, see Section 3.11). Note that  $\rho$ (OBC Energy Flux) has units  $\text{Wm}^{-1}$ .

Alert tracking may be made active using the following:

```
ALERT          ACTIVE <alert_file>
```

Using the ACTIVE alert mode, when a maximum value exceeds defined thresholds then specific action is taken. This action falls into three categories:

LEVEL1 : 2D or 3D velocities exceed the VELMAX parameter. Horizontal diffusion is increased to the value  $\Delta x^2/4\Delta t$  which most effectively damps the shortest waves possible in the grid (Kowalik and Murty, 1993, eqn. 3.141). Velocity thresholds may be defined using the following parameters:

```
VELMAX      2      # Maximum horizontal velocity (ms-1)
WMAX        1e-3   # Maximum vertical velocity (ms-1)
```

LEVEL2 : 2D divergence =  $\partial \eta / \partial x$ , or 3D divergence =  $\partial w / \partial z$ , exceed a (hardwired) threshold. The Shapiro (1970) smoothing filter is applied to the relevant velocity field (Kowalik and Murty, 1993, eqn. 3.136)

LEVEL3 : momentum tendencies exceed (hardwired) thresholds. The relevant process is omitted during the next time-step.

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Individual alert actions can be turned on or off by prescribing 0 or 1 for each individual action::

```
          eta vel2d vel3d w tend 2d_div 3d_div cfl ts shear hdiff
ALERT_CODE 1      1      1      0      0      0      0      0      0      1      1
```

Alert information written to file has the following format (note: indexes in brackets are in Cartesian coordinates, outside the brackets are sparse coordinates);

Simulation time = 10.000000 (days)

Maximum absolute sea level :  
elevation : 0.248644 at 26 (25 1 22)

Maximum absolute velocity :  
u1 3D : 0.203112 at 1226 (1 25 22)  
u1 2D : 0.093261 at 1066 (45 21 22)  
u2 3D : 0.093234 at 1225 (0 25 22)  
u2 2D : 0.001336 at 1023 (2 21 22)  
w : 0.000044 at 12290 (49 25 14)  
Div 3D : 0.000004 at 1249 (24 25 22)  
Div 2D : 0.000000 at 767 (1 16 22)

Maximum absolute tendencies :  
u1 velocity  
u2 velocity

Area averaged energy :  
Mechanical energy : 231.513328 (J/m2)  
Excess mass : -0.003424 (m)  
Energy flux (W/m2) :  
Boundary 0 (West) : 2.276448  
Boundary 1 (East) : 2.272259

-----  
Simulation maximum absolutes

```
eta      : 0.248644
u1 3D    : 0.203115
u1 2D    : 0.093282
u2 3D    : 0.121123
u2 2D    : 0.006932
w        : 5.72e-05
div 3D   : 5.20e-06
div 2D   : 3.60e-06
```

## 4.31.18 Total mass, volume, heat and salt

The total mass, volume, heat and salt in the domain, useful for diagnosing conservation properties, may be output in time series format. The totals are output to the time-series file 'totals.ts'. If `OutputPath` is set, then the totals file will reside in this directory. To invoke the totals diagnostic use:

```
TOTALS          YES      # Invoke totals diagnostic
TOTALS_DT       1 hour   # Interval to print totals.
                  # The default is 1 hour.
```

The default is for no totals to be calculated. The output timeseries file consists of the following:

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```
## COLUMNS 5
##
## COLUMN1.name Time
## COLUMN1.long_name Time
## COLUMN1.units days since 1990-01-01 00:00:00 +10
## COLUMN1.missing_value -999
##
## COLUMN2.name Total mass
## COLUMN2.long_name Total mass
## COLUMN2.units kg
## COLUMN2.missing_value 0.000000
##
## COLUMN3.name Total volume
## COLUMN3.long_name Total volume
## COLUMN3.units m3
## COLUMN3.missing_value 0.000000
##
## COLUMN4.name Total heat
## COLUMN4.long_name Total heat
## COLUMN4.units deg C m3
## COLUMN4.missing_value 0.000000
##
## COLUMN5.name Total salt
## COLUMN5.long_name Total salt
## COLUMN5.units psu m3
## COLUMN5.missing_value 0.000000
##
```

Additional tracer totals may be computed by appending the tracer name to the TOTALS diagnostic, e.g;

```
# Include 'silt' and 'Chla' in totals diagnostic
TOTALS          YES silt Chla
```

The additional tracer totals will then appear in the time series. Note that `temp` and `salt` are always included. If a tracer included a sediment component, then the total mass is the sum of mass in the water column and the sediment. If the tracer is a 2D tracer, then the areal mean is reported.

Finally the volume flux through each open boundary, in  $\text{m}^3\text{s}^{-1}$ , is computed.

### 4.31.19 De-correlation length scales

The de-correlation length scales in the `e1` and `e2` directions can be computed and stored in `decorr_e1` and `decorr_e2` respectively. This is computed according to Romanou et al, 2006, where the de-correlation length scale is defined as the zero crossing point of the auto-correlated lags. The length scale is calculated on a sub-set of the grid, where the user specifies the length scale of the sub-set, `sz`. The de-correlation length scale is invoked using;

```
DECORR_LENGTH    <variable> sz <scale>
```

where `<variable>` may be;

```
<variable>      eta    # Sea level de-correlation length scale
                 u1     # u1 velocity
                 u2     # u2 velocity
                 any valid 3D tracer name (e.g. temp, salt)
```

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<scale> is a scaling factor for *sz*; e.g. if <scale> = km then the sub-set size *sz* is assumed to be in kilometres, and output length scales will also be in km. The default is metres if <scale> is absent; e.g;

```
DECORR_LENGTH      temp 1000      # Temperature de-correlation length
                                # scale using sub-set size of 1000m.
```

## 4.31.20 GHRSSST SST

Sea surface temperature derived from the GHRSSST database and its associated error provided via THREDDS server (<https://www.ghrsst.org/ghrsst-data-services/services/>) can be imported into the model. The product of choice must first be identified by navigating the THREDDS server to the desired product on the website. For example, if one wishes to use the L4 global (GLOB) product from the UK Meteorological Office (UKMO), then the link to historical data would be :

<https://data.nodc.noaa.gov/thredds/catalog/ghrsst/L4/GLOB/UKMO/OSTIA/catalog.html>

or

<https://www.ncei.noaa.gov/thredds-ocean/catalog/ghrsst/L4/GLOB/UKMO/OSTIA/catalog.html>

The GHRSSST diagnostic is invoked by either supplying a multi-netCDF file containing all the daily images to be imported, e.g.;

```
GHRSSST      UKMO.mnc
```

or providing a link to the THREDDS server in conjunction with an image name (with the date prefix stripped out). If the latter is used, then SHOC/COMPAS will find create a list of images based on the *start\_time* and *stop\_time* of the simulation (i.e. the year and day of the image will be computed by SHOC/COMPAS) and create a multi-netCDF file called *ghrsst\_list.mnc*, e.g.;

```
GHRSSST <path> <name>
```

where <path> is the path to the THREDDS server and <name> is the image name with the date prefix stripped off. Note the path can be retrieved by navigating to the OpenDAP link and cutting the path from the Data URL. An example for UKMO L4 products is;

```
GHRSSST
https://data.nodc.noaa.gov/thredds/dodsC/ghrsst/L4/GLOB/UKMO/OSTIA/
-UKMO-L4HRfnd-GLOB-v01-fv02-OSTIA.nc.bz2
```

Sometimes multiple image names are used; e.g. UKMO products can have a name convention of either *YYYYMMDD-UKMO-L4HRfnd-GLOB-v01-fv02-OSTIA.nc.bz2* (where *YYYY* is the year, *MM* the month and *DD* the day) or *YYYYMMDD120000-UKMO-L4\_GHRSSST-SSTfnd-OSTIA-GLOB-v02.0-fv02.0.nc*. In this case, use:

```
GHRSSST <path> <name1> <name2>
```

e.g. using UKMO L4 products;

```
GHRSSST
https://data.nodc.noaa.gov/thredds/dodsC/ghrsst/L4/GLOB/UKMO/OSTIA/
-UKMO-L4HRfnd-GLOB-v01-fv02-OSTIA.nc.bz2 120000-UKMO-L4_GHRSSST-
SSTfnd-OSTIA-GLOB-v02.0-fv02.0.nc
```

If the netCDF file using the <name1> template cannot be opened, then the file with the <name2> template is used. If neither of these files can be opened, then the image for that day is omitted.

Often there is a mixture of product name used on any given day and in this case the multi-netCDF file may need to be manually adjusted to ensure the image names are correct.

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The GHRSSST import option is set up to be generic, so potentially different SST products may also be imported. For example, the BoM 6 day night pass L3 product is located at:

<http://rs-data1-mel.csiro.au/thredds/dodsC/imos-srs/sst/ghrsst/L3S-6d/ngt/>

with a template of, e.g.

```
032000-ABOM-L3S_GHRSSST-SSTskin-AVHRR_D-6d_night-v02.0-fv02.0.nc
```

Unlike GHRSSST, these files are not placed in individual directories for each day, i.e. all files for a given year are found in yearly directories. To prevent the day being included in the path written to the `ghrsst_list.mnc` file, use;

```
GHRSSST_OPTIONS          NODAY
```

The variable name required to be read may differ from the GHRSSST L4 `analysed_sst` and `analysis_error`, and variable substitution can be invoked, e.g. for BoM files;

```
GHRSSST_OPTIONS VARIABLES (ghrsst=sea_surface_temperature) (ghrsst_error=quality_level)
```

The format of image files may change from year to year – e.g. sometimes more variables are included in files for some years than others. The netCDF multifile reader used to import SST files assumes that each file format in the multifile list must be identical. If this is not the case, then a separate `ghrsst_list.mnc` file may be produced for each year using:

```
GHRSSST_OPTIONS          YRMNC
```

having output of, e.g. `ghrsst_list-2000.mnc`, `ghrsst_list-2001.mnc` etc. Note that automated import in this situation will fail for the abovementioned reason, and the user must subsequently manually enter the list files, e.g.;

```
GHRSSST          ghrsst_list-2000.mnc ghrsst_list-2001.mnc
```

Note that variable substitution (Section 4.32.1) may be used with the above, and `GHRSSST_OPTIONS` can be combined.

### 4.31.21 *Mass Budgets*

The model domain can be arbitrarily divided into a number of regions for which mass and volume budgets can be computed over a predefined period. A netCDF file containing the region partitions (usually appended with `.bnc'`) must first exist. These files can be created using the `'BOX CREATION'` option in PLUM. Instructions for creating regions in PLUM are as follows:

1. Enter PLUM in Matlab.
2. Click on `GRID CREATION` and then `Read NETCDF File` to read in the Shoc grid information.
3. Click on `Draw/Erase Grid` to remove the grid line detail, leaving just the bathymetry.
4. Return to Main Menu and click on `BOX CREATION`, and then `Create New Boxes` to draw required boxes over the bathymetry. Note that instructions are provided in the matlab window.
5. Click on `Edit Boxes` to optimize the regions.
6. Click on `Partition SHOC` to partition all of the water cells into the 2D regions.
7. Click on `Assign Box Layers` as many times as there are regions that are required to be a function of depth; e.g. enter a vector such as `[4 0 -20 -40 -100]` to create 3 layers in Box 4 with layer faces at 0, -20, -40 and -100m. A

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maximum of 5 layers can only be assigned to any box. The depth slider can be used to scan layers and observe the different 3D regions.

8. The output is saved to a '.bnc' file. This can be read back via `Read netcdf File` at a later date to make more changes by repeating the above procedure.

Any '.bnc' file that SHOC/COMPAS attempts to read must contain the variable 'boxnos', and have the dimensions 'i\_centre', 'j\_centre' and 'k\_centre' to specify the grid size in x,y and z directions respectively. **Note: be sure that .bnc files are created for the input file you wish to use.** If the variable `regionid` in the output file shows values of -9999 as region numbers, then this is probably not the case and region exchanges may be incorrect. A warning is only issued if the grid dimensions in the .bnc and input file differ (# wet cells are not compared).

### COMPAS only:

Regions may be automatically generated using the `metis` libraries;

```
REGION      METIS <n>
```

Where <n> is the number of regions required.

To invoke the budgets over the regions, use:

```
REGION      path/name.bnc  # Path and filename of the .bnc region
              # file.
REGION_DT   10 days      # The time interval over which the
              # budgets are computed.
REGION_VARS passive      # Tracers for which the budgets are
              # computed.
```

The variables 'salt' and 'temp' are always computed by default (i.e. these variables do not need to be specified in `REGION_VARS`). A volume budget is also created by default. The keywords `MONTHLY`, `SEASONAL` and `YEARLY` may be input as `REGION_DT`, and `ALL`, `TRACERS_WC` and `TRACERS_DIAGN_WC` may be used for `REGION_VARS`.

Output is created for each region in the ascii file `region*.ts` where \* is the region number. If `OutputPath` is present, the files will be written to this directory. These files contain the mass at the start of the interval `REGION_DT` for each variable, mass at the end of the interval, the mean mass and standard deviation over the interval, the mass fluxes through segments connecting regions or through open boundaries (i.e. mass transfers from region to region, or across open boundaries) and the mass budget of the region, where:

```
mass budget = start mass + mass fluxes - end mass
```

Note that the mass fluxes are positive if mass is imported into the region, and negative if mass exits the region. If the budget is not approximately zero, then this means that there has been net import of mass into (positive budget) or export from (negative budget) the region. This may be due to a point-source/sink delivering mass into the region over the interval, fluxes through the surface or sediment or non-conservative processes associated with the tracer. The mean concentration in the region can be computed using mean mass divided by mean volume.

The volume budget is typically very small for a region, but mass budgets may be several orders of magnitude. This is due to compounding numerical error in the advection scheme, however, this error is small in comparison to the initial mass in the region and mass budget error should therefore be expressed as a percentage of the initial start mass to get a true indication of budget error. When this is done, mass budget error is typically < 0.1%.

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Note that in order for the mass to be initialized in the region scheduling, the very first dump in the region files use an interval that is one model time-step less than `REGION_DT`.

The mass fluxes in the hydrodynamic model are computed using the same fluxes as are used to update tracer advection, which are basically the (tracer concentration at a cell face) x (velocity through the face) x (area of the face) x (model time-step). This is also true of the transport model using the FFSL scheme.

**SHOC only:** The transport model using the semi-Lagrangian scheme computes fluxes by multiplying any interpolation weights that lie outside the region by the mass of the destination cell.

Both these methods are inaccurate near open boundaries; the hydrodynamic model because conservation is not respected in the boundary cell, and the transport model because a source cell for outflow may be a destination cell beyond the domain grid. These issues can be overcome by effectively migrating the open boundary location into the domain or creating extra 'boundary' regions for which it is acknowledged that the mass budget will be inaccurate. To migrate a boundary into the interior, use;

```
REGION_MODE          OBC_BDRY      # Migrate OBC into the interior
REGION_OBC_ZONE      1              # Number of cells to migrate the OBC
```

For the hydrodynamic model it is sufficient to migrate the boundary only 1 cell, and this is recommended (a warning is displayed if this is not the case). To create new regions adjacent to open boundaries, use;

```
REGION_MODE          OBC_AREA      # Migrate OBC into the interior
REGION_OBC_ZONE      5              # Cell width of the OBC regions
```

Regions may be used with multiple windows for the hydrodynamic model, but must be used with one window with the transport model. When `REGION` is used, the region partitions are written to the variable `regionid`, which is written to the output files.

**SHOC only:**

For the transport model using the semi-Lagrange scheme the update rule for tracer concentration  $C_i^t$  in destination cell  $i$  is:

$$C_i^t = \sum_j a_{ij} C_j^{t-1}$$

where  $C_j^{t-1}$  is the tracer concentration in source cell  $j$  at time  $t-1$ . The mass at time  $t$  in destination cell  $i$  is  $C_i^t V_i^t$ , therefore  $a_{ij} C_j^{t-1} V_i^t$  can be regarded as a mass transfer from cell  $j$  to cell  $i$ . This is the basis of our mass conservation analysis. It follows that  $a_{ij} C_j^{t-1} V_i^t$  is also a mass transfer from region  $r_j$  to  $r_i$ . If the total mass fluxes between regions is to be computed, then all these mass transfers are required to be cumulated. For the transport model, the mass budget is represented as:

```
start mass + mass fluxes + mass error + global fill = end mass
```

and as above, denoting the budget as:

```
mass budget = start mass + mass fluxes - end mass
```

then:

```
mass budget + mass error + global fill = 0
```

Here `mass error` is the mass conservation error for source cells in a region, and `global fill` is the mass change in the region due to the global filling algorithm. The former errors arise from using the non-conservative semi-Lagrangian advection scheme and an underlying flow field that is non-conservative (see Section 9.3). These errors are rectified globally using the global



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fill (i.e. mass is conserved over the whole domain), but this manifests as an input or removal of mass within a region, which is represented by `global fill`. If global filling is not invoked, then this error is zero. If the transport model uses the FFSL scheme then `mass error + global fill = 0`.

If sediments or ecology is invoked, then separate quantities are listed in the regions file that accounts for the change in mass due to the model performing point source, sediment or ecological transformations. Note that if the net exchange of mass between the sediment and water column over `REGION_DT` is non-zero (e.g. due to a denitrification flux in the sediment), then `mass_budget` will be non-zero, and can be attributed to these processes. If there are atmospheric fluxes, then these are similarly not accounted for resulting in a non-zero `mass_budget`. It is possible that the FFSL may sometimes be locally non-conservative if the Lipschitz condition is violated, which may also contribute to non-zero `mass_budget`.

If `ALL_TRANSFERS` is included in `REGION_MODE` when using the transport model, then mass or volume transfers from all defined regions are reported (as opposed to only those that share common boundaries).

The residence time for each region is output in each time-series file, and as a tracer in netCDF output having the name `residence`. This time is computed over the interval `REGION_DT`. The residence time in this case is the time it takes for the volume in each region to be turned over (i.e. replaced with water from other regions) due to volume fluxes through the region perimeters or open boundaries. Note that this must be considered in the context of the time and space scales of dynamics in play, and the size and location of the region. For example, a small region in an area of large tidal flow will have a small residence time, which may not be informative for, e.g. the time it takes fresh water deposited in the region to become saline again (since the tidal current may have a large instantaneous flux but a small residual). This residence time is also listed in the region output timeseries files. Additionally, the residence time computed using the net flow through the region perimeters (i.e. the sum of incoming and outgoing fluxes) is listed in this file under `residence_time_net`. This is the time it would take the residual flow to turn the volume within the region over.

## 4.31.22 *Glider comparisons*

A glider trajectory may be viewed as a time series where the glider observation is brought toward the model output by averaging the glider observations into model volumetric cells at discrete time intervals. The smallest time interval possible is that of the time-step of the model, and this may not always result in the glider located in contiguous model cells; i.e. the glider may pass through several model cells over the course of a model time-step. This is a limitation of the temporal discretization of the model, and cannot be avoided. Once glider and model data are co-located in time and space, then results for certain variables (temperature, salinity, etc.) can be visualized as a time series, allowing standard quantitative time series metrics to be computed (RMSE, MAE, bias, correlation Willmott). The depth of the glider and number of observations used to generate the glider volumetric average is also supplied.

A further metric of Brunt Vaisala frequency (buoyancy frequency) squared ( $N^2$ ) is supplied;

$$N^2 = -\frac{g}{\rho_0} \frac{\partial \rho(z)}{\partial z} \quad (s^{-2})$$

This metric allows behaviour in the mixed layer to be assessed. Vertical mixing processes in the model are controlled by source terms of buoyancy production, shear production and dissipation. Buoyancy production is  $N^2$  multiplied by a vertical mixing coefficient. Although glider data cannot provide information on the vertical profile of vertical mixing, it can supply insight into the contribution of buoyancy to vertical mixing. A maximum of  $N^2$  in the water column usually coincides with the bottom of the mixed layer. The use of  $N^2$  allows assessment of the mixed layer diagnostic by any criteria related to density gradient.

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In addition to coincident model and glider variables, a neighbourhood can be defined around the glider location in the model, and fuzzy verification techniques (Ebert, 2008) may be used to assess the extent of any double penalty issues. At this stage, a simple bound is placed around the glider variable representing minimum and maximum values of the variable in the model within the neighbourhood. If the glider observation falls within these bounds, we can assume the model is reproducing observed dynamics within a length scale representing a tolerable displacement of features. In terms of Ebert's decision model definition:

'Useful forecast predicts the observed variable within an area having a length scale that represents a tolerable displacement of a feature in the model.'

The generation of glider-averaged variables and neighbourhood bounds is performed inline as the model runs using the time series capability (Section 4.32.5). Input is a glider file containing glider location and variable values, and output is a time-series file containing glider location, glider-averaged values, model values and model bounds in the neighbourhood. The timeseries file is specified as, e.g;

```
TS0.name           glider_metrics.ts
TS0.location       glider_data.nc # Glider position data
TS0.dt             1 minute      # Interval to make comparisons
TS0.reference      surface
TS0.vars           eta
TS0.data_file      glider_data.nc(PRES=pressure) # Variable data
TS0.data_name      oxygen # Additional variables to include
TS0.data_kernal    2.5 km # Neighborhood size
TS0.data_metric    GLIDER # Glider comparison metric
```

The `GLIDER` diagnostic must also be specified under `NUMBERS` (Section 4.31.14), e.g;

```
NUMBERS           GLIDER
```

The glider data must contain the variables with names in the table below. Variable substitution should be used if the names in the file differ from those expected.

Note that if the `TS0.location` file has no dimensions or coordinates for the `lat` and `lon` variables, then the data is read in assuming it is fixed mooring (the sensor may vary with depth). This is useful to read in IMOS netCDF mooring data.

Variable	Name	Units
Temperature	temp	DegreesC
Salinity	salt	psu
Pressure	PRES	dbar
Time	time	tunits
Longitude	lon	degrees_east
Latitude	lat	degrees_north
Depth	depth	m

### 4.31.23 Normalized vertical profiles

A normalized vertical profile of a tracer may be generated, i.e. the tracer value at all depths divided by the surface concentration of tracer. This allows a tracer profile to be reconstructed from a surface distribution. To invoke the vertical profile use:

```
PROFILE <tracer>
```

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Where `<tracer>` is the name of the tracer to profile, e.g. `temp`.  
If a 2D tracer is also included;

```
PROFILE      <tracer> <tracer2D>
```

Then the 3D profile in tracer `nprof` is scaled by the 2D tracer, e.g. a 3D temperature representation could be reconstructed from a satellite SST image, e.g.;

```
PROFILE      temp ghrsst
```

## 4.31.24 Tracer monotonicity (COMPAS only)

The monotonic behaviour can be diagnosed for a tracer with name `<tracer>` using;

```
MONOTONE     <tracer> min max
```

Where `min` and `max` are minimum maximum values. The maximum difference in a run of any overshoots or undershoots beyond the bounds of the minimum and maximum values are reported in the tracer `mono`. If the `FFSL`, `QUICKEST` or `VANLEER` advection schemes are used, then the `min` and `max` values are retrieved from tracer values within the stencil used for that particular scheme, rather than those explicitly supplied above.

## 4.31.25 Error norm timeseries (COMPAS only)

Error norm loss for a tracer relative to a 'truth' tracer may be computed for the L1, L2 and L norms;

```
ERROR_NORM      passivet  passive  
ERROR_NORM_DT   10 minutes
```

Where `passivet` is the tracer representing the 'truth' (e.g. `GHRSSST`), `passive` is the model tracer (e.g. surface temperature). If the surface layer only is to be computed, the append `surf` to the above. Output of the timeseries is 1 hour by default, unless specified by `ERROR_NORM_DT`.

## 4.31.26 Generic data import

The import and interpolation onto the model grid of 2D or 3D data may be achieved using:

```
IMPORT2D      <name> <units> <file.nc> <x days> # Import 2D data  
IMPORT3D      <name> <units> <file.nc> <x days> # Import 3D data
```

Where `<name>` is the name of the tracer to appear in the output with units `<units>`, `<file.nc>` is the file to interpolate from (note that variable substitution may be included here) and if the file is time dependent, an optional `<x days>` may be used to specify the time record to interpolate, relative to the time stamp in the file. An example is:

```
IMPORT2D      mean_eta m /home/climatology.nc 9100 days
```

This feature is useful to import data using the automation options `-a` or `-r`.

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## 4.31.27 Diagnostic tracer names

The following table lists the tracer names (2D and 3D) associated with each diagnostic. These names must be used when attempting to output the relevant diagnostic to file.

Diagnostic name	Purpose	Tracer names
CALC_FLUXES	Tracer flux calculation	flux_e1, flux_e2, flux_w, flux_kz
MEAN VEL3D	3D mean velocity (ms <sup>-1</sup> )	ulmean, u2mean, wmean
MEAN VEL2D	2D mean velocity (ms <sup>-1</sup> )	ulav_mean, u2av_mean
MEAN ETA	Mean sea level (m)	eta_mean
MEAN KZ	Mean vertical diffusivity (m <sup>2</sup> s <sup>-1</sup> )	Kzmean
MEAN WIND	Mean wind (Nm <sup>-2</sup> or ms <sup>-1</sup> )	wlmean, w2mean
MEAN VOLFLUX	3D mean volume flux (m <sup>3</sup> s <sup>-1</sup> )	ulvmean, u2vmean
MEAN TS	Mean temperature and salinity	temp_mean, salt_mean
MEAN <trname>	Mean 2D or 3D tracer	tracer_mean
MIX_LAYER	Mixed layer depth (m)	mixed_layer
FLUSHING_TR	Flushing tracer	flush
STERIC_HEIGHT	Steric height (m)	steric
VORTICITY ABSOLUTE	Absolute vorticity (s <sup>-1</sup> )	abs_vor
VORTICITY RELATIVE	Relative vorticity (s <sup>-1</sup> )	rel_vor
VORTICITY POTENTIAL	Potential vorticity (m <sup>-1</sup> s <sup>-1</sup> )	pot_vor
VORTICITY TENDENCY	Vorticity tendencies (s <sup>-2</sup> )	rv_drvdt, rv_nonlin, rv_beta, rv_strch, rv_jebar, rv_wsc, rv_bsc
MIXING_SCHEME	Mixing length scale (m)	lscale
CFL	CFL stability criterion (s)	cfl2d, cfl3d
MOM_TEND	Momentum tendencies (ms <sup>-1</sup> )	u1_adv, u1_hdif, u1_vdif, u1_btp, u1_bcp, u1_cor u2_adv, u2_hdif, u2_vdif, u2_btp, u2_bcp, u2_cor
HEATFLUX	Heat flux components (Wm <sup>-2</sup> )	swr, lwr, shf, lhf, nhf
WAVE_VARS	Wave variables	wave_amp, wave_period wave_dir, wave_ub, ustrcw
WAVES	Wave bottom drag Wave radiation stress	wave_Cd wave_Sxy, wave_Syx
PROFILE	Normalized vertical profile	nprof
BRUNT	Brunt-Vaisala frequency (s <sup>-1</sup> )	brunt_vaisala
INT_WAVE	Internal wave speed (ms <sup>-1</sup> )	int_wave_speed
RICHARDSON_GR	Gradient Richardson number	richardson_gr
RICHARDSON_FL	Flux Richardson number	richardson_fl
REYNOLDS	Reynolds number	reynolds
FROUDE	Interfacial Froude number	froude
ROSSBY_EX	External Rossby radius (m)	rossby_external
ROSSBY_IN	Internal Rossby radius (m)	rossby_internal
SIGMA_T	Sigma_t, $\sigma_t$ (kgm <sup>-3</sup> )	sigma_t
SOUND	Speed of sound (ms <sup>-1</sup> )	sound
	Sonic layer depth (m)	sonic
	Sound channels (m)	sound_channel
SHEAR_V	Vertical shear (s <sup>-1</sup> )	shear_vert
BUOY_PROD	Buoyancy production (m <sup>2</sup> s <sup>-2</sup> )	buoy_prod

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SHEAR_PROD	Shear production ( $m^2s^{-2}$ )	shear_prod
SPEED_2D	2D Current Speed ( $ms^{-1}$ )	current_speed_2d
	2D Current Direction (DegT)	current_dir_2d
ENERGY	Mechanical energy ( $Jm^{-3}$ )	energy
KINETIC	Kinetic energy ( $Jm^{-3}$ )	kenergy
SPEED_3D	3D Current Speed ( $ms^{-1}$ )	current_speed_3d
	3D Current Direction (DegT)	current_dir_3d
SPEED_SQ	3D Current Squared ( $m^2s^{-2}$ )	speed_sq
WIND_CD	Momentum drag coefficient	wind_Cd
UNIT	Unit passive tracer	unit
OBC_PHASE	OBC phase speed ( $ms^{-1}$ )	obc_phase
CALC_PERCS	Tracer percentiles (%)	percentile_<tr name>
ALERTS	Alert information	alerts_actual alerts_cumulative
SHOW_WINDOWS	Window partitions	windows
WET_CELLS	Wet cell diagnostic	wet_cells
SHOW_LAYERS	Layer thickness (m)	layer_thick
BOTSTRESS	Bottom stress	tau_bel, tau_be2, tau_bm
SURF_LAYER	k index of surface layer	surf_layer
SLOPE	Surface slope ( $mm^{-1}$ )	surf_slope_x, surf_slope_y
REGION	Region budgets	regionid
AGE	Age tracer	age
DECORR_LENGTH	De-correlation length scale	decorr_e1, decorr_e2
EKMAN_PUMP	Ekman pumping velocity	sep, bep
GHR SST	GHR SST sea surface temp	ghrsst
GLIDER	Glider density ( $kgm^{-3}$ )	glider
RESOLUTION	COMPAS mesh resolution	cell_resolution
U1VH	COMPAS horz. viscosity	u1vhc
CONTINUITY	Volume continuity ( $m^3$ )	vol_cont
TPXO	Custom tide elevation	tpxotide
TPXO_VEL	Custom tide velocity ( $ms^{-1}$ )	tpxou, tpxov
TPXO_TRAN	Custom tide transport ( $m^2s^{-1}$ )	tpxoU, tpxoV
Particle tracking invoked	Particle concentration	ptconc

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## 4.32 Data variables and input time-series files

There are a variety of parameters in SHOC/COMPAS for specifying input time-series datafiles. It is expected that:

- The datafile specified be either a NetCDF or ASCII time-series datafiles
- The files conform to the coordinate conventions described in section 10.
- The files contain the necessary variables name(s) for the parameter.

Following is a list of the parameters names and the variables that each parameter expects to find in the datafile:

<b>Parameter name</b>	<b>Expected variable names in datafile</b>	<b>Substitution names</b>
AIRTEMP	air_temp	air_temp
BOUNDARY?.DATA (elevation)	eta	eta
BOUNDARY?.DATA (u1)	u1 or u and v	u1 or u and v
BOUNDARY?.DATA (u2)	u2 or u and v	u2 or u and v
BOUNDARY?.DATA (tracers)	tracer-name	tracer-name
CLOUD	cloud	cloud
ETA_RELAXATION_FILE	eta	eta
EVAPORATION	evaporation	evaporation
HUMIDITY	humidity	humidity
ORBITAL_VEL	ub	ub
WAVE_AMPLITUDE	amplitude	amplitude
WAVE_PERIOD	period	period
WAVE_DIRECTION	direction	direction
PRESSURE	pressure	pressure
PRECIPITATION	precipitation	precipitation
WET_BULB	wet_bulb	wet_bulb
RADIATION	swr	swr
TRACER?.RELAXATION_FILE	tracer-name	tracer-name
TRACER?.DATA	tracer-name	tracer-name
WIND_TS	u, v	wind_u, wind_v

### 4.32.1 Variable substitution

Since it is not always possible to supply datafiles with exactly the required variables names, **SHOC/COMPAS** permits the expected variable name to be substituted for an alternate name. This is done by assigning (=) the new variable name to the default expected variable name. Multiple assignments are separated by commas . The assignments are enclosed within parentheses. No whitespace is permitted.

For example, for a standard file assignment such as:

```
WIND_TS windfile.ts
```

**SHOC/COMPAS** would search for the variables `u` and `v` within `windfile.ts`. If these variables were not present then **SHOC/COMPAS** would quit with an error. If however, there were two variables called `wu` and `wv` then the following substitution could be used.

```
WIND_TS windfile.ts(wind_u=wu)(wind_v=wv)
```

## 4.32.2 *Multiple datafiles*

At this time the specification of multiple datafiles is only permitted when defining boundary inputs, wind files, relation and resetting. Following is an example of how to substitute variable names and specify multiple time-series files for a boundary parameter:

```
BOUNDARY1.DATA t1.nc(salt=salinity) t2.nc(temp=tmp)
```

A list of files may be included in a separate text file, to which the boundary (or wind etc) specification may define, e.g. a multi-file-netcdf text file, `boundary.mnc` may be generated having the following format:

```
multi-netcdf-version 1.0
nfiles 2
file0.filename t1.nc
file1.filename t2.nc
```

Boundary data may then be defined via (with variable substitution included):

```
BOUNDARY1.DATA boundary.mnc(salt=salinity)(temp=tmp)
```

This is a convenient method of specifying a long list of files as input. **Note that the netCDF attributes for the list are retrieved from the first file in the list, so it is essential that the ordering of attributes and dimensions in each file in the list is the same.**

## 4.32.3 *Model variable initialisation*

At the start of a model run, the model variables are initialised for each grid using a netCDF input file which is either generated from the parameter file using the `-g` option, or obtained from the output of a previous run. This initialisation input file for each grid is specified as follows:

```
INPUT_FILE in.nc
```

The input file may contain more than one record, the record is selected based on the `START_TIME` parameter for this run. The time in the datafile must match **exactly**.

## 4.32.4 *Model variable output*

**SHOC/COMPAS** provides two mechanisms for recording its results: ASCII time-series of values as computed for particular locations and as an n-dimensional netCDF datafiles.

## 4.32.5 *ASCII time-series*

ASCII time-series output files contain values for significant model variables at specific locations. A time series file is created for each location in the model domain and records are written at a pre-determined interval. Currently the output variables include time, surface elevation, current components (2D and 3D; for COMPAS components are rotated east and north), and tracers. Non-time dependent geometry information is also provided (cell centre, bottom depth, etc.) in the header. Time series output in **SHOC/COMPAS** are referenced to the free surface, mean sea level or the bottom.

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ASCII time-series are convenient for comparisons with point observations (such as tide gauges or current meters).

```
# Number of time-series outputs.
TSPOINTS 2

# Parameters for each time-series point.
TS0.pname      MP1.ts          # Filename prefix
TS0.location   319672.69 5758871.98 -4 # Location (X Y Z)
TS0.dt         1800 seconds     # Output interval.
TS0.reference   surface        # reference level
TS0.vars       salt temp       # Tracer variables output
TS0.type       simple          # SHOC only: Velocity
                                     # output type.

TS1.pname      MP2.ts
TS1.location   319672.69 5758871.98 -12.75
TS1.dt         0.5 hour
TS0.reference   bottom
```

**SHOC only:** An output type of `simple` will cell centre the velocity variables and rotate them onto the east-west / north-south axis. A `standard` type will print the velocity at the cell face relative to the  $e_1/e_2$  grid orientation (i.e. as they are used by the model). The `simple` type is the default.

For COMPAS velocities are always centered and rotated to east and north components.

The reference level is determined by the following:

```
TS0.reference   surface        # referenced to the free surface
TS0.reference   msl           # referenced to mean sea level
TS0.reference   bottom        # referenced to the bottom
```

The default value is `reference = msl`. If the reference level is `surface`, then output will always occur at the specified depth below the free surface and if the free surface is fluctuating may not always be in the same cell. If the reference level is `msl` then output will be the specified depth below the undisturbed sea surface and will always be in the same cell if it is wet. Note that the depth below the free surface may change in this case. If the reference level is `bottom` then output is the specified depth above the bottom. This will always occupy the same cell providing the cell is wet. For the surface and bottom cases, the sign of the depth may be positive or negative.

If the `vars` field is absent then all tracers are included in the time series file.

Time series files are ASCII files, with a header containing information about the data in the files, and data in columns. Their format is described in section 11.1.

Time series output also allows the import of observational data (`.ts` or `.nc`) which can be compared to the model data inline. The comparison takes the form of a variety of established metrics, and can be done over a predefined area, or kernel, of the model grid. This stems from neighbourhood techniques (or fuzzy verification) that is used, where for higher resolution models, closeness to observations is not rewarded using traditional verification metrics (e.g. RMSE, cc). Predictions that are slightly offset relative to the observations are as severely penalized as those that are significantly offset with these traditional methods. Neighbourhood techniques attempt to overcome this by rewarding predictions where the shape and magnitude of a feature are correctly simulated, but it is slightly offset in time or space. This is discussed in detail in Ebert (2008) in relation to meteorological forecasts, and at:

[http://www.cawcr.gov.au/staff/eee/Precipitation%20Book\\_ch.16.pdf](http://www.cawcr.gov.au/staff/eee/Precipitation%20Book_ch.16.pdf)

These techniques are invoked by supplying an observation file, kernel size, variable name for the comparison and metric type to the time series:



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```
TS0.data_file      observations.ts    # Observation file.
TS0.data_name      salt temp          # Variable names to compute
                                     # metrics for.
TS0.data_kernel    3                  # Kernel size (odd numbers only)
                                     # or size in m or km (e.g. 5 km).
TS0.data_metric    MEAN              # Metric to apply to observations
                                     # and model data.
TS0.data_threshold 30.0              # (Optional) threshold for
                                     # categorical metrics.
```

A `data_kernel = 1` will perform the metric only at the location of the observation, a `data_kernel = 3` will perform the metric on a 3 x 3 subset of the grid, a `data_kernel = 5` will perform the metric on a 5 x 5 subset of the grid etc. For unstructured meshes, a kernel of 3 uses a 'ring' of cells surrounding location of the observation, a kernel of 5 uses two 'rings' of cells etc. The available metrics are;

```
CLOSEST           The model value within the kernel closest to the
                  observation value is output.
MINMAX            Same as CLOSEST, but minimum and maximum neighbourhood
                  Values are also reported.
MEAN              The model mean over the kernel is output.
RMSE              Output RMSE between observations and model values over
                  the kernel.
CATEGORICAL       Categorical contingency table values are output. The
                  maximum frequency of categorical values in the kernel is
                  output, where;
                  hit = 0, miss = 1, false alarm = 2, correct reject = 3.
                  Hit = observation and prediction above the threshold.
                  Reject = observation and prediction below the threshold.
                  Miss = observation above and prediction below threshold.
                  False alarm = observation below and prediction above
                  threshold.
HIT_RATE          hits / (hits + misses)
FALSE_ALARM_RATE  false alarm / (hits + false alarms)
CRITICAL_SUCCESS  hits / (hits + misses + false alarms)
TRUE_SKILL        HK (Hanssen-Kuipers) score; hits / (hits + misses
                  + false alarms)
PREDICTION_RATE   (hits+rejects) / (hits+misses+false_alarms+rejects)
ZINTERP           Interpolate model output vertically onto the z-coordinate
                  supplied in a TS.location file.
GLIDER           Glider comparison metric (Section 4.31.22)
```

For the categorical metrics (`HIT_RATE`, `FALSE_ALARM_RATE` etc.), a threshold must be supplied. This can either be a number, or the name of a tracer in the tracer list. If the latter is used, for example, a climatology could be used as the threshold by using the name of a tracer where climatology is read in using the `RESET` function.

The time series output will contain two extra columns for each `data_name` listed; the computed metric and observational value.

### 4.32.6 NetCDF dump files

More than one netCDF output dump file maybe specified in the **SHOC/COMPAS** parameter file. Each output file contains the grid geometry, times and selected model variables.

The number of output files are specified by the parameter `OutputFiles`. The parameters for each output are specified with the prefix `file<N>` where `<N>` is the output file number.

Numerous netCDF output conventions are supported by **SHOC/COMPAS**, as detailed below.

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1. For structured files, the `standard` output contains up to four staggered grid geometries, based on a quadrilateral Arakawa C-Grid. Variables are placed on their native locations on the grid (e.g. velocities on the faces, tracers at the centres).
2. For structured grids, the `simple` format contains only one grid geometry, with all data variables interpolated on to the cell centre. Velocity components are therefore represented as eastward and northward components, rather than components relative to the grid used (i.e.  $e_1$  and  $e_2$  directions which may be spatially variable for curvilinear grids). Vector variables can be stored as vector components, or speed and direction. The `simple_cf` format is a `simple` output with variable names and attributes that conform to the Climate and Forecast netCDF conventions (<http://cfconventions.org/>).
3. The point array, `parray`, is essentially a standard output on user defined cells, therefore generally using significantly less disk space than other file formats. This is useful for outputting open boundaries for nesting purposes. Velocities are represented as eastward and northward components.
4. The UGRID v1.0 CF compliant netCDF format (<https://github.com/ugrid-conventions/ugrid-conventions>) is available for unstructured or structured output. The 3D layered mesh topology is used in this instance (<http://ugrid-conventions.github.io/ugrid-conventions/>), and results may be visualized with GODIVA 3 or PLUM.
5. **SHOC only:** Output in the Modular Ocean Model (MOM) format is achieved using the type `mom`.
6. **SHOC only:** Output in the Regional Ocean Modelling System (ROMS) format is achieved using the type `roms`.
7. The `sparse` output contains a dump of the sparse format used internally in **SHOC/COMPAS**, i.e. a one dimensional vector of *only* the wet cells in the grid. If a large amount of the model grid contains land, the sparse format can therefore use significantly less disk space than standard formats, and is an extremely useful format to use in conjunction with the transport (-t) mode. Note that the sparse format cannot be sub-sectioned, i.e. the whole array must be dumped for 3D or 2D variables. The exception to this is that the surface only may be dumped if the filename is appended with `'_surf'`.  
(n.b. The sparse netCDF format does contain geographic information in the file and mappings from sparse position to Cartesian (i,j,k) locations. This information may be used to visualize a sparse format file directly. If a sparse format is to be read back into the model then it must be un-packed using the routine `'unpack_sparse()'` to scatter the file data to wet cell locations).  
The internal structure of `sparse` files are different for SHOC and COMPAS, with COMPAS using a non-layered variant of the UGRID conventions.

```
# Specifying two output files for a grid.
OutputFiles                2

# Specify the path for output files. Time series files are also
# output to this path. If the SEQUENCE flag is invoked (Section
# 4.4) then /run<n> is appended to the path, where <n> is the
# run sequence number.
OutputPath                  /home/data/output

OutputTransport             <tag>
# Output transport files. Files are created for each month with
# the name tag_trans_mmmyyyy.nc where 'tag' is the tag specified
# above, mmm is the month (e.g. 'jan') and yyyy is the year.
# Files are output in 'sparse' format. Variables output are:
# eta, ulmean, u2mean, wmean, temp, salt, Kzmean

# Output file 0
# The tag ALL for the vars parameter means the following
```

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```
# variables are save to the output dump file.
# eta, u1, u2, w, ulav, u2av, topz, wtop, wind1, wind2, patm,
# dens, dens_0, Kz, Vz, Cd, ulbot, u2bot, ulvh, u2vh, flag
# all the tracers and ptconc if particle tracking is enabled.
# This is in addition to the coordinate variables.
# COMPAS only: The tag FORCING_VARS only outputs atmospheric
# variables wind1 patm air_temp cloud precipitation dew_point
# The following fields are manadatory.
file0.name          out.nc          # Output prefix.
file0.type          standard        # Standard dumpfile.
file0.tinc          1 day           # Output interval.
file0.bytespervalue 4              # 2 - shorts
                                   # 4 - floats.
                                   # 8 - doubles
file0.vars          ALL             # ALL variables.

# Output file 1
# A spatial subset of the grid (possible for use in nesting).
# Notice only a subset of the variables are being output.
file1.name          nested_smp.nc
file1.type          simple          # simple output.
file1.tinc          1 hour          # Output interval.
file1.bytespervalue 2              # Output as shorts.
file1.vars          eta salt temp   # Limited variables

# These fields are optional, if they any are not specified
# then the full range is used for that dimension.
file1.tstart        0 days          # Output start time.
file1.tstop         44 days         # Output stop time.
file1.i_range       60 70          # Cells 60 to 70 along I.
file1.j_range       13 18          # Cells 13 to 18 along J.
file1.k_range       0 45           # Half water column.

# File points (parray only)
# A list of geographic locations is specified for the point array
# output, e.g;
file0.points 2
  lon1 lat1
  lon2 lat2
```

**COMPAS only:** If the name of an open boundary is specified for points, then data at the locations required to force that boundary is output.

If a polygon file (ending with `.xy`) is specified for points, then all the locations within that polygon are used for parray output.

If the file name is appended with `'_surf.nc'`, then only the topmost layer of the grid dumped to file (e.g. equivalent to `<file?.k_range 20 20>` for a 20 layer model). If `tstart` and `tstop` are absent, then these values assume the specified `START_TIME` and `STOP_TIME` respectively.

The following output intervals are also supported:

```
file0.tinc  YEARLY  # Output occurs on 1 Jan every year
file0.tinc  SEASONAL # Output occurs on 1 March for summer
                                   # 1 June for autumn
                                   # 1 September for winter
                                   # 1 December for spring
file0.tinc  MONTHLY # Output occurs on 1st day of the month
file0.tinc  DAILY   # Output occurs for each day of the year
```

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An option exists to automatically **chunk** netcdf output DAILY, MONTHLY or YEARLY as follows:

```
file1.name out.nc
file1.chunk DAILY # or MONTHLY or YEARLY
```

In the above case there will be multiple output files created with the date stamp as a suffix

```
out_2011-02-01.nc
out_2011-02-02.nc
...
```

Note that there may not necessarily be one file per day, it depends on the file increment. The option merely enforces *at most one days (months or years)* worth in each file. For MONTHLY only the year and month suffix is added and for YEARLY, only the year. This applies to standard, simple, simple\_cf, parray and sparse output netcdf formats.

A sparse or standard formatted files may have the additional modulo attribute which may take the value year, month, week, day, hour, minute or second, e.g;

```
file0.modulo year # yearly modulo
```

When these sparse formatted files are input via tracer resets or in the transport mode, then the model time is converted relative to the defined modulo. For example, if a year modulo is specified then all model times are converted to times within the range 0 to 365, and an input file of length 1 year may be used to cycle through a simulation of many years length. When dumping, the modulo is relative to the tstart time specified for the output file (e.g. for year modulo, set tstart to be 1 Jan for a particular year).

A filling algorithm may be applied to the output variables prior to dumping which re-assigns values over land, e.g;

```
file0.fill_rule default # eta = 0 and 3D tracers = NaN at
# land cells.
file0.fill_rule no_fill # No filling applied
file0.fill_rule zero_fill # eta = 0 and 2D & 3D tracers = 0
# at land cells.
file0.fill_rule cascade_search # Land cells filled with the
# nearest wet cell for eta, 2D
# and 3D tracers.
```

Output may be filtered before being dumped by using:

```
file0.filter avarge3 # 9 point convolution smoothing filter
average5 # 25 point smoothing filter
weighted3 # 9 point Shapiro filter
shapiro3 # 9 point Shapiro filter
weighted5 # 25 point weighted filter
shuman3 # 9 point Shuman filter
highpass3 # 9 point high pass Laplacian filter
```

Filtering is useful for the update of coarse resolution grids when using 2-way nesting.

2D and 3D tracer output may be masked to NaN when the bottom depth is deeper or shallower than a certain threshold using;

```
file0.bathy_mask -200 # Mask values shallower than 200 m
file0.bathy_mask 200 # Mask values deeper than 200 m
```

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## 4.32.7 Multi-dumpfiles

Dump files may be specified using a system analogous to the multi-netcdf input specification (Section 4.30.2); in this case a valid text file is specified for `OutputFiles` with the following format:

```
OutputFiles      df.txt      # Name of the multi-dumpfile text file
```

With `df.txt` containing, for example:

```
multi-dumpfile-version 1.0
nfiles      2
file0       standard.txt
file1       simple.txt
```

Each of the text files `standard.txt` and `simple.txt` then contains a list of output files as described in Section 4.30.6, e.g;

In `standard.txt`:

```
OutputFiles      2
file0.name       out.nc
file0.type       standard
file0.tstart     0 days
file0.tinc       1 day
file0.tstop      44 days
file0.bytespervalue 4
file0.vars       ALL

file1.name       out_surf.nc
file1.type       standard
file1.tstart     0 days
file1.tinc       1 day
file1.tstop      44 days
file1.bytespervalue 4
file1.vars       eta temp salt u1 u2
```

In `simple.txt`:

```
OutputFiles      1
file0.name       out.nc
file0.type       simple
file0.tstart     0 days
file0.tinc       1 day
file0.tstop      44 days
file0.bytespervalue 4
file0.vars       ALL
```

## 4.32.8 Coastlines

Coastline data may be specified; these are ASCII files containing 2 columns (x and y). A file may contain more than one coastline section (several islands, for example). It is preferable that each coastline section forms a closed polygon which does not contain any self-intersections. Coastline sections are separated by a blank line (and/or usually one or more comment lines as well). An example coastline file is shown below:

```
# This is an optional comment line.
# This is another comment line.
0 0
0 1
1 1
```

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```
1 0
0 0

# A second coastline section
1 0
1 1
2 1
2 0
1 0
```

You can have as many coastlines as you like, in as many files as you like, but it is usually convenient to keep all the data in one file.

## 4.32.9 Bathymetric data

In order to define the area to be modelled, you need to specify the bathymetry of the area. To do this, you need an ASCII file containing bathymetric data in 3 columns (x y and depth, free format). An example file is as follows:

```
# This is an optional comment line.
# This is another comment line.
# The 3 columns are x, y and depth
1000 1000 20
2020.2 1354 10
1520 7322 15
# You can even have comments in the middle of the data
7261 6123 8
8761 7991 5
```

The data does not need to be on any sort of regular grid - they may be randomly scattered in x and y. See Section 4.9 for options of interpolating bathymetry in SHOC and COMPAS.

## 4.33 Diagnostic files

### 4.33.1 *setup.txt*

A summary of the simulation is always printed to the file `setup.txt` upon execution of **SHOC/COMPAS**. This file is written to the path specified by `OuputPath` and the directory **SHOC/COMPAS** is run from. Typically this summary contains the following information:

---

```
SHOC Simulation Summary
Version : v1.0
Input file = open.prm
Open channel test domain
Grid description : Coarse open channel (120:1)

Simulation start time : Mon Jul 31 16:02:58 2006

Operating in 3D mode
3D time step = 40.000
2D time step = 5.000
Tracer time step = 40.000
Sub-stepping stability compensation; excluding surface layer
Thin layer adjustment implemented
```

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Exit on fatal eta instabilities when  $|\eta| > 10.00$   
Exit when above variables = NaN

Grid dimension : 212 x 52 x 25

Vertical structure

Vertical coordinate system = 'z'  
-40.0 -30.0 -25.0 -21.0 -18.0 -15.0 -13.0 -11.0 -9.0 -8.0 -7.5 -7.0 -  
6.5 -6.0 -5.5 -5.0 -4.5 -4.0 -3.5 -3.0 -2.5 -2.0 -1.5 -1.0 -0.5

2nd order momentum advection scheme.

QUICKEST (flux form : variable grid) tracer advection scheme.

Ultimate filter invoked.

Free slip condition.

Horizontal diffusion (x direction) = 2.000

Horizontal diffusion (y direction) = 2.000

Horizontal viscosity (x direction) = 20.000

Horizontal viscosity (y direction) = 20.000

Mean horizontal grid spacing : e1 = 275.01, e2 = 228.49

Vertical mixing scheme : mellor\_yamada\_2\_0

Surface roughness length scale = 0.100

Background diffusivity = 1.000e-07

Background viscosity = 5.000e-07

Bottom roughness length scale = 0.000100

Number of tracers = 2

Tracer #0 : salt [0.00e+00 : 4.00e+01]

Tracer #1 : temp [0.00e+00 : 4.00e+01]

Number of open boundaries = 2

Boundary #0 : west

Normal velocity = NOGRAD

Tangential velocity = CLAMPD

Elevation = FILEIN|MILLER

Tracer #0 (salt) = FILEIN|UPSTRM

Tracer #1 (temp) = FILEIN|UPSTRM

Relaxation constant = 0.008 (hours)

Boundary data file #0 : /home/mgs/dent/c2/west\_ets.nc

Boundary #1 : east

Normal velocity = NOGRAD

Tangential velocity = CLAMPD

Elevation = FILEIN

Tracer #0 (salt) = FILEIN|UPSTRM

Tracer #1 (temp) = FILEIN|UPSTRM

Boundary data file #0 : /home/mgproja/derwent/st\_meco/east\_ets.nc

Wind forcing from file /home/mgproja/dent/wind/wind\_grid.nc

Wind speed scale = 1.00

Wind speed threshold #1 = 10.00

Wind speed threshold #2 = 26.00

Surface drag coefficient #1 = 0.00114

Surface drag coefficient #2 = 0.00218

Heat flux calculated

Heat flux calculated : bulk formulation

Bulk scheme = Kondo (1975)

Reference height for air temperature/humidity = 4.00

Air temperature file : /home/mgproja/dent/heat\_obs/airport\_3hr.ts

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```
Wet bulb temperature file :  
/home/mgproja/dent/heat_obs/airport_3hr.ts  
Cloud cover file : /home/mgproja/dent/heat_obs/airport_3hr.ts  
Atmospheric pressure file :  
/home/mgproja/dent/press_meco/press_grid2.nc
```

No salt flux specified

```
Number of output file dumps = 6  
Output file #0 : /home/swirl1/test1/test_all  
Output file #1 : /home/swirl1/test1/test_sur
```

---

### 4.33.2 *diag.txt*

At every time step the simulation progress is written to file `diag.txt` which is useful to estimate the time remaining for the simulation. This file contains the following information:

```
Simulation start = 0.0000 (days) : 1990-01-01 00:00:00  
Simulation stop = 400.0000 (days) : 1991-02-05 00:00:00  
Simulation time = 400.0000 (days) : 1991-02-05 00:00:00
```

```
CPU time used this iteration = 0.000 (sec)  
Mean CPU time used / iteration = 0.000 (sec)  
CPU run time ratio = 1236051.502146  
Elapsed time = 0 day(s) 00:08:22  
Total time ratio = 68844.621514  
Time to completion = 0 day(s) 00:00:00  
Percent complete = 100.0%  
Running...
```

### 4.33.3 *Debugging*

Information useful for debugging model crashes may be generated using:

#### SHOC only

```
DEBUG_LOC i j k
```

#### COMPAS only

```
DEBUG_LOC us c j
```

where  $i$ ,  $j$  and  $k$  are integers specifying the  $(i, j, k)$  location in the grid information is desired to be generated at for SHOC, or the cell index ( $c$ ), index of the edge ( $j$ ) of cell  $c$  that velocity is to be diagnosed for COMPAS. Note the  $k$  index for the surface layer is given by `LAYERFACES - 2`. At present the debug information relates mostly to the 2D mode, providing velocity values at the debug location after each term in the equations is computed, for each step of the 2D mode. Maximum velocities in the window containing the debug location are listed. Elevation flux divergence details and elevation at the forward time-and tendencies for temperature and salinity are provided. The debugging information is written to the file 'debug.txt' at the current time-step. If a history of debugging information is required, use:

```
DEBUG_LOC i j k append
```



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Note that these files can then become quite large. The debugging information may be written after *n* days (or hours, minutes, seconds etc.) of simulation using:

```
DEBUG_LOC    i j k append after 2 days
```

The debugging can print the position in the computational flow of control (i.e. what numerical algorithm the code is currently computing) using:

```
DEBUG_LOC    i j k step
```

## COMPAS only:

The location of instabilities, including a label indicating the nature of the instability, is written to the file `crash.site` in the output directory when the model goes unstable.

### 4.33.4 History log

#### COMPAS only:

A history log may be generated where details of every run with the same parameter file name are appended to the log. The `HISTORY` option is turned off by default, and is invoked using:

```
HISTORY      LOG
```

Differences between the current run and the last run performed with the same parameter file, as inferred from the `setup.txt` file, may be included:

```
HISTORY      LOG DIFF
```

The history log is written to file `prmname.hist`, where `prmname` is the name of a `.prm` or `.tran` parameter file. Note that the `setup.txt` file from the current run is copied to `prmname.txt` if the `DIFF` option is invoked. Information in the history log is typically:

```
HISTORY LOG for parameter file est_quad.prm
Hydrodynamic model

-----
Run1:                Thu May  7 10:23:35 2020
EMS Version:         v1.2.1 rev(6487:6538M)
Executable file:     /home/her127/ems_us/main/model/hd-us/compas
Working directory:   /home/her127/work/meco/compas/est
ID_CODE:             GRID0|G0.00|H1.40|S0.00|B0.00
Input file:          est_quad.nc
Parameter header:    COMPAS estuarine test
Start time:          0 days
Stop time:           30 days
Difference summary
  New:    Simulation start time :  Thu May  7 10:23:35 2020
         Old:    Simulation start time :  Thu May  7 10:22:41 2020
Run successful at Thu May  7 10:37:02 2020
```

A separate file summarising any model re-configuration may be produced using:

```
HISTORY      LOG NOTES
```

This will list any new `NOTES` descriptors in the parameter file, linking it to the Run number in the history log and the model `ID_CODE`. If a `NOTES` descriptor is included in the parameter file (Section 4.4) when major model re-configuration occurs, e.g. prompting a change to the `ID_NUMBER`, then this is useful for a quick overview of the historical model configuration, and

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when used in conjunction with the history log can cross reference further details of changes to the model. The notes logfile is written to `prmmname.notes`.

A master history log can be maintained via:

```
HISTORY      MASTER /file_path/master_log.txt
```

In this case (for example) the details of the current run are written to the file `master_log.txt` in the directory path `/file_path`. Any model run with this specification will append details to the master log, allowing the user to have an overview of all model simulations performed across all applications.

## 4.33.5 Run code

The model run code a unique text code that is tagged in output. This allows the version numbers to be tracked through the grid generation process, hydrodynamic simulation and sediment transport or biogeochemistry simulation. The code is a set of floating point numbers separated by '|', and if present the code will be reported in the `setup.txt` file as a hydrodynamic version identifier (first number), sediment transport identifier (second number) and biogeochemical identifier (last number).

This code is automatically generated, based on `ID_NUMBER` present in netCDF input files or the parameter file. The user should not attempt to change the `ID_CODE` directly.

The code is of the form:

```
NAME|Grd_id|Hhyd_id|Ssed_id|Bbgc_id
```

NAME is a text string, `grd_id`, `hyd_id`, `sed_id` and `bgc_id` are floating point, e.g.

```
GBR|G2.3|H5.2|S1.0|B0.0
```

The individual ids can be in any order, but must be separated by '|'. An id of 0.0 indicates that model component has not been invoked.

The way the `ID_CODE` is generated is as follows:

Automatic grid generation using the `-a` or `-r` options (see Section 5); the `ID_CODE` NAME is set to NAME in the parameter file. The `grd_id` always set to 1.0 unless specified otherwise using the `ID_NUMBER`.

Input netCDF file generation using the `-g` option; the `grd_id` inherits the current `ID_NUMBER`. If no number is specified, the `grd_id` is set to 1.0.

A hydrodynamic simulation using the `-p` option; the `grd_id` is read from the netCDF input file, and the `hyd_id` is set the `ID_NUMBER`. If no number is specified, the `hyd_id` is set to 1.0.

A sediment transport or biogeochemistry transport simulation using `-t` option; The `grd_id` and `hyd_id` are read from the transport file, and the `sed_id` or `bgc_id` is set to the `ID_NUMBER`. If the model component is sediments, then the `ID_CODE` is recorded in the parameter file. This is used downstream to include the `sed_id` in BGC runs. Note that this means the parameter file is written to when used in this capacity, whereby the `ID_CODE` is overwritten if present, or written to the end of the file if not already present. If the model component is biogeochemistry, then the `sed_id` is read from the parameter file.

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## 4.33.6 Run regulation

The user may interactively control various aspects of the simulation using the `REGULATE_FILE` command. By defining a valid filename with this command, the user can enter commands in real-time to stop, pause, resume and re-configure various aspects of the run. This functionality is invoked via a scheduled function that reads the nominated file at a user defined interval. The run regulation is invoked via:

```
REGULATE_FILE      filename.txt      # Name of the file that contains
                                     # run regulation commands.
REGULATE_DT        1 hour            # Time interval that the file is
                                     # read.
```

Note that the `REGULATE_FILE` may be the parameter file. Any run regulation commands may begin with the keyword `REGULATE`. Valid commands are:

```
REGULATE STOP      # Stop the simulation. Output is dumped prior
                   # to quitting.
REGULATE PAUSE     # The run is suspended.
REGULATE RESUME    # A paused run is resumed.
REGULATE DUMP_REINIT # A new dump file specification is invoked.
                   # Any existing files are appended. Dump
                   # specification should be listed in the
                   # input parameter file.
REGULATE TS_REINIT # A new ascii time-series file specification
                   # is invoked. Any existing files are
                   # appended.
REGULATE WIN_REINIT # A new window partitioning is invoked.
                   # Window information should be listed in the
                   # input parameter file.
REGULATE OBC_REINIT <obc_name> <obc_type> # A the boundary condition
                   # <obc_type> is applied to open boundary
                   # <obc_name>. Valid types are:
                   NEST1WAY # 1 way nesting (Section 4.10.7)
                   NEST2WAY # 2 way nesting
                   RIVER    # River OBCs (Section 4.10.6)
                   NOTHIN  # No OBCs (Section 4.10.14)
                   SOLID   # The OBC emulates a solid boundary.
REGULATE DT_REINIT # Re-initialises the time-step to that
                   # specified in the input parameter file.
                   # Horizontal mixing is also adjusted.
REGULATE HVISC_REINIT # Re-initialises the horizontal viscosity to
                   # a constant value (i.e. non Smagorinsky).
REGULATE PSS_REINIT # Re-initialises the point source/sink
                   # specification.
```

The run regulation may be invoked at a specific time, by using `@ n days` where `n` is a valid day number relative to the timestamp, e.g:

```
REGULATE OBC_REINIT West NEST1WAY @ 10 days
or
REGULATE PAUSE @ 0.5 days
```

## 4.33.7 Rendering

A copy of the parameters used to configure a hydrodynamic, sediment transport or ecology simulation may be saved in binary form within the EMS executable. These configurations may be recalled to exactly replicate the saved configuration, and an `ascii` parameter file may be

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generated containing the configuration keywords and their values. This process is referred to as rendering. Note that this process differs to that of simply saving a parameter file in some form, since the rendering process imprints a binary copy of the data structures that the models use to define the configuration rather than an interpretation of that configuration using keywords and values that must be subsequently imported, re-interpreted and decoded. This creates a convenient way to robustly freeze a model configuration for later use.

The rendering process writes a C header file containing the model parameters (using C99 conventions) and a module containing global rendering management datastructures, and if EMS is re-compiled with this code then the configuration becomes part of the EMS executable, and as such becomes transportable with that executable and impervious to user corruption.

Rendering is controlled by the following:

```
RENDER_NAME name           # Name of the configuration
RENDER_DESC Standard config # Configuration description (optional)
RENDER_PATH /path          # Path to write render files (optional)
RENDER_TYPE HYDRO SED ECO  # Components to render (optional)
RENDER_OPTIONS DUMP LIST   # Options
RENDER_REMOVE name        # Remove configurations
```

When the code is run using the `-p` option, the rendering process is then performed. In the above example, the hydrodynamic, sediment transport and ecology configuration will be saved to a file `name.h` within the directory `/path`. A file `render_globals.c` is also automatically generated. If `RENDER_PATH` is absent, the files are written to the current directory. If these files are desired to be directly written to the EMS code, then for COMPAS `/path` should be:

```
~/ems/main/model/hd-us/render
```

And for SHOC:

```
~/ems/main/model/hd/render
```

If the path is the EMS code as above, then if EMS is re-compiled, the configurations become part of the executable. Otherwise, the files must be copied from `/path` to the above EMS code directories and re-compiled.

The `RENDER_TYPE` specifies if the hydrodynamic (`HYDRO`), sediment transport (`SED`) or ecology (`ECO`) configurations are written, By default all three are written.

If `LIST` is included in the options, then a list of all available configurations is written to file in the current directory. This file is called `name_list.txt` if a `RENDER_NAME` is specified, or `config_list.txt` if the `RENDER_NAME` is absent (i.e. a list may be generated without rendering a configuration).

If `DUMP` is included in the options, then ascii parameter files are generated that may be a starting point for re-configuring a simulation by the usual methods. If `HYDRO` is included in `RENDER_TYPE`, then the name of the parameter file is `name_hydro.prm` if `RENDER_NAME` is specified, or `hydro.prm` if absent. . If `SED` or `ECO` is included in `RENDER_TYPE`, then the name of the parameter file is `name_ecosed.prm` if `RENDER_NAME` is specified, or `ecosed.prm` if absent.

Any rendered configurations may be removed from the available configurations by specifying its name in `RENDER_REMOVE` and recompiling. Note that advanced users may wish to observe the available configurations by viewing `/render/render_globals.c` or the configuration values in `render/name.h`.

To recall a ended configuration use:

For hydrodynamics:

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HYDRO\_CONFIG                    name

Note that for hydrodynamics, tunable parameters are rendered, but the model forcing and initial conditions are not. Initial conditions (e.g. grid, bathymetry, temperature, salinity, sea level, currents) are contained in the `INPUT_FILE` and open boundary, atmospheric forcing, tracers used, layer structure, output files, start & stop time are required to be specified in the parameter file.

For ecology:

```
DO_ECOLOGY                    YES
PROCESSFNAME                 name # Ecology processes
BIOFNAME                     name # Ecology process parameters
ECO_VARS_ATTS                name # Ecology tracer attributes
```

See Section 17 for more information on ecology initialisation.

For sediment transport:

```
DO_SEDIMENTS                 YES
SEDFILE                      name # Sediment parameters
SED_VARS_ATTS                name # Sediment tracer attributes
```

The number of sediments layers (`NSEDLAYERS`) and sediment classes (`SED_VARS`) are still required to be specified in the parameter file.

See Section 17 for more information on sediment transport initialisation.

## 4.34 Explicit mapping (SHOC only)

**SHOC** operates on a sparse coordinate system internally, where all cell locations are aggregated in a one-dimensional vector and each cell's position in space is determined by the location in the vector of its neighbours. Ordinarily every cell is mapped to its immediate neighbour in three-dimensional space, but with the sparse system this does not need be the case. Cells can be made to have 'neighbours' which are nowhere near the cells geographic position. This explicit mapping method can be useful, for example, for connecting two ends of a channel if the channel cannot be resolved by the models discretization. Furthermore, a range of vertical cells may be specified which are subjected to this explicit mapping. This makes it possible to simulate flow beneath solid structures floating on the surface.

Explicit maps can be specified in either the `e1` or `e2` directions. The (i,j) cell locations listed for the maps must correspond to the cell centers. For the `e1` direction, one of the cells must be adjacent to a solid boundary on the left edge, and the other a solid boundary on the right edge. The cell with the right edge will then map through the solid boundary to access water properties in the cell with the solid left edge, and vice versa. For the `e2` direction, one of the cells must be adjacent to a solid boundary on the back edge, and the other a solid boundary on the front edge. Explicit maps through the whole water column are specified using the following:

```
MAP_POINTS_E1 2        # Maps cell (2,4) to cell (4,4), and cell
2 4 : 4 4             # (2,5) to (4,5) in the e1 direction. The
2 5 : 4 5             # reverse maps are also implied.

MAP_POINTS_E2 2        # Maps cell (9,12) to cell (9,14), and cell
9 12 : 9 14           # (10,12) to (10,14) in the e2 direction. The
10 12 : 10 14         # reverse maps are also implied.
```

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If the source and destination cells have different depths the mapping is performed through the water column until the bottom of shallower of the cells is reached. A vertical range of the map can be specified by appending the upper and lower k level the maps are operate within after the number of mapping points, e.g.

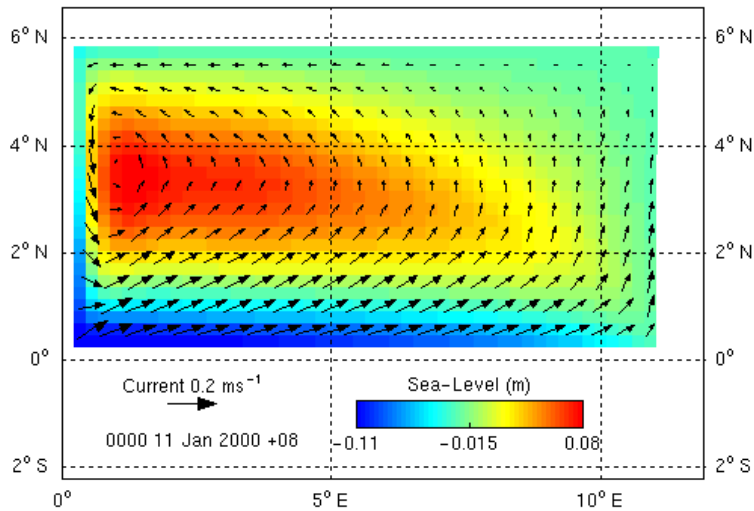
```
# Map the first cells in the list between layer 22 and layer
# 10. The upper-most layer (closest to the surface) is always
# listed first. The second cells in the list are mapped through
# the whole water column.
MAP_POINTS_E1 2
2 4 : 4 4 : 22 10
2 5 : 4 5
```

The explicit mapping list may contain any combination of cells mapped only between certain layers and cells mapped through the whole water column, i.e. any combination of the formats:

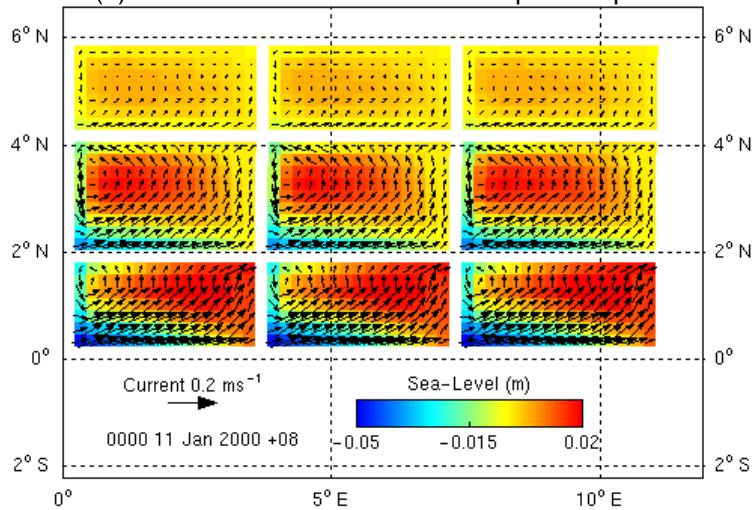
```
is ie : js je
is ie : js je : kt kb
```

Using the auxiliary program `jvismeco` is generally helpful when determining the map lists. An example of a domain using 2 explicit maps in the e1 and e2 directions is illustrated in Figure 4.31.1. The domain is divided into 9 sub-sections separated by land, but the explicit maps make the domain behave as if it were one connected region. The explicit mapping function only works with 'z' coordinates.

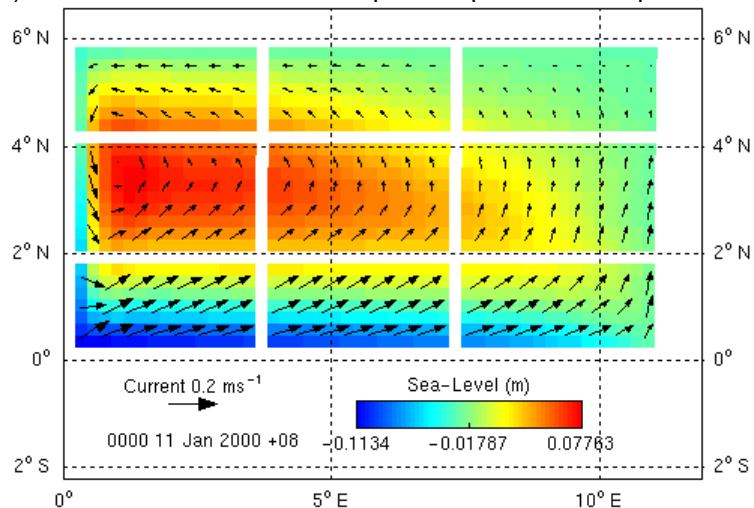
Figure 4.31.1 :  
(a) Un-partitioned closed basin solution



(b) Closed basin solution without explicit maps



(c) Closed basin solution with explicit maps across the partitions



Note : Fig 4.31.1 (a) and (c) utilize slightly different bathymetry, i.e. Fig 4.31.1 is 2 cells narrower in either direction since the 'walls' are not recognized as part of the domain, and bathymetry has a step across these 'walls', hence any slight differences in solutions between (a) and (c); the general dynamics are the same however.

## 5 Automatic setup (-a option)

As mentioned in section 3, the parameters outlined in this section may be automatically generated using the `-a` option in **SHOC/COMPAS**. In this case the parameter file must contain the following information:

```
# The start and stop time of the model simulation period,
# relative to the epoch (01/01/1990 00:00:00+8 by default).
# Relative time specifications here and elsewhere in the parameter
# file can be specified in seconds, minutes, hours, or days.
# Here, the start time corresponds to 1995-02-10 00:00:00 +8
#, and the end time to 1995-03-13 00:00:00 +8.
START_TIME          1866 days
STOP_TIME           1897 days

# The name of the input and parameter output files. The input
# netCDF file will have '.nc' appended to this name (i.e. test.nc)
# and the input parameter file will have '.prm' appended (i.e.
# test.prm).
INPUT_FILE          test

# Grid information (see section 4.7) defining the grid layout is
# mandatory. An example is included below:
PROJECTION          geographic
GRIDTYPE            GEOGRAPHIC_RECTANGULAR
NCE1                10
NCE2                20
DLAMBDA             0.01 # Long. cell interval in aux. coords.
                    # (degrees)
DPHI                0.01 # Lat. cell interval in aux. coords.
                    # (degrees)
X00                 144.3856 # Longitude of origin (degrees)
Y00                 -38.2030 # Latitude of origin (degrees)
POLE_LONGITUDE     0 # Longitude of false pole (degrees).
POLE_LATITUDE      90 # Latitude of false pole (degrees).

# Bathymetry : example depth values for a 3 by 4 grid
BATHY 12
22.2
12.3
7.4
23.5
12.0
6.0
25.8
13.7
5.8
27.6
14.2
4.9
```

The parameter file may then contain optional fields specifying the forcing and initialization of the model, i.e;

```
# Information regarding any forcing data to be read (e.g. wind,
# pressure).
# A time series file containing wind East and North
# velocity components, which must be called 'u'; and 'v'
# respectively, and have units of ms-1.
```



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```
WIND_TS                cyc_bobby95.nc
# How often to read data from the wind file and update
# the wind field in the model.
WIND_INPUT_DT         10 minutes

# A time-series file containing the variable 'pressure' with
# units of Pa.
PRESSURE              cyc_bobby95.nc
# How often to read the file and update the pressure
# field in the model.
PRESSURE_INPUT_DT     10 minutes      # Update every 10 minutes.

# Information regarding any initialization data for tracers temp
# and salt.
TRACER0.data profile.nc
TRACER1.data profile.nc
```

The open boundaries are automatically generated by **SHOC** on the basis that any wet cell at the grid extremes or any cell in the grid interior adjacent to an `OUTSIDE` flagged cell are set to open boundary cells. The grid is searched for these occurrences in the following order:

1. u1 boundaries on the left hand (i=0 or west) grid extremities
2. u1 boundaries on the right hand (i=NCE1 or east) grid extremities
3. u2 boundaries on the bottom (j=0 or south) grid extremities
4. u2 boundaries on the top (j=NCE2 or north) grid extremities
5. Interior u1 boundaries from i=0 to i= NCE1
6. Interior u2 boundaries from j=0 to j= NCE2

Open boundaries are automatically generated in **COMPAS** at the grid extremities that do not have a land neighbour. Note that no boundaries are identified by this method if the mesh is coastline fitted (i.e. no land is included in the mesh with an associated land mask). Boundaries that are not captured automatically must be manually specified using methods outlined in Section 4.11.2.

If elevation boundary data is present in the parameter file, the corresponding boundary is set to be elevation forced, otherwise the boundary is set to be passive, e.g;

```
# Set the first 3 boundaries found to be elevation forced
BOUNDARY0.DATA eta_west.ts
BOUNDARY1.DATA eta_south.ts
BOUNDARY2.DATA eta_north.ts
```

River inputs may be specified at a location using;

```
RIVER# <name> <lon> <lat> <flowfile>
```

Where # is the number of the river in a consecutive list, <lon> is the longitude of the river, <lat> is the latitude of the river and <flowfile> is the name of a file containing the river flow. The river will be located at the nearest coastal location in the model grid to <lon>, <lat>. A u1 or u2 custom river open boundary is created for each river specified. If <lon>, <lat> lies outside the footprint of minimum & maximum longitude and latitude for the grid, it is ignored. An example is;

```
RIVER0 river1 137.9 -33.4 flow1.ts
RIVER1 river2 137.8 -33.5 flow2.ts
```

Alternatively, a full boundary specification may be included, giving the user exclusive control over the open boundaries. Often this is best performed using a two step approach, where a grid is first created with all boundaries closed, i.e. by specifying;

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```
# Set all boundaries closed
NBOUNDARIES    0
```

Then boundaries are defined using external tools (e.g. `jvismeco`) and pasted back into the parameter file.

Various parameters automatically generated by **SHOC/COMPAS** using the `-a` option may be over-riden by specifying that parameter in the input parameter file. Parameters which fall into this category are:

```
# Open boundaries (see above)

# The epoch for all time related parameters, as well as
# for all output files generated by the model. Currently, the
# units must be 'seconds since ...', but this may change in future
# versions. The epoch is specified in standard ISO date/time
# format, including a possible timezone specification. The
# timezone here is 8 hours ahead of UTC.
TIMEUNIT        seconds since 1990-01-01 00:00:00 +08

# The base time unit that will be used for all
# timeseries and netCDF output files.
OUTPUT_TIMEUNIT    days since 1990-01-01 00:00:00 +08

# A single line description of the model run. This string is
# written into all output files.
PARAMETERHEADER    NWS 20km rectangular grid, Run 1

# The internal (3-d) time-step, and the number of times
# the external (2-d) code will be run per 3-d time-step.
# The external (2_d) time-step is thus DT divided by IRATIO.
DT                120 seconds
IRATIO            5

# Vertical geometry; z coordinates of the model layer interfaces.
LAYERFACES 5
-10.0
-8.0
-4.0
-2.0
0.0

# Bathymetry limits
# All cells will be at least 20m deep
BATHYMIN          20

# No cell will be more than 2000m deep
BATHYMAX          2000

# Invoke thin layer merging
HMIN              0.05

# Bottom roughness (values in metres).
Z0                0.001

# Mixing scheme
mellor_yamada_2_0
ZS                0.2
```

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```
# Horizontal viscosity in u1 equation
U1VH          1.0
# Horizontal viscosity in u2 equation
U2VH          1.0
# Horizontal diffusivity in the x direction (m2s-1)
U1KH          100
# Horizontal diffusivity in the y direction (m2s-1)
U2KH          100

# Sigma
SIGMA        YES

# Tracer relaxation
TRACER0.relaxation_file saltprof.nc
# How often to perform relaxation calculation
TRACER0.relaxation_input_dt 1 hour
# Relaxation time constant
TRACER0.relaxation_time_constant 20 days

# Full tracer specification
NTRACERS 2
TRACER0.name salt
TRACER0.long_name Salinity
TRACER0.units psu
TRACER0.fill_value 35.0
TRACER0.valid_range 0 40
TRACER1.name temp
TRACER1.long_name Temperature
TRACER1.units degrees C
TRACER1.fill_value 20.0
TRACER1.valid_range 0 40

# Output files for a grid.
OutputFiles          1
file0.name           out.nc          # Output prefix.
file0.gridtype       standard        # Standard dumpfile.
file0.tstart         0 days          # Output start time.
file0.tinc           1 day           # Output interval.
file0.tstop          44 days         # Output stop time.
file0.bytespervalue  4               # 2 - shorts
                                       # 4 - floats.
                                       # 8 - doubles
file0.vars            ALL            # ALL variables.
```

If transport output is specified (see Section 9) then a netCDF transport file for the and a transport parameter file run will be created;

```
TRANS_OUTPUT        YES
TRANS_MODE           SP_FFSL
OutputTransport      autotest
```

where the parameter file bears the name of the `INPUT_FILE` (e.g. for the example above, `autotest_trans_1995-02.nc` and `test.tran` will be created).

Executing **SHOC/COMPAS** with the `-a` option will result in the generation of an input netCDF file (having a name of the `INPUT_FILE` name with `'nc'` appended) and an input prm file template (having a name of the `INPUT_FILE` name with `'prm'` appended) which may be subsequently modified and executed using the `-p` option (see section 2). **SHOC/COMPAS** will then proceed to run using the automatically generated parameter specification. If it is

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desired that the run terminate after input and parameter files are generated (i.e. the model does not actually run through the integration period), then use the `-ag` option.

### **COMPAS** only

A template of a file required to execute the `-a` option may be created using:

```
compas -at <name>
```

Where the file created is `<name>.prm` and is written to the current working directory. This file contains JIGSAW, coastmesh, weighting and bathymetry options that the user is required to populate (see Section 14).

## 6 Restarts

### 6.1 Basic restarts

The model may be restarted using any `standard` format netCDF output file (see Section 4.31.6) containing ALL variables as the `INPUT_FILE`. In this case the model `START_TIME` must correspond to one of the dump times in the netCDF file. A warning is issued if this is not the case.

### 6.2 Restarts using restart file (-restart option)

Alternatively, a restart facility exists to allow the model to be seamlessly hot-started. Firstly, when initially running the model a `restart_dt` must be specified which defines an output interval that a special restart file, named `restart.nc`, is dumped at (in standard format, containing ALL variables), e.g;

```
restart_dt          2 days      # Create a restart.nc file every 2 days
```

This restart file is overwritten at the interval `restart_dt`. A path and restart filename may be specified using:

```
restart_name        <path>/<name> # Restart path and name, e.g.
                    # <path> = /home/data
                    # <name> = restart_1.nc
```

Or a path may be explicitly specified:

```
restart_path        <path>
```

Once this file is written, the model may be terminated, or may crash, and can be restarted using the `restart.nc` file, e.g;

```
shoc -p test.prm -restart
```

Using this restart method the model will read the appropriate `START_TIME` from the `restart.nc` file, and will append subsequent data generated to existing netCDF and time-series output files defined in the `.prm` parameter file (in the above example `test.prm`).

Note that restarts generally do not produce bit-exact solutions if output dumps are saved in floating point precision (`bytespervalue = 4`).

### 6.3 Near real-time restarts (-nrt option)

A near real-time operation mode may be invoked capitalising on restarts. This allows simulations to be repetitively started daily without having to manually alter the parameter file; this mode is invoked using:

```
shoc -p test.prm -nrt
```

In this case, the `START_TIME` for the simulation is read from the netCDF file specified as the `INPUT_FILE`, the stop time for the simulation is this `START_TIME` + `STOP_TIME` specified in the parameter file (i.e. the `STOP_TIME` is an increment rather than an absolute value), both the `RAMSTART` and `RAMPEND` are set equal to the `START_TIME` (i.e. no ramping is performed)

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and the output file `tstart` and `tstop` are set to the start and stop simulation times. This means that the `START_TIME`, `RAMSTART`, `RAMPEND`, `tstart` and `tstop` are not required to be set in the parameter file. Furthermore, if a restart file is overwritten to the same location, then this may be used as the `INPUT_FILE`. Additionally, the `SEQUENCE` option may be used to store model output in a unique directory, requiring that the only manual tasks to initiate repetitive simulations are the creation of the directory and commencement of the simulation, both of which are easily scripted. A near real-time parameter file for daily simulations may therefore appear as:

```
STOP_TIME          1 day                # Run length
INPUT_FILE         /home/data/restart.nc # Input file
restart_dt         1 day                # Restart interval
restart_name       /home/data/restart.nc # Restart file name
OutputPath        /home/data/          # Path for output
SEQUENCE          setup.txt            # Sequence set from file

OutputFiles        1                    # Output files
file0.name         out.nc
file0.filetype     standard
file0.tinc        1 hour
file0.bytespervalue 4
file0.vars        ALL
```

Then to run:

```
mkdir /home/data/run<n>          # <n> is the current run
shoc -p test.prm -nrt
```

## 6.4 Crash recovery (-cr option)

Often when a model fails, the strategy to maintain stability is to reduce the time-step, modify time dependent parameterisations (e.g. horizontal mixing coefficients) and restart the model before the failure occurred. This process can be automated using the `'-cr'` option, e.g;

```
shoc -p test.prm -cr
```

A restart file (Section 6.2) must be specified for this option to operate. If the model fails when this option is invoked (e.g. due to sea level rising above `ETAMAX`) then the time-step is progressively reduced (currently by a factor of 2), horizontal mixing is adjusted and the prognostic fields are re-initialised from the last restart file dump. The model then progresses using the smaller time-step to the next restart dump event, whereupon the time-step and mixing are reset to original values. If the model fails during the restart, the time-step is further reduced and the process repeated. Output to netCDF and timeseries files are over-written during the period the time-step is reduced. If the time-step is reduced more than 5 times, then the model will exit, on the assumption that it cannot recover by simply reducing the time-step. In this case, the instability may have to be diagnosed and rectified by other means (e.g. alternative OBCs, better forcing etc).

### COMPAS only

The crash recovery option may be run in an optimization mode, where horizontal viscosity is progressively increased and the time-step reduced until a stable run is achieved. If the model fails, then it is restarted from a restart file as above. This mode allows the user to automate the process of prescribing the largest time-step with smallest horizontal mixing for a run. The initial time-step prescribed should be roughly the CFL condition in this case, and `IRATIO` is kept constant as the time-step is reduced. The `DIFF_SCALE` for horizontal viscosity should be set to `AUTO` in this mode (Section 4.23). The time-step reduction and increments for viscosity increase may be set using, e.g;

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CRASH\_RECOVERY OPTIMIZE DT:0.8 VH:5 VHL:200

In this case the time-step is progressively reduced by 0.8 of its current value, and viscosity is increased in increments of 5% of the `AUTO` setting up to a limit of 200%. If `VHL` is absent, the limit is assumed to be 100%.

## 7 ROAM (-r option)

SHOC/COMPAS may be configured to operate in the ROAM (Relocatable Ocean and Atmospheric Model) or RECOM (RElocatable Coastal Ocean Model) environment. The ROAM configuration is essentially the same as the `-a` option configuration with a number of alternative parameterisations. The ROAM configuration is invoked using the `'-r'` option. The same mandatory information as used in the `-a` option is required (start/stop time, grid information, bathymetry). The ROAM option is designed to nest SHOC/COMPAS within a global ocean model and use information from this larger scale model for initial and boundary conditions. It is assumed that global model output exists covering the region of interest containing output dumps at approximately 1 day intervals. Temperature, salinity and sea level are required to be present in this output.

Currently the global model is a derivative of the GFDL MOM3 (Modular Ocean Model) model termed OFAM (Ocean Forecasting Australia Model <http://wp.csiro.au/bluelink/global/ofam/>). Using the `-r` option, these global model data are specified using:

```
OFAM_DATA          EAC_200401.nc      # OFAM input filename
```

These data will then be used for T, S and  $\eta$  initial and boundary conditions. Whenever an open boundary is located, the information found in the global model file is used to prescribe T, S and  $\eta$  OBC's. The sea level contained in the OFAM data represents the low frequency component only, and the ROAM configuration will prescribe these values on the open boundary with a tide superimposed using the global tide model of Cartwright and Ray (1990), (see Section 4.11, Science Manual). This model requires paths to the orthotide functions and nodal corrections to be present, e.g:

```
TIDE_CSR_CON_DIR   /home/tide/nodal      # Path to nodal
                   # correction directory.
TIDE_CSR_ORTHOHEIGHTS /home/tide/ortho_csr_4.0 # Orthotide functions
```

Temperature and salinity are prescribed on the open boundary using an upstream advection open boundary condition. Normal velocity uses a no-gradient condition and tangential velocity is clamped to zero. A horizontal sponge zone 8 cells wide is also imposed on the open boundaries.

It is possible to prescribe initial conditions for T, S and  $\eta$  which are different to the open boundary data defined in `OFAM_DATA` by using:

```
INIT_DATA          EAC_2004_init.nc # T,S, $\eta$  Initialisation data file
```

Furthermore, each stream of T, S and h may be defined independently using:

```
TEMP_DATA          EAC_temp.nc      # Input temperature filename
SALT_DATA           EAC_salt.nc      # Input salinity filename
ETA_DATA            EAC_eta.nc       # Input sea level filename
```

If only these specifications are present, then the data contained in these files is also used for open boundary forcing. However, if `OFAM_DATA` is present then the data contained in this file is used for T, S and  $\eta$  boundary forcing.

The ROAM configuration may be restarted from a previous run using the `'-rs'` option. In this case a restart file must be supplied:

```
RESTART_FILE       run1_all.nc      # Restart filename
```

The restart may be configured to commence using the temperature and salinity initial conditions from OFAM using the `'-rso'` option. The `'-rg'` option will terminate after the input



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and parameter files have been created (i.e. the setup is complete but the simulation does not commence).

Bathymetry may be specified in the ROAM configuration using a bathymetric database rather than supplying the bathymetry list via `BATHY`, e.g. by specifying;

```
BATHYFILE /home/bathy/ga2002_tiled.bth
```

the bathymetry will be interpolated onto the grid using the information contained in the bathymetric database 'ga2002\_tiled.bth'. This file has a unique format and lists all the tiled netCDF bathymetry files that comprise the database.

ROAM is designed to use surface fluxes from a relocatable atmospheric model (currently RAMS - Relocatable Atmospheric Model). The wind and pressure inputs may be the same as for the `-a` option. Alternatively, if wind and pressure are present in the same file, then use:

```
RAMS_DATA /home/atmos/EAC_rams.nc # Atmospheric forcing file
```

If the `RAMS_DATA` file contains heatflux data, e.g.

- incident flux of shortwave radiation (W m<sup>-2</sup>)
- incident flux of longwave radiation (W m<sup>-2</sup>)
- upward flux of longwave radiation (W m<sup>-2</sup>)
- surface sensible heat flux (W m<sup>-2</sup>)
- surface latent heat flux (W m<sup>-2</sup>)

then a heat flux may be imposed using:

```
HEATFLUX COMP_HEAT # Create net heatflux from components
```

This formulation of the heatflux will create a net heat flux from the longwave, sensible and latent fluxes, truncating the latent heat flux to zero to omit contributions from condensation. The shortwave flux is depth distributed according to the `SWR_TRANSMISSION` and `SWR_ATTENUATION` parameters (note defaults are 0.42 and 0.2 respectively).

All atmospheric data are read in with a time interval of 10 minutes. Wind and pressure may have an alternative input time specified.

The ROAM configuration was designed for robust simulation (at the expense of accuracy) and therefore various defaults differ in comparison to the `-a` configuration, viz;

- The Mellor-Yamada 2.0 mixing scheme is used.
- Smagorinsky horizontal diffusion is used with a constant of 0.1.
- One bathymetry smoothing pass is performed (`SMOOTHING 1`) and a maximum bathymetry gradient of 0.05 is specified (`MAXGRAD 0.05`).
- Minimum bathymetry is 1m. If maximum bathymetry is > 200m and minimum bathymetry < 4m then minimum bathymetry = 4m.
- The time-step is far more conservative by at least one half.
- Relaxation of T and S to OFAM data is performed using a 20 day relaxation time.
- OFAM temperature and salinity are present as tracers 'otemp' and 'osalt' respectively, read in on a daily time interval.
- `RAMPVARS WIND TIDALH` is used.
- Active alerts are implemented on 2D & 3D velocity and eta (`ALERT ACTIVE`). The eta relaxation file is taken to be the global model data; i.e. SHOC/COMPAS sea level is relaxed back to the low frequency sea level if the difference between the mean ROAM sea level (tidally averaged) and OFAM sea level exceeds the prescribed threshold.
- Thresholds for `ACTIVE ALERTS` are:
  - `VELMAX = 3.51 ms-1`
  - `VELMAX_2D = 2.40 ms-1`

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- `ETA_DIFF = 0.26 m`
- Mean sea level is computed for the active eta alerts (`MEAN ETA`).

The robustness of ROAM may be altered using the parameter `ROBUST` which is assigned from 1 (least robust) to 10 (most robust). There are a number of versions of the robustness configuration, which include older legacy implementations and also the `RECOM` configurations. The robustness version invoked is controlled using `ROAMv` flag where the full suite of robustness configurations is:

```
ROAMv  CPD      # Standard ROAM, clamped open boundaries.
ROAMv  RMD      # Standard ROAM, RAYMND radiation OBCs.
ROAMv  FLA      # Standard ROAM, FLATHR OBCs.
ROAMv  ROAMv1   # Standard ROAM, velocity forced OBCs.
ROAMv  ROAMv2   # ROAMv1 with alternative ROBUST parameterisation.
ROAMv  ROAMv3   # ROBUST parameterisation based on initial condition.
ROAMv  ROAMv4   # Same as ROAMv3 but uses TIDALC OBCs.
ROAMv  ROAMv5   # Same as ROAMv4 but uses TIDALC velocity OBCs.
ROAMv  RECOMv1  # Standard RECOM, no ROBUST.
ROAMv  RECOMv2  # RECOM with ROBUST parameterisations.
```

The `ROBUST` levels for `ROAMv1` has levels 1 to 5 linearly increasing the Smagorinsky coefficient from 0.1 to 0.5. For `ROBUST > 2` the horizontal diffusion distribution is smoothed using a 9 point convolution filter, and mixing coefficients have an upper limit corresponding to the computed constant mixing coefficients. For `ROBUST > 5` constant mixing coefficients are used and the time-step is linearly decreased from its computed value using `ROBUST = 6` to half its computed value with `ROBUST = 10`. The model starts from an initial velocity distribution at rest for `ROBUST > 6`. The default value is `ROBUST = 6`. Note that more robust parameterisations are generally less accurate. This configuration is summarized as:

## ROAMv1

```
ROBUST=1: Initial conditions use OFAM currents + Smagorinsky = 0.1
ROBUST=2: OFAM currents + Smagorinsky = 0.2
ROBUST=3: OFAM currents + Smagorinsky = 0.3
ROBUST=4: OFAM currents + Smagorinsky = 0.4
ROBUST=5: OFAM currents + Smagorinsky = 0.5
ROBUST=6: OFAM currents + constant viscosity + Smagorinsky = 0.1
ROBUST=7: Start from rest + constant viscosity + Smagorinsky = 0.1,
          Δt*=0.875
ROBUST=8: Start from rest + constant viscosity & diffusivity,
          Δt*=0.875
ROBUST=9: Start from rest + constant viscosity & diffusivity,
          Δt*=0.625
ROBUST=10: Start from rest + constant viscosity & diffusivity,
           Δt*=0.5
```

The `ROAMv2` configuration allows more choice of initial conditions, with choices of Smagorinsky or constant viscosity. The default is `ROBUST = 7`.

## ROAMv2

```
ROBUST=1: OFAM currents + Smagorinsky = 0.1
ROBUST=2: OFAM currents + Smagorinsky = 0.2
ROBUST=3: Geostrophic currents + Smagorinsky = 0.1
ROBUST=4: Start from rest + hard T/S relaxation + Smagorinsky = 0.1
ROBUST=5: Start from rest + Smagorinsky = 0.1
ROBUST=6: Start from rest + Smagorinsky = 0.2
ROBUST=7: OFAM currents + constant horizontal viscosity
ROBUST=8: Geostrophic currents + constant horizontal viscosity
ROBUST=9: Start from rest + constant horizontal viscosity
```

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ROBUST=10: As for ROBUST=9 with reduced time-step

A ROBUST 0 flag has been implemented that will use a more optimized configuration that one may typically use for a case study. While this configuration may have higher accuracy than standard ROAM configurations, it is also more prone to instability. This option is recommended only for more experienced modellers. The configuration is as follows:

- The model starts from rest,
- The k- $\omega$  mixing scheme is used,
- Smagorinsky horizontal diffusion is used with a constant of 0.1, with 2 smoothing passes,
- The ULTIMATE QUICKEST tracer advection is used,
- Boundary sponges of 8 cells ramp to 5 times the interior value,
- No active alerts,
- Flux adjusted open boundaries using the default timescale.

The ROAMv3 configuration allows horizontal mixing to be explicitly set, with ROBUST controlling the initial condition. There are only 5 levels in this configuration. The default is ROBUST = 4.

## ROAMv3

ROBUST=1: Initialisation with OFAM currents  
ROBUST=2: Initialisation with geostrophic currents  
ROBUST=3: Start from rest + hard T/S relaxation  
ROBUST=4: Start from rest  
ROBUST=5: Start from rest,  $\Delta t^*=0.5$

The ROAMv4 configuration is the same as ROAMv3 except TPXO tidal forcing is performed if a TPXO tide file (see Section 4.11.23) is supplied. The ROAMv5 configuration is the same as ROAMv5 using TPXO tidal velocity forcing on the open boundaries as well as a flux adjustment using TPXO tidal elevations. The ROBUST levels for ROAMv5 are:

## ROAMv5

ROBUST=1: Initialisation with OFAM currents + dual relaxation  
ROBUST=2: Initialisation with OFAM currents  
ROBUST=3: Start from rest + hard T/S relaxation + dual relaxation  
ROBUST=4: Start from rest + hard T/S relaxation  
ROBUST=5: Start from rest + dual relaxation  
ROBUST=6: Start from rest

The horizontal mixing is set using the following:

```
SMAGORINSKY b1.s1 b2.s2 b3.s3 b4.s4
```

Where  $b_1$  and  $b_2$  are base viscosities in the  $e_1$  and  $e_2$  directions respectively expressed as a percentage of the automatically computed optimum constant viscosity,  $b_3$  and  $b_4$  are base diffusivities in the  $e_1$  and  $e_2$  directions respectively expressed as a percentage of the automatically computed optimum constant diffusivity, and  $s_1$ ,  $s_2$ ,  $s_3$  and  $s_4$  are empirical Smagorinsky constants for viscosity and diffusivity. The Smagorinsky mixing is added to the base rate when applied in the mixing scheme. An example using a base viscosity with no added Smagorinsky, and Smagorinsky diffusion with no base rate is given by:

```
SMAGORINSKY 100.0 100.0 0.1 0.1
```

Using ROAMv = RECOMv1 sets the ROBUST parameterisation as:

## RECOMv1

ROBUST=1: Same as ROBUST 0 above, Smagorinsky, no alerts  
ROBUST=2: Same as ROBUST 0 above, constant viscosity, no alerts

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ROBUST=3: Same as ROBUST 1, active alerts  
ROBUST=4: Same as ROBUST 2, active alerts  
ROBUST=5: Standard ROAM parameterisation,  $Smag = 0.1$ , rest start  
ROBUST=6: Standard ROAM parameterisation,  $Smag = 0.1$ , OFAM start  
ROBUST=7: Rest + hard T/S ramp relaxation + Smagorinsky = 0.1  
ROBUST=8: Rest + hard T/S ramp relaxation + Smagorinsky = 0.1  
ROBUST=9: OFAM currents + constant horizontal viscosity  
ROBUST=10: Start from rest + constant horizontal viscosity

As mentioned, the time-step parameterisation using the `-r` option is very conservative. Speed may be increased using the `SPEED` parameter which is assigned from 1 to 10. The speed is controlled by altering the 'safety factor' applied to the CFL condition. The ROAM 'safety factor' is assigned a value 0.4 (note; 0.8 is used for `-a` option), and further decreases depending on the maximum depth. If `SPEED = 1` then the safety factor is unchanged. For `SPEED > 1` the safety factor linearly scales to 0.9 for `SPEED = 10`. Using `SPEED = 10` will generally double the time-step used, and still satisfy the CFL condition.

## 8 Input file generation (-g option)

The input netCDF file containing initial values for the model variables over the model grid and the model geometry / bathymetry required to run SHOC/COMPAS using the `-p` option may be generated from any parameter file using the `-g` option, i.e.

```
shoc -g prmname infile.nc
```

where `prmname` is the name of the model parameter file and `infile.nc` is the name for the generated input netCDF file. Note that whenever initialization data is changed (e.g. `TRACER?.data`), model geometry is changed (e.g. number of `LAYERFACES`) or the bathymetry is changed a new input netCDF file must be generated.

### COMPAS only

A COMPAS mesh may be partitioned into numerous tiles having the same underlying mesh as the original. This is achieved using:

```
COOKIE_CUT file.bncc t1 t2 ... tn tname
```

This will make `.prm` files `tnamet1.prm`, `tnamet2.prm` etc. using the regions `t1 t2 ... tn` specified in the region file `file.bncc`.

The tiling may be set up for 2-way nesting using:

```
COOKIE_CUT file.bncc t1 t2 ... tn tname sf bf 2way
```

where `sf` = separation interface (cells, typically 2) and `bf` is a Boolean flag indicating if barotropic coupling is to be configured; `bf = 0`, `NO`, `FALSE` no barotropic coupling, `bf = 1`, `YES`, `TRUE` for barotropic coupling. The 2-way nesting configuration is set up according to the methodology described in Herzfeld and Rizwi (2019).

When the `-g` option is invoked with a `COOKIE_CUT` specification, a set of `.prm` parameter files with accompanying mesh specification are generated for each box specified (`t1 t2 ... tn`) in the region file. Included in this are the locations of the open boundaries required to prescribe OBC information (or exchange information across a 2-way interface). For 2-way configuration, the level of overlap, or interface separation, of these boundaries may be specified by the user. Also, output multi-dumpfile specifications (named `df_tnamet#.txt`, with additionally the data for exchange between e.g. regions `t1` and `t2` in `df_tilet1-t2.txt`) are created containing the locations required for information exchange in 2-way nesting (temperature, salinity and elevation at cell centres, and normal and tangential boundary velocity at cell edges). For barotropic coupling these files also contain output of depth averaged velocities. Aside from these additions, the tile parameter file is a mirror image of the host model in terms of parameterization and forcing.

## 9 Transport mode (-t option)

The transport option allows import and processing of offline data, and export of those data. In its simplest form (`TRANS_MODE = NONE`) only scheduled functions are invoked by the model as it runs. This includes atmospheric input, tracer resets, time series output and netCDF output. This allows, for example, data input via tracer resets, and output of those data into a different netCDF format.

If `TRANS_MODE = SP_DUMP` then open boundary routines are added to scheduled functions. This allows open boundary data to be imported in the same manner as during a run using `-p`, and output to file at a specified frequency or format for later use.

Using the `TRANS_MODE` options `SP_EXACT`, `SP_INTERP`, `XYZ_INTERP`, `GLOBAL` or `SIMPLE` allows data to be imported from the file specified by `TRANS_DATA`. These offline data comprise of sea level, temperature & salinity, velocities and vertical diffusivities. All tracer diagnostics, including sediment transport, biogeochemistry, tracer statistics, source/sinks, particle tracking and SHOC/COMPAS diagnostics will function in this mode. This then allows conservative, long-timestep transport of tracers to be performed using the Flux Form semi\_lagrange scheme; `TRA_SCHEME = FFSL`; If this is `TRA_SCHEME = NONE` then no tracer transport is performed, however, particle tracking or access to model and tracerstats diagnostics may still be performed. If `TRANS_MODE` is `XYZ_INTERP`, `GLOBAL` or `SIMPLE`, then tracer transport may only be achieved using non-conservative semi-Lagrange schemes (`TRA_SCHEME = LAGRANGE`), as these files do not contain enough information for conservative transport. The `LAGRANGE` scheme is unconditionally stable allowing increased time-steps (e.g. 1 hour) to be used which dramatically increases run time ratios. The scheme is, however, also quite diffusive.

The concept of using offline velocities to drive a transport model is not new, however, in practice it is rarely used due to the enormous amounts of disk space required to run for extended periods. This problem is circumvented by generating the offline velocity/diffusivity files with a sparse file format (Section 4.31.6) which eliminates land from the dumpfile and can lead to large saving in disk space (savings up to 90% are possible). I/O overhead can be reduced if the sparse format file is read into SHOC/COMPAS without interpolation, i.e. the dumpfile contains information on **exactly** the same grid as the transport model is using for **exactly** the times required. This input is achieved using `SP_EXACT`.

The transport option requires a standard input file for initialization, from which model initial conditions, grid, layer structure and bathymetry are defined. A forcing file containing the variables `eta`, `u1`, `u2`, `w`, `Kz` must also be supplied (only `u1` is supplied for COMPAS). If the grid definition is incompatible with the forcing file the model will terminate with an error. The variables `temp`, `salt` may optionally be included in the forcing file if the `advect` and `diffuse` attributes are false for these variables in the tracer list. A transport mode is also defined to specify the format of the offline file, which has consequences for the speed at which I/O is performed. To define input and offline data a transport parameter file is created which defines:

```

INPUT_FILE          in.nc          # Initialisation file

TRANS_DATA          offline.nc     # File containing eta, u1, u2 (SHOC), w
                                # and Kz.
                                # This may be a multifile using
                                # variable substitution.

TRANS_MODE          NONE           # No reading of forcing data and no
                                # advection is performed. Useful for
                                # format conversion using tracer reset
                                # capability in conjunction with
    
```

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```

# different forms of file output.
SP_DUMP      # Same as NONE except open boundary
              # routines are also exercised.
              # Useful for outputting OBC data into
              # different formats of temporal
              # frequencies.
SP_EXACT     # The TRANS_DATA file is expected to
              # be in sparse format, with time
              # records corresponding exactly to the
              # input intervals required by the model
              # (determined by the start time and
              # time-step).
SP_INTERP    # TRANS_DATA is in sparse format
              # (contains information on exactly the
              # same grid as the transport model) but
              # may be at different times to the
              # input interval (interpolation in time
              # is performed which slows I/O).
XYZ_INTERP   # TRANS_DATA is in standard format and
              # may be spatially and temporally
              # different to the grid. Interpolation
              # in space and time is performed on
              # input. The slowest method using the
              # most disk space.
GLOBAL       # Reads BRAN or OceanMAPS global data
              # and reads eta_t, T/S, u and v into
              # the model variables. Velocities are
              # rotated onto the grid.
SIMPLE       # Reads SIMPLE formatted data
              # and reads eta, T/S, u and v into
              # the model variables. Velocities are
              # rotated onto the grid.
SP_CHECK     # Used to check transport data files
              # for NaN values or values greater than
              # specified limits (etamax & velmax).
              # Set TRANS_DATA to the file required
              # to be checked when using this mode.
TR_CHECK     # Checks the input data for NaN and
              # values greater than specified limits,
              # and checks valid source cells &
              # interpolation weights (>0 and <1)
              # are computed.
```

Monthly transport files in sparse format can be automatically generated when running a model in `-p` mode using:

```
TRANS_OUTPUT      YES
TRANS_DT          1 hour      # optional dump increment
```

In this case the transport files will be created for each month with the name `prmname_trans_mmmmyyyy.nc` where `'prmname'` is the name of the parameter file, `mmm` is the month (e.g. `'jan'`) and `yyyy` is the year. An alternative to `prmname` can be generated using `OutputTransport` (Section 4.32.6). Files are output in `'sparse'` format. Variables output are `eta`, `ulmean`, `u2mean`, `wmean`, `temp`, `salt` and `Kzmean` (`swr` is also output if present). The mean variables required for output are automatically invoked. The default dump increment is 1 hour, unless specified using `TRANS_DT`.

### SHOC only:

Note that `TRANS_OUTPUT` may be used in transport mode when wishing to dump multi-grid output (for the `STREAMLINE` mode; see below). In this case output variables are `eta`, `u1`, `u2`, `temp`, `salt`, `Kz`, `origin`, `p`, `q` and `r`.

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Note that if a list of tracers is generated for the transport mode then the tracers must have unique names, e.g. if `eta`, `u1`, `u2` or `w` are used as tracer names then these will be in conflict with the prognostic variables of those names, and output may not be correctly generated (`u1` and `u2` will not output to `standard` files, `u` and `v` will not output to `simple` files). This is especially relevant when using `TRANS_MODE = NONE`.

Additionally the following attributes are mandatory in the transport parameter file (see Section 4 for a description of these parameters):

```
CODEHEADER          SHOC default version      # Code version
PARAMETERHEADER     Transport model          # Header text
TIMEUNIT            seconds since 1990-01-01 00:00:00 +08
OUTPUT_TIMEUNIT     days since 1990-01-01 00:00:00 +08
LENUNIT             metre
START_TIME          1866 days
STOP_TIME           1897 days
DT                  1 hour                  # Transport timestep
HMIN                0.02                   # The minimum layer thickness
Z0                  0.002                  # Bottom roughness - optional :
                                      # required for sediment transport only.
NAME                # Comments (optional)
```

A tracer list (Section 4.10) and the definition of the open boundaries (Section 4.11) is also required. The latter is required so that the open boundary conditions for any additional tracers may be defined. Open boundary conditions for `temp` and `salt` are best created offline and stored in a point array file, in conjunction with the `FILEIN` open boundary condition. The `UPSTRM` open boundary condition is reconfigured for the transport mode to use the characteristic for outward flowing velocity.

Additionally, any diagnostics (e.g. source / sink, particle tracking, mixed layer, diagnostic numbers, flushing times, steric height, conservation diagnostics, tracer statistics) and any surface forcing (e.g. `HEATLUX` for `temp`, `SALTFLUX` for `salt` : these may require additional atmospheric input) may be specified in the transport parameter file.

Additional tracers may exist in the forcing file, and these may be reset in the transport mode by listing the names of these variables using the `TRANS_VARS` attribute, e.g;

```
TRANS_VARS          NO3 Chl_a sand silt
```

If the time-step does not violate stability criteria, alternative advection schemes may be used. The `ULTIMATE` and `STABILITY` options may be used in conjunction with this. Often the velocity fields read into the transport model (snapshots or means) are not conservative in the sense that the divergence of the depth averaged velocity does not always equal the change in elevation over the time-step. This can lead to conservation errors using advection schemes solved using the flux method. Conservation may be forced locally in time by computing the change in elevation over the time-step and vertical velocity from the specified velocity distributions. This maintains conservation for tracers using non semi-Lagrangian advection schemes, and is invoked using:

```
CONSERVATION        YES      # Force volume conservation
```

The sea level may be re-initialized to that in the transport file or left to evolve over time by using;

```
CONSERVATION        RE_INITIALIZE      # Force volume conservation with
                                      # eta re-initialization.
CONSERVATION        NO_INITIALIZE      # Force volume conservation with
                                      # no eta re-initialization.
```



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Additionally only vertical velocity or sea level may be forced to conserve by adding `W` or `ETA` to the `CONSERVATION` specification, e.g;

```
CONSERVATION      NO_INITIALIZE ETA
CONSERVATION      RE_INITIALIZE W
```

The default is `CONSERVATION = RE_INITIALIZE W ETA`.

For the `FFSL` scheme (see below), vertical velocity may be only recomputed in the water column if the new vertical velocity does not violate the Lipschitz condition using `WSTAB` instead of `w`.

Note that the semi-Lagrangian scheme is not compatible with multi-processing, hence the transport model will only operate on one window unless an alternate advection scheme is specified. The order of the semi-Lagrange advection scheme may be specified using:

## SHOC only

```
ORDER_SL  0      # Original tri-linear formulation.
ORDER_SL  1      # 1st order tri-linear (same as ORDER_SL = 1)
ORDER_SL  2      # 2nd order tri-quadratic
ORDER_SL  3      # 3rd order tri-cubic
ORDER_SL  4      # 4th order tri-quartic
```

## COMPAS only

```
ORDER_SL  LINEAR      # Linear interpolation on a triangulation
ORDER_SL  BAYLINEAR   # Same as linear using baycentric
                  # interpolation.
ORDER_SL  BILINEAR    # Bi-linear interpolation (quad grids only)
ORDER_SL  QUADRATIC   # Least squares quadratic interpolation
ORDER_SL  CUBIC       # Least squares cubic interpolation
ORDER_SL  NN_SIBSON   # Sibson natural neighbours
ORDER_SL  NN_NON_SIBSON # Non-Sibson natural neighbours
```

The default is `ORDER_SL = 0` for `SHOC` and `LINEAR` for `COMPAS`. The higher order schemes are non-monotonic and require a monotonicity constraint to be applied. The higher the order, the slower the scheme.

Speed is reduced if IO is excessive, hence any variables read into the model from file should have an `INPUT_DT` at least as much as the timestep used (e.g. don't input a variable at `INPUT_DT=10` minute intervals, or output data with `tinc = 10` minutes if the timestep `DT=1` hour). Additionally, if file input or output is less than the time-step, then the model will effectively run using the smaller time-step; this may cause the semi-Lagrangian scheme to become stuck in an infinite loop.

The transport model may be used with input fields derived from other models (e.g. MOM). Sometimes these models do not account for leap years in their simulation; to account for this specify:

```
NO_LEAP_YEARS      YES      # Always use 365 days per year
```

A transport parameter file may be generated from a full parameter `.prm` file when using the `-g` or `-p` option by including `TRANS_DATA` in that parameter file. The name of the transport file in this case is `<INPUT_FILE>.tran`; e.g. if the input file in the `.prm` file is `'infile.nc'`, then the transport filename will be `'infile.tran'`. To invoke this use:

```
TRANS_DATA          dummy.txt
```

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If `TRANS_MODE = SP_DUMP` in the `.prm` parameter file, then a transport file will be similarly generated containing the specification for model forcing import/export using the `SP_DUMP` mode.

Alternatively, a transport file template may be generated from parameter file `<in.prm>` using;

```
compas -at <in.prm>
```

When the transport mode is invoked using semi-Lagrangian advection, a tracer `vi` with long name 'Volume error' is created which contains the volume conservation error (in  $\text{m}^3$ ) for each cell resulting from the use of the semi-Lagrange scheme.

## 9.1 Multiple grids (SHOC only)

It is possible to perform transport on a subset of the grid used to save the transport files. In this case, the streamline origin is computed on the source grid, which is defined as the grid on which the `TRANS_DATA` were created, and the values of tracer variables are interpolated on a different target grid. All output is performed on the target grid. The target grid must lie completely within the source grid, and will conform to one of the following:

1. The target grid may be an exact duplicate of the source grid. This may be for a smaller subset of the source grid. In this case the target grid is defined as having an `EXACT` relationship to the source grid, and resolution of source and target grids are the same.
2. The target grid may be a decimation of the source grid, i.e. 4, 9, 16 etc. source cells may be grouped to form a target cell, so that the target grid has coarser resolution than the source grid. In this case the target grid is defined as a `SUBSET` of the source grid.
3. The target grid is completely different to the source grid. An example of this may be a target grid created at higher resolution than the source grid. These grids are defined as a `SUPERSET`.

To perform transport on multiple grids, a `SOURCE_GRID` must be defined in the parameter file. This is simply an input file containing the grid configuration one wishes to use as the source grid. The `TRANS_DATA` files must also be created on the source grid. The target grid is assumed to be defined as the grid nominated by the `INPUT_FILE` in the parameter file. These files must be created using the `-g` option. An example is as follows:

```
INPUT_FILE          in.nc          # Target grid
SOURCE_GRID         source.nc      # Source grid
```

The transport model will compare these grids to determine if the relationship is `EXACT`, `SUBSET` or `INEXACT`, and handle them accordingly. From a users perspective, the differences are that `EXACT` grids operate the fastest and `INEXACT` the slowest, owing to the amount of interpolation involved between grids.

## 9.2 STREAMLINE mode (SHOC only)

An intermediate step may be performed to create transport files that contain information regarding the streamline origin, rather than velocities used to calculate the streamline. This approach may increase execution speed since the streamline origin is no longer required to be calculated. If multiple grids are used, then potentially slow input of velocity information for the source grid may also be avoided.

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The `STREAMLINE` data files may be created when running the transport mode normally and dumping the variables `origin`, `p`, `q`, and `r` to `SPARSE` formatted files (Section 4.32.6). This file is then used to specify the `TRANS_DATA`, using the `STREAMLINE` option. Note that these `TRANS_DATA` input files to the `STREAMLINE` option cannot be interpolated in space and time, and must be read in exactly as written, hence the use of the `SPARSE` data format. Note also that this means that if `STREAMLINE` data files are created, the user is locked into using the time-step corresponding to that for which the files were created.

When using the `STREAMLINE` option, the input of data from file and transport computation are out of sync, necessitating reading `TRANS_DATA` information one time-step in advance. For this reason, when creating `STREAMLINE` data files, the stop time should be at least one time-step longer than the `STREAMLINE` transport is to run for.

Open boundary input is required if global `MONOTONIC` fills are used, so mass flux through open boundaries can be calculated. This information may be saved to file under normal operation of the transport mode, and re-read using the open boundary specification. Alternatively, complete `u1` and `u2` velocity fields may be saved to the `STREAMLINE` data files, which may be used in the global filling. This approach will be automatically invoked if `BCOND_NOR = NOTHIN` for all open boundaries. Note that when files are read into SHOC interpolation is always performed, even if the input file geometry and model grid are exactly the same; this can lead to slightly different numerical values entering the code compared to the values in the file. `SPARSE` formats do not suffer this problem, since no interpolation in space occurs when they are read into SHOC.

The `STREAMLINE` mode is invoked via:

```
TRANS_MODE          STREAMLINE
```

## 9.3 Conservation

The transport model is non-conservative for two reasons:

1. The semi-Lagrange scheme is cast in advective form and is non-conservative.
2. Continuity is not achieved when using snapshots or temporal averages of velocity and surface elevation fields. For a snapshot this is obvious; continuity is only achieved if the velocity is constant over the transport time-step. For temporal means, the elevation change over a time-step,  $\Delta\eta$ , is *not* equal to the horizontal divergence of depth averaged mean velocity multiplied by mean total depth, i.e.

$$\Delta\eta = \int_{t_1}^{t_2} \eta dt \neq \nabla_H \int_{t_1}^{t_2} D dt \int_{t_1}^{t_2} v dt$$

hence continuity is also not achieved.

The global filling attempts to compensate for these effects, and an option exists to impose a global fill on the tracer solutions to ensure conservation. This method computes the mass before advection, and the mass after advection accounting for input of mass through the open boundaries and due to source/sinks. If the scheme is conservative then mass before and after should equal. If not, then the excess or shortage of mass is distributed over all cells equally. This excess/shortage mass usually results in very small (multiplicative) adjustments to the concentrations in each cell. Furthermore, the mass adjustment may be computed so that resulting tracer values remain monotonic, i.e. the adjusted concentrations are not greater or less than the local maximum or minimum concentrations.

```
FILL_METHOD          NONE          # No conservation adjustment
                     GLOBAL        # Global filling
                     MONOTONIC     # Global filling ensuring monotonicity
```

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The default method is `FILL_METHOD = MONOTONIC`.

Continuity dictates that total volume in the whole domain at the end of the time-step is equal to total volume at the start of the time-step plus volume fluxes into the domain. Volume is not subject to errors from 1) above, so ideally (assuming volume fluxes are due to  $n$  open boundaries only):

$$V^t + \sum_n OBC_n = V^{t+1}$$

Any error from 2) can be compensated by adjusting the boundary fluxes by some factor  $f$ ;

$$f = \frac{V^{t+1} - V^t}{\sum_n OBC_n}$$

This factor may then be applied to mass fluxes for tracers in the transport model, so that the global fill factor is adjusted to reflect extra mass that would need to be added (or subtracted) if volume conservation were achieved in the domain. In practice continuity is not achieved in the 3D model at open boundary locations since velocity and elevation are prescribed independently via OBCs, and these OBCs rarely honour continuity (e.g. a radiation condition on elevation is often used with a no-gradient condition on normal velocity and zero tangential flow, leading to zero divergence but non-zero change in elevation). This can corrupt the above computation, therefore  $f$  is computed excluding open boundary cells, with boundary fluxes computed at the first interior location to open boundaries. The open boundary adjustment is invoked by including `OBC_ADJUST` in the `FILL_METHOD`, e.g. for `MONOTONIC` filling:

```
FILL_METHOD          MONOTONIC OBC_ADJUST
```

If the `MONOTONIC` transport mode is invoked, then a 2D diagnostic variable `vol_cons` is written to the output files which contains the volume error of each water column expressed as a percentage of total volume in each water column. This volume error is the difference between the volume at the end of a time-step and the sum of volume at the start of the time-step and volume flux divergence into the water column.

If `DIAGNOSE` is included in the `FILL_METHOD`, then a time series file containing the mass that must be added (or subtracted) to the domain for each tracer to achieve mass conservation, and the corresponding multiplicative fill factor is created. This also contains the total domain volume error and open boundary scaling factor.

## 9.4 Flux form semi-Lagrange

The flux form semi-Lagrange (FFSL) advection scheme, developed by Leonard et al. (1996) and Lin and Rood (1996), is a conservative advection scheme that can be used with the transport model. While not unconditionally stable, the scheme is constrained by the less restrictive Lipschitz condition, that basically ensures that streamlines cannot cross. The advantage of the FFSL scheme lies in that it is locally conservative. It is based on the 3<sup>rd</sup> order scheme of Van Leer, hence is more accurate than the 1<sup>st</sup> order semi-Lagrangian scheme. The FFSL scheme may be used in fully coupled mode, or in transport mode. For the latter, the average volume fluxes through cell faces must be additionally saved to the transport files. To invoke this when running `shoc` or `COMPAS` using the `-p` option, use:

```
TRANS_MODE          SP_FFSL # Save volume fluxes to transport files.
```

When running the transport model with the FFSL scheme, use:

```
TRANS_MODE          SP_FFSL # Use FFSL transport mode
```

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```
FILL_METHOD          NONE          # No fill method
TRA_SCHEME           FFSL          # FFSL advection
STABILITY            SUB-STEP-NOSURF # Enable sub-stepping
MERGE_THIN          YES           # Merge thin layers
CONSERVATION         ETA W        # Conservation options
```

### COMPAS only:

COMPAS can operate the FFSL scheme on a structured grid using transport forcing files generated by SHOC. In this case the FFSL scheme must be specified as:

```
TRANS_MODE           SP_FFSLS
```

Compas may also operate using the layered topology UGRID files that are typically output with COMPAS using:

```
TRANS_MODE           SP_FFSLU
```

If transport files are generated with COMPAS using the `-p` option in conjunction with `SP_FFSLU`, then the UGRID transport output files will also contain the cell and edge layer thicknesses, `dz` and `dzul`.

Note that an overhead is involved with remapping these files to the internal COMPAS coordinate system, which may impact computational efficiency.

Since vertical velocity is a diagnosed quantity, computed from the volume fluxes (which are accessible in the FFSL transport mode), it is possible to reconstruct the vertical velocity distribution. This is the recommended approach and is achieved by using:

```
CONSERVATION         W           # Enforce w conservation
```

The vertical velocity may be recomputed only if it does not violate the Lipschitz condition by using:

```
CONSERVATION         W WSTAB     # Enforce stable w conservation
```

If this occurs, then the tracer `vol_cons` will be assigned the value 1 at that water column. Sea level may be similarly recomputed; in this case sea level is updated to the computed value if that value and the value in the transport files differ by some threshold (currently  $1 \times 10^{-5}$  m). This is invoked using:

```
CONSERVATION         ETA         # Enforce  $\eta$  conservation
```

If this occurs, then the tracer `vol_cons` will be assigned the value 2 at that water column. If vertical velocity or sea level are re-computed (enforcing conservation), then any water fluxes input via point sources or sinks must be accounted for. These cannot be read in during the transport simulation in exactly the same manner as during the hydrodynamic simulation due to differences in time stepping, and are therefore also saved to the transport file during the hydrodynamic simulation. To minimize file size, these volume fluxes are saved to the vertical velocity variable in the transport file if point sources are specified in the hydrodynamic simulation with volume fluxes (i.e. hydrodynamic point source files contain `flow`), and copied to the point source volume flux variables when re-read in the transport mode. This only occurs if the point sources are also specified in the transport simulation with volume fluxes (i.e. transport point source files contain `flow`). To override this transfer of vertical velocity to volume fluxes in transport mode, use:

```
CONSERVATION         NO_PSS_FLOW # No volume flux transfer
```

A no-gradient condition can be enforced for each tracer before entering the FFSL advection scheme by using:

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```
CONSERVATION          NOGRAD    # Enforce no gradient conditions
```

This can assist in ensuring the transverse terms do not contain spurious data, however, should only be used if severe non-conservation is observed as this option has been known to degrade the solution in some applications.

If the transport files contain unreasonable data due to the hydrodynamic model tending toward instability, then this may be mitigated in the surface layer by merging volume fluxes and velocities using:

```
CONSERVATION          MERGED    # Merge surface layer volume fluxes
```

This should be a last resort option when trying to ensure conservation in the FFSL model.

To ensure that consistency (and hence conservation) occurs between hydrodynamic transport files and transport simulations, **ALWAYS USE THE SAME POINT SOURCE CONFIGURATION IN THE TRANSPORT MODE AS THAT SPECIFIED IN THE HYDRODYNAMIC SIMULATION.** If volume fluxes are used in the hydrodynamic simulation, then those same point sources in the transport mode must also use volume fluxes. If no volume fluxes are present in the hydrodynamic simulation, then do not specify volume fluxes for point sources in the transport mode.

The FFSL advection scheme is not as diffuse as the semi-Lagrangian scheme, and it may be desirable to explicitly include horizontal mixing, e.g.;

```
DIFF_SCALE            LINEAR
U1KH                  -0.455
U2KH                  -0.940
SMAGORINSKY           0.1
```

Note that if the `DYNAMIC` river open boundary is used in the hydrodynamic model (Section 4.10.6), then there will be inflow and outflow at the river open boundary in the transport model. If a `TRCONF` tracer open boundary condition is used, then the value supplied with the `TRCONF` OBC rather than the cell interior value will be multiplied by any outflow through the boundary face to get the boundary flux. This may result in negative boundary cell tracer concentrations.

## 9.5 Hints

- If the `TRANS_DATA` do not contain sufficient information for conservative transport (e.g. `TRANS_MODE = XYZ_INTERP, GLOBAL` or `SIMPLE`) then do not specify any `CONSERVATION` options.
- If `TRA_SCHEME = LAGRANGE` then it is useful to specify a ghost zone at open boundaries, so as to inform the scheme when a streamline may be exiting the domain through an open boundary. To do this, for each boundary, set;

```
BOUNDARY<n>.GHOST_CELLS    2
```

- While transport schemes may be unconditionally stable, the open boundary condition may not be. A `FILEN` OBC is generally safest to use, although `UPSTRM` is designed to work with `LAGRANGE`. `TRCONC` is designed to use with `FFSL`, although it appears more stable with `COMPAS`.

## 10 Percentile computations (-ps option)

SHOC can compute the percentile distributions, i.e. order statistics of temporal records (in increments of 5%-iles), of a time series file using:

```
shoc -ps prmname
```

The keywords required in the parameter file are:

```
P_IFILE      # Input file. This may be ASCII, netCDF, multi-netcdf or
              # sparse format (including multiple datafiles (Section
              # 4.32.2) sparse files.
P_OFILE      # Output file. If OutputPath is specified, the file is
              # placed in this directory.
P_VARS       # Variable names to compute percentiles.
P_STIME      # Start time of the computations relative to TIMEUNIT
P_ETIME      # End time of the computations relative to TIMEUNIT
P_DT         # Processing interval; subsamples the input file.
```

An example is as follows.

```
TIMEUNIT     seconds since 2000-01-01 00:00:00 +08
OutputPath   /home/work/

P_IFILE      inut.txt
P_OFILE      perc.nc
P_VARS       temp salt
P_STIME      10 days
P_ETIME      20 days
P_DT         12 hours
```

With `input.txt` containing:

```
multi-netcdf-version 1.0
nfiles 2
file0.filename  t1.nc
file0.filename  t2.nc
```

the files `t1.nc` and `t2.nc` may be sparse formatted files. Every record in the input file is read and included in the computations unless `P_DT` is specified, when every  $n$  record is included where  $n = (\text{P\_DT in seconds}) / (\text{output interval of P\_IFILE in seconds})$ .

## 11 File formats

**SHOC/COMPAS** uses two file formats for input and output data exchange. An ASCII time series column format and a multi-dimensional netCDF format. Both of these files support multiple variables, an unlimited number of time records, and the association of geometry with variables.

Typically ASCII time series files are used when a time series of multiple variables is required for a specific location, and netCDF files for input/output of time varying grid or multi-point data.

### 11.1 ASCII time series

An ASCII time-series file contains data formatted into columns and a header describing the number of columns, their names, units, missing values, etc. Typically the first column contains the time (which must monotonically increase) and the remaining columns the data and coordinate variables.

Following is a schematic representation of a time series file:

```
# Comments
## COLUMNS n
##
## COLUMN1.name time
## COLUMN1.long_name Time
## COLUMN1.units days since 1990-01-01 00:00:00 +10
## COLUMN1.missing_value -99999999
##
## COLUMN2.name XXXX
## COLUMN2.long_name XXXX
## COLUMN2.units XXXX
## COLUMN2.missing_value XXXX
##
.
.
.
##
v v v v ...
v v v v ...
v v v v ...
.
.
.
```

#### 11.1.1 Units

The units for each variables should follow the standard **udunits** conventions, however at this stage, other than time, no interpretation of the units is made by **SHOC/COMPAS**. Since **SHOC/COMPAS** uses SI units internally it is suggested that these units be adopted for all input variables.

An ISO date/time format has been adopted in for time units, it has the following syntax:

```
[units since ]yyyy-MM-dd [hh[:mm[:ss[.sss]]][ +|-hh[:ss]]]
|---- 1 ----| |-- 2 ---| |----- 3 -----| |-- 4 --|
1 - The scaling units (e.g. days, hours, seconds, ms, us, etc.)
2 - Date (year, month, day_of_month).
```



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- 3 - Time of day (hours, minutes, seconds, milliseconds).
- 4 - Time zone relative to UTC (+ or - UTC, hours, seconds).

All text enclosed within square brackets is optional.

## 11.1.2 Utilities

The time series format is well suited for use with standard plotting packages such as gnuplot or Matlab. Two Matlab scripts (`tsheader` and `tsread` have been installed in the Matlab software repository directory `/home/software/matlab`).

- `tsheader` reads the header from a time series file and returns a vector of structures each containing the time series file attributes as fields of the structure.
- `tsread` reads the header into a structure and returns a column vector of time's, and a matrix of the data records.

## 11.2 NetCDF time series

The netCDF file format is commonly used by many research organizations for the storage of time varying gridded data in a manner that it is platform independent. NetCDF also permits the association of attributes with any variable, this feature is extensively used by **SHOC/COMPAS** to describe the units, missing values, coordinate conventions, etc. The netCDF library was written by Unidata (<http://www.unidata.ucar.edu/>), and can be download from <ftp://ftp.unidata.ucar.edu/pub/netcdf/netcdf.tar.Z>. **SHOC/COMPAS** requires version 3 or higher.

All **SHOC/COMPAS** input/output dumpfiles are stored using netCDF.

### 11.2.1 Units

Units for netCDF variables are handled the same as for ASCII time series files.

#### 11.2.1.1 Coordinate conventions

The netCDF library provides a framework for reading and writing blocks of data, but it does not provide any implicit mechanism by which coordinate information is associated with data variables. This association needs to be explicitly made by the software reading the netCDF file.

To assist in automating this association, **SHOC/COMPAS** has adopted it's own coordinate convention for binding data variables and coordinate variables. The convention requires the specification of special attributes for both data and coordinate variables. Data variables contain a **coordinates** attribute which defines a list of coordinate variables associated with it. The coordinate variables contain an attribute **coordinate\_type** that describes the spatial coordinate this dimension corresponds to. Following is an example NetCDF CDL snippet:

```
netcdf file {
  dimensions:
    nrecord = UNLIMITED;
    ni = 10;
    nj = 20;
    nk = 5;

  variables:
    // Time coordinate variable.
```

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```
double t(nrecords);
    t:units="seconds since 1990-01-01 00:00:00 +10";
    t:coordinate_type="TIME";

// X coordinate variable of a 2d rectangular grid.
double x(nj, ni);
    x:units="m";
    x:coordinate_type="X";
    x:analytic="rectangular 0 0 10 20 0 0 1000 1000 0";

// Y coordinate variable of a 2d rectangular grid.
double y(nj, ni);
    y:units="m";
    y:coordinate_type="Y";
    y:analytic="rectangular 0 0 10 20 0 0 1000 1000 0";

// Z coordinate variable.
double z(nj, ni);
    z:units="m";
    z:coordinate_type="Z";

// Each record, and dimension has a unique T, X, Y and Z
// coordinate associated with it. The coordinates are stored
// in units of m.
double salt(nrecords, nk, nj, ni);
    salt:units="practical salinity units";
    salt:long_name="Salinity";
    salt:coordinates="t, x, y, z";
};
```

In the above example, the salinity variable represents a four dimensional gridded data object. The **coordinates** variable associates with this the t, x, y, and z coordinate information. Note that all dimensions used in the salinity variable are collectively found in the coordinate variables, and there are no additional dimensions.

The optional **analytic** attribute should be specified for coordinate systems where a simple analytically definition is possible (e.g. rectangular grids). The inclusion of an **analytic** attribute permits faster and more accurate conversion between coordinate and indice space. **SHOC/COMPAS** currently understands both rotated rectangular and polar grids. The attribute should be associated with each coordinate variable.

To define an analytic attribute for a rectangular grid, use the following syntax:

```
var:analytic = "rectangular ioff joff ni nj x0 y0 dx dy rot";
ioff - I offset within the grid 0 is grid edge 0.5 is centre.
joff - J offset within the grid 0 is grid edge 0.5 is centre.
ni - number of grid points along i dimension (one more than number
of cells).
nj - number of grid points along j dimension (one more than number
of cells).
x0 - X coordinate origin.
y0 - Y coordinate origin.
dx - Width of cell in X direction.
dy - Height of cell in Y direction.
rot - Mathematically defined angle of rotation of grid.
```

To define an analytic attribute for a polar grid, use the following syntax:

```
var:analytic = "polar ioff joff ni nj x0 y0 rmin arc";
ioff - I offset within the grid 0 is grid edge 0.5 is centre.
joff - J offset within the grid 0 is grid edge 0.5 is centre.
```

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ni - number of grid points along i dimension (one more than number of cells).  
nj - number of grid points along j dimension (one more than number of cells).  
x0 - X coordinate origin.  
y0 - Y coordinate origin.  
rmin = Minimum radius.  
arc = Angular width of cell.

This example netCDF CDL snippet defines a geographic grid. If a `PROJECTION` parameter was specified as the default coordinate system, then SHOC/COMPAS will automatically convert from geographic coordinates to the map projection (if necessary), when reading the data file.

```
netcdf file {
  dimensions:
    nrecord = UNLIMITED;
    ni = 10;
    nj = 20;
    nk = 5;

  variables:
    // Time coordinate variable.
    double t(nrecords);
    t:units="seconds since 1990-01-01 00:00:00 +10";
    t:coordinate_type="TIME";

    // Latitude coordinate variable of a 2d rectangular grid.
    double lat(nj, ni);
    lat:units="degrees_east";
    lat:coordinate_type="latitude";

    // Longitude coordinate variable of a 2d rectangular grid.
    double lon(nj, ni);
    lon:units="degrees_east";
    lon:coordinate_type="longitude";

    // Z coordinate variable.
    double z(nj, ni);
    z:units="m";
    z:coordinate_type="Z";

    // Each record, and dimension has a unique T, X, Y and Z
    // coordinate associated with it. The coordinates are stored
    // in lat/lon units.
    double salt(nrecords, nk, nj, ni);
    salt:units="practical salinity units";
    salt:long_name="Salinity";
    salt:coordinates="t, lon, lat, z";
};
```

This a snippet demonstrate how to define a 3d grid with a map projection (Australian Map Grid):

```
netcdf file {
  dimensions:
    nrecord = UNLIMITED;
    ni = 10;
    nj = 20;
    nk = 5;
```

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```
variables:
  // Time coordinate variable.
  double t(nrecords);
    t:units="seconds since 1990-01-01 00:00:00 +10";
    t:coordinate_type="TIME";

  // X coordinate variable of a 2d rectangular grid.
  double x(nj, ni);
    x:units="m";
    x:coordinate_type="X";
    x:projection="proj=amg zone=55";

  // Y coordinate variable of a 2d rectangular grid.
  double y(nj, ni);
    y:units="m";
    y:coordinate_type="Y";
    y:projection="proj=amg zone=55";

  // Z coordinate variable.
  double z(nj, ni);
    z:units="m";
    z:coordinate_type="Z";

  // Each record, and dimension has a unique T, X, Y and Z
  // coordinate associated with it. The coordinates are stored
  // in AMG units.
  double salt(nrecords, nk, nj, ni);
    salt:units="practical salinity units";
    salt:long_name="Salinity";
    salt:coordinates="t, x, y, z";
};
```

Finally if the data is not stored on a grid but as a series of discrete points then an evaluation at an arbitrary point will use an inverse weighted interpolation scheme (1/r). Of course this assumes the **coordinates** and **coordinate\_type** attributes have been specified.

```
netcdf file {
  dimensions:
    nrecord = UNLIMITED;
    np = 1000;

  variables:
    // Time coordinate variable.
    double t(nrecords);
      t:units="seconds since 1990-01-01 00:00:00 +10";
      t:coordinate_type="TIME";

    // X coordinate variable of a 2d rectangular grid.
    double x(np);
      x:units="m";
      x:coordinate_type="X";

    // Y coordinate variable of a 2d rectangular grid.
    double y(np);
      y:units="m";
      y:coordinate_type="Y";

    // Z coordinate variable.
    double z(np);
      z:units="m";
```

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```
z:coordinate_type="z";

// Each record and point has a unique T, X, Y and Z
// coordinate associated with it.
double salt(nrecords, np);
salt:units="practical salinity units";
salt:long_name="Salinity";
salt:coordinates="t, x, y, z";
};
```

### 11.2.1.2 Utilities

The simplest way to view the contents of a netCDF file is to use the standard netCDF utility `ncdump`.

To view the file header, use:

```
ncdump -h filename
```

or to view the entire file, use:

```
ncdump filename
```

This gets impractical for large output files, and doesn't produce graphical output, this is particularly true for model dumpfile. Another way to view the netCDF dumpfiles is to use `jvismeco`, `olive` or `dive`, which can read these files and display the values of most variable. These techniques are useful for examining the model in detail, to find the cause of an instability, for example. However, it still doesn't allow you to save any sort of graphical output.

Modules to read and write netCDF files have been added to the commercial application Matlab (commonly used in the scientific community). Matlab is a good tool for analysing the model dumpfiles. A number of supplementary Matlab scripts (`mecoread2d`, `mecoread3d` and `ncinfo`) have been installed in the Matlab software repository directory `/home/software/matlab` for reading **SHOC/COMPAS** netCDF dumpfiles.

- `mecoread2d` reads a two dimensional variable and associated geometry from a **SHOC/COMPAS** file. Following is an example of how to use `mecoread2d`:

```
[xl,yl,ulav] = mecoread2d('out.nc','ulav',10);
```

- `mecoread3d` reads a three dimensional variable and associated geometry from a **SHOC/COMPAS** file. The data is returned as a 3d volume unless a specific layer is specified. Following is an example of how to use `mecoread3d`:

```
[xc,yc,eta] = mecoread3d('out.nc','salt',44);
```

or

```
[xl,yl,ulav] = mecoread3d('out.nc','u1',10, 151);
```

- `ncinfo` provides summary information about all variables within a netCDF file, and their dimensions.

```
ncinfo('out.nc');
```

## 12 Tests Cases

A suite of tests has been collected for the structured model. These tests are used to validate the model against analytic solutions or other known, simply understood situations. They are particularly useful to check the correct operation of the model after modifications to the model code.

These tests will also operate using COMPAS, although slight modification of the parameter file is required (e.g. momentum advection scheme).

### 12.1 No forcing

Test 1 is an extremely simple, null case, test, where no forcing is applied to a closed model domain. The purpose is to demonstrate that no model variables deviate from their initial values. A rectangular grid is used with a horizontal grid of 5 by 10 cells, and 5 layers in the vertical having 1m vertical spacing. The bathymetry varies and the water is initially vertically stratified. Vertical diffusion of salt and heat is turned off in this case to avoid diffusive changes. Each run consists of a 1000 second integration with no externally applied forcing. The initial variable values (zero elevation, zero velocity, salinity and temperature) should remain unchanged for the duration of the integration.

### 12.2 Ekman Spiral

A wind of constant stress and direction is blown over a homogeneous open ocean of constant depth. The model uses cyclic open boundaries reflect the open ocean condition, and utilizes constant vertical viscosity and linear bottom friction for simplicity. According to Kowalik and Murty (1993, p27) the linear resistance coefficient is related to the bottom drag coefficient via:

$$r = \rho C_d |v| \quad 12.2.1$$

where  $C_d$  is the drag coefficient,  $v$  is the bottom current speed and  $\rho$  is the density. Given a constant eddy viscosity, the Ekman depth,  $D_E$ , is given by (Pond and Pickard, 1983, p108):

$$D_E = \pi \sqrt{2V_z / |f|} \quad 12.2.2$$

where  $V_z$  is the eddy viscosity and  $f$  is the Coriolis parameter. The surface current speed,  $V_o$ , is then given by (Pond and Pickard, 1983, eqn 9.10):

$$V_o = \frac{\sqrt{2\pi\tau_s}}{D_E \rho |f|} \quad 12.2.3$$

where  $\tau_s$  is the wind stress, and the current speed,  $V_b$ , at the Ekman layer depth is (Pond and Pickard, 1983, p108):

$$V_b = V_o \exp(-\pi) \sim 0.04V_o \quad 12.2.4$$

Therefore, using a wind stress of  $0.01 \text{ Nm}^{-2}$  on an  $f$ -plane with  $f = 1e^{-4}$ , and  $V_z = 0.0507 \text{ m}^2\text{s}^{-1}$ , the Ekman layer depth  $D_E = 100\text{m}$ . Furthermore, using 12.2.3 with  $\rho = 1025 \text{ kgm}^{-3}$  gives  $V_o = 4.33 \times 10^{-3} \text{ ms}^{-1}$  and  $V_b = 1.87 \times 10^{-4} \text{ ms}^{-1}$ . Using the bottom velocity in 12.2.1 and a nominal drag coefficient of  $C_d = 0.003$  gives a resistance coefficient of  $r = 0.00058$ . Linear friction is achieved by setting the parameter `UF` to a large value and `Z0` to a low value. The value of `Z0` below which bottom drag is set to the parameter `QBFC` is given by:

$$Z_0 < \frac{0.5\lambda_{bot}}{\exp(\kappa q)(1/QBF\epsilon)} \quad 12.2.5$$

Using the value of  $QBF\epsilon$  quoted above,  $Z_0 < 7.7 \times 10^{-8}$ . Using these values with  $UF = 1.0$  provides linear bottom friction with the required resistance coefficient. Using the above configuration, model results should show an Ekman spiral with velocities rotating clockwise with depth, surface current speed  $\sim 0.0043 \text{ ms}^{-1}$  and bottom current speed  $\sim 0.00019 \text{ ms}^{-1}$ . Surface elevation should be equal to zero.

### 12.3 Constant wind stress – closed basin

This test examines the set-up due to a steady wind applied to a 1-layer (depth-averaged) model domain. If a constant wind is applied to a homogeneous closed basin of constant depth then depth averaged velocities are equal to zero in the steady state. For a linear model and constant wind stress in the x direction the surface slope should balance the applied wind stress, and the equations of motion reduce to an expression for the sea level gradient in the x direction:

$$\frac{\partial \eta}{\partial x} = -\frac{\tau_s}{\rho g L} \quad 12.3.1$$

where D is the water depth. If a wind stress of  $1 \text{ Nm}^{-2}$  is applied to a homogeneous ocean of temperature  $20^\circ\text{C}$  and salinity 35 psu so  $\rho = 1024.76 \text{ kgm}^{-3}$ , then the slope in a 10m deep basin is equal to  $9.958 \times 10^{-6}$ , and the depth averaged velocities should be near zero.

### 12.4 Constant wind stress – alongshore open channel

An analytical solution exists for a linear model of constant wind stress applied in a longshore direction along an infinitely long coast. Assuming cross-shelf transport and alongshore sea level gradient are small, then along shelf transport, U, is given by (Chapman, 1985, eqn 4.5):

$$U = \frac{D\tau_s}{\rho} (1 - \exp(-r/D)) \quad 12.4.1$$

with a steady state velocity ( $t \rightarrow \infty$ ) given by:

$$U = \frac{D\tau_s}{\rho} \quad 12.4.2$$

Note U is the transport, hence velocity  $u = U/D$ .  
The sea surface slope is given by (Chapman, 1985, eqn 4.6):

$$\frac{\partial \eta}{\partial y} = -\frac{fU}{gD} = -\frac{f\tau_s}{\rho g r} (1 - \exp(-r/D)) \quad 12.4.3$$

with steady state sea level given by:

$$\eta(y) = -\frac{f\tau_s}{\rho g r} \left(\frac{L}{2} - y\right) \quad 12.4.4$$

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where  $L$  is the width of the channel and it is assumed  $\eta=0$  at  $y = -L/2$ .

Cyclic open boundaries are used to represent an infinite coastline. Using a wind stress of  $0.1 \text{ Nm}^{-2}$  in a channel  $500\text{km}$  wide (the dimensions of this domain are the same as the test domain used by Palma and Matano (1998) except the Southern hemisphere is considered) with linear resistance coefficient  $r = 0.0005$ , Coriolis  $= -1.028e^{-4}$  and  $\rho = 1024.76 \text{ kgm}^{-3}$ , the along-shore depth averaged velocity is  $0.195 \text{ ms}^{-1}$ , the cross-shore depth averaged velocity is zero and elevation at the coast is  $0.49 \text{ m}$  (slope of  $2.05 \times 10^{-6}$ . Note the first elevation cell center is found at  $y = 10\text{km}$ ). This result assumes a linear depth averaged model is used, and a non-linear 3-D model with quadratic bottom friction is expected to give different results.

## 12.5 Constant wind stress – cross-shore open domain

A wind applied perpendicular to an infinitely long coastline (on the southern boundary in this case) will result in an elevation setup against the coast with zero depth averaged currents everywhere. The on-shore wind stress drives depth averaged flow to the west (east) in the northern (southern) hemisphere, and the sea level gradient resulting from setup at the coast drives this flow to the east (west). In a perfect situation the sea level gradient and wind stress forces balance resulting in no flow. Boundary effects and numerical error may make one of these forces dominate, leading to non-zero flow in the east (west) direction in the northern (southern) hemisphere if the sea level pressure gradient dominates, and vice versa if wind stress dominates. Assuming a linear model with linear bottom friction, the analytical solution for sea level profile is given by (Chapman, 1985, eqn 4.13a):

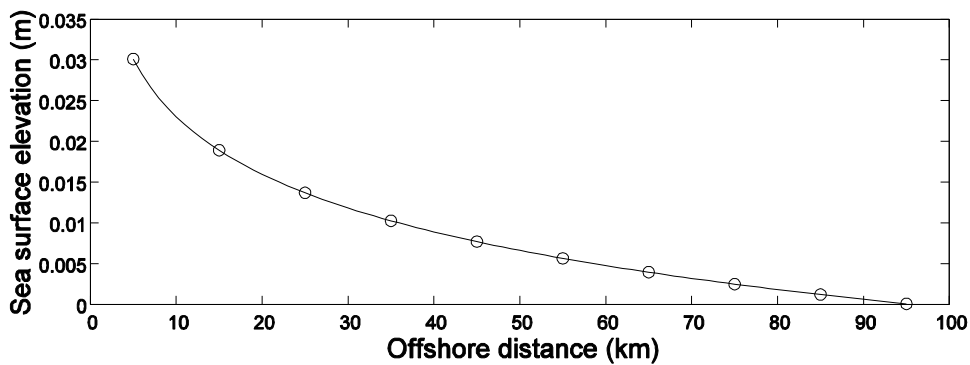
$$\frac{\partial^2 \eta}{\partial y^2} = -\frac{\tau_s}{\rho g D} \quad 12.5.1$$

Using a domain with two cyclic cross-shelf open boundaries and one offshore boundary with elevation clamped to zero, and the linear depth profile used by Chapman (1985, eqn 4.1), then the sea level profile is given by Chapman (1985, eqn 4.14) and shown in Figure 12.5.1 and Table 12.5.1. The boundary conditions of eqn. 12.5.1. for this domain are:

$$\frac{\partial \eta}{\partial y} = -D_0 \text{ at } y=0 \quad \therefore \quad \frac{\partial \eta}{\partial y} = \frac{\tau_s}{\rho g D} \text{ and } \eta=0 \text{ at } y=L \quad 12.5.2$$

where  $L$  is the distance to the offshore boundary.

Figure 12.5.1 : Sea level profile for onshore wind stress.





Offshore distance (km)	Surface elevation (m)
5	0.0301
15	0.0189
25	0.0137
35	0.0103
45	0.0077
55	0.0057
65	0.0039
75	0.0025
85	0.0012
95	0.0001

Table 12.5.1 : Sea level profile for onshore wind stress.

Again, a non-linear 3-D model with quadratic bottom friction is expected to give different results, and bottom friction is generally required to be increased for solutions to match theory. Specifically, adequate solutions were obtained using the `CONSTANT` mixing scheme with background vertical viscosity  $\nu_{z0} = 0.0507$  (see Test2) and minimum bottom drag coefficient of  $Q_{BFC} = 0.003$  ( $U_F = Z_0 = 1e-8$ ). Horizontal viscosity of  $U_{1VH} = U_{2VH} = 800$  is also required for stability.

## 12.6 Propagation of a bore

This test simulates a wetting bore propagating along an initially dry channel. The model domain represents a channel 2km wide and 100km long with uniform (flat) bathymetry. A constant velocity of  $1 \text{ ms}^{-1}$  is applied at one end of the initially dry channel. A bore propagates along the channel, with a parabolic shape (surface elevation profile) determined by a balance between the quadratic bottom friction and surface slope. The length of the bore is related to the depth at the inflow via:

$$L = \frac{gD}{2C_d U^2} \quad 12.6.1$$

## 12.7 Wind stress curl – closed basin

Wind stress possessing curl applied to a closed basin with a gradient of  $f/D$  results in the formation of a gyre due to conservation of potential vorticity which is biased to the east if  $f/D < 0$  and biased to the west if  $f/D > 0$  (e.g. Herzfeld and Tomczak, 1999). The gradient of  $f/D$  may result from a gradient of  $f$  ( $\beta$  effect) or a change in topography. This test consists of a closed basin in the southern hemisphere with constant depth in the east – west direction, 50m depth at the southern coast and 100m depth at the northern coast. Wind stress in the  $e1$  direction is applied, with  $0.1 \text{ Nm}^{-2}$  at the southern boundary and 0 at the northern boundary, hence this stress possesses negative curl. The gradient of  $f/D$  is positive in this case, thus an anticyclonic gyre biased to the west is expected, generated by topographically induced conservation of potential vorticity. Theory predicts that:

- A negative gradient of  $f/D$  (i.e. `CORIOLIS = 1.0e-4`) results in an eastward biased gyre.
- A flat bottom (`BATHYMAX = 50`) results in an unbiased gyre.
- Wind stress with positive curl (`WIND_SPEED_SCALE = -1`) results in a cyclonic gyre with unaltered bias.

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### COMPAS only:

COMPAS can generate several standard structured test cases for a closed basin, open channel and the test estuary, where the dimensions of the test case are scaled to NCE1 and NCE2, e.g;

```
TESTCASE    basin bmin bmax ref
            channel bmin bmax ref
            estuary bmin rmin
```

where:

bmin = bathymetry of the bay / minimum bathymetry of the basin/channel

bmax = maximum bathymetry of the basin

rmin = bathymetry at the head of estuary

ref = orientation (0 = slope in N-S direction) (1 = slope in E-W direction)

### 13 Tracer Statistics

A library named tracerstats exists in the directory ems/model/lib (see Figure 2.1) which allows various operations to be performed on existing tracers in the model. This includes sediment transport and ecological tracers if they exist. The tracerstats library offers a convenient way to perform processing on the fly rather than post-processing an output file. The advantage of using processing while the model is running is that statistics are computed at every time-step, rather than at the times data is dumped in an output file. Note that the tracerstats library must be present when the code is configured for the user to access this functionality.

The statistics available to be performed on 2D or 3D tracers are:

```
fluxel      # Flux of 3D tracer in the e1 direction
            usage:  TRACER<n>.tracerstat  fluxel(<3Dtracer>)
fluxe2      # Flux of 3D tracer in the e2 direction
            usage:  TRACER<n>.tracerstat  fluxe2(<3Dtracer>)
fluxw       # Flux of 3D tracer in the vertical direction
            usage:  TRACER<n>.tracerstat  fluxw(<3Dtracer>)
meanfluxel  # Mean flux of 3D tracer in the e1 direction
            usage:  TRACER<n>.tracerstat  meanfluxel(<3Dtracer>)
            optional: TRACER<n>.dt      <m> days
meanfluxe2  # Mean flux of 3D tracer in the e2 direction
            usage:  TRACER<n>.tracerstat  meanfluxe2(<3Dtracer>)
            optional: TRACER<n>.dt      <m> days
meanfluxw   # Mean flux of 3D tracer in the vertical direction
            usage:  TRACER<n>.tracerstat  meanfluxw(<3Dtracer>)
            optional: TRACER<n>.dt      <m> days
mean        # Cumulative moving mean of 2D or 3D tracer
            usage:  TRACER<n>.tracerstat  mean(<tracer>)
            optional: TRACER<n>.dt      <m> days
run_mean    # Exponential moving mean of 2D or 3D tracer
            usage:  TRACER<n>.tracerstat  run_mean(<tracer>)
            TRACER<n>.dt      <m> days
variance    # Variance of 2D or 3D tracer
            usage:  TRACER<n>.tracerstat  variance(<tracer>)
stdev       # Standard deviation of 2D or 3D tracer
            usage:  TRACER<n>.tracerstat  stdev(<tracer>)
corr        # Correlation coefficient of two 2D or 3D tracers
            usage:  TRACER<n>.tracerstat  corr(<tracer2>:<tracer>)
cov         # Covariance of two 2D or 3D tracers
            usage:  TRACER<n>.tracerstat  cov(<tracer>:<tracer>)
sum         # Sum of 2D or 3D tracers
            usage:  TRACER<n>.tracerstat  sum(<tr1>,<tr2>...
)
diff        # Difference of two 2D or 3D tracers
            usage:  TRACER<n>.tracerstat  diff(<tracer>:<tracer>)
max         # Maximum tracer value over a given time period
min         # Minimum tracer value over a given time period
vmax       # Maximum water column value of a 3D tracer
vmin       # Minimum water column value of a 3D tracer
vint       # Vertical integral of 3D tracer
            usage:  TRACER<n>.tracerstat  vint(<3Dtracer>)
vmean      # Vertical mean of 3D tracer
            usage:  TRACER<n>.tracerstat  vmean(<3Dtracer>)
vdiff      # The ratio of a series of layers of a 3d tracer
            usage:  TRACER<n>.tracerstat
                    vdiff(<3Dtracer>:<toprange>:<botrange>(strict))
copy       # Copy of a tracer
            usage:  TRACER<n>.tracerstat  copy(<tracer>)
copy_layer # Copy of a tracer layer (i.e creates a 2D
```

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```
# tracer)
Usage      TRACER<n>.tracerstat      copy_layer (<tracer>:<layer>)
# <layer> is 0 to nz, or 'surface' or 'bottom'
sectionflux # integrate the flux over a defined area and time
usage:     RTSTAT<n>.name      section(<3Dtracer>:<direction>)

rmse      # Compute the RMS error between two tracers
usage:     TRACER<n>.tracerstat      rmse (<tracer1>:<tracer2>)

exposure  # Exposure time of a tracer above/below a threshold
usage:     Tracer<n>.tracerstat
exposure (<3Dtracer>:<threshold>:<expose_time>)
optional:  TRACER<n>.dt              <m> days
optional:  TRACER<n>.start           <m> days
optional:  TRACER<n>.scale_factor    <m> days
```

where:

<3Dtracer> is a 3-dimensional tracer  
<tracer> is a 3-dimensional or 2-dimensional tracer

To initiate a tracerstat operation, an additional attribute TRACER?.tracerstat in the tracer list must be specified. The form of this attribute is of the type operation(tracer\_name), where operation is the statistic from the list above, and tracer\_name is the name of the tracer to operate on. For example, to specify the flux in the e1 direction of a tracer named temp, and output to a tracer called flux\_temp, the following tracer is specified;

```
TRACER?.name          flux_temp
TRACER?.long_name     Temp flux in e1 direction
TRACER?.tracerstat    fluxe1(temp)
TRACER?.fill_value_wc 0
TRACER?.valid_range   -1e-10 1e10
TRACER?.advect        0
TRACER?.diffuse       0
TRACER?.diagn         0
```

Note that these tracers are diagnostic and are not to be advected or diffused. Also, the diagn flag is turned off so that these tracers are not re-initialized to zero at every dump step. If a mean of tracer temp is required at 12 hourly intervals, use;

```
TRACER?.name          mean_temp
TRACER?.long_name     Average temp
TRACER?.tracerstat    mean(temp)
TRACER?.dt            12 hours
TRACER?.fill_value_wc 0
TRACER?.valid_range   -1e-10 1e10
TRACER?.advect        0
TRACER?.diffuse       0
TRACER?.diagn         0
```

The mean tracerstat is a cumulative moving mean ([https://en.wikipedia.org/wiki/Moving\\_average](https://en.wikipedia.org/wiki/Moving_average)) where if  $T_i$  are tracer values at model step  $i$  and  $\Delta t_i$  is the model timestep, then the cumulative mean is:

$$\bar{T}_i = \frac{\sum_i T_i \Delta t_i}{\sum_i \Delta t_i}$$

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so that

$$\bar{T}_{i+1} = \frac{\bar{T}_i \sum_i \Delta t_i + T_{i+1} \Delta t_{i+1}}{\sum_i \Delta t_i + \Delta t_{i+1}}$$

The `run_mean` tracerstat is an exponential moving mean, where if  $A = \text{TRACER}\langle n \rangle . dt$ , then:

$$\bar{T}_i = \begin{cases} T_1 & t=1 \\ \alpha T_i + (1-\alpha)T_{i-1} & t>1 \end{cases} \quad \text{where } \alpha = \Delta t / A$$

If the attribute `TRACER?.dt` is absent the mean for the whole simulation is calculated.

For statistics involving multiple tracers, the tracer names are separated by a colon in the `tracerstat` attribute. For example, to calculate the covariance of tracers `passive1` and `passive2` use;

```
TRACER?.name           covariance
TRACER?.long_name      Covariance of passive1 and passive2
TRACER?.tracerstat     cov(passive1:passive2)
TRACER?.fill_value_wc  0
TRACER?.valid_range    -1e-10 1e10
TRACER?.advect         0
TRACER?.diffuse        0
TRACER?.diagn         0
```

The variance, standard deviation and covariance statistics for any tracers also require that that tracer's mean be specified. The correlation coefficient of two tracers requires that those tracers' means and standard deviations are specified. The vertical integral, mean or difference of a 3D tracer is placed in a 2D tracer, e.g. to specify the vertical integral of a tracer `chl_a` use;

```
TRACER?.name           vint_chla
TRACER?.long_name      Vertical integral of chl_a
TRACER?.type           WC2D
TRACER?.tracerstat     vint(chl_a)
TRACER?.fill_value_wc  0
TRACER?.valid_range    -1e-10 1e10
TRACER?.advect         0
TRACER?.diffuse        0
TRACER?.diagn         0
```

The vertical difference tracer statistic calculates the difference between the sums of various layers, e.g.

$$vdiff \int_{toprange} \int_{botran}$$

where `toprange` and `botrange` are a list of individual layer numbers or layer ranges in the format `<from>_<to>`, separated by commas, e.g.

```
TRACER?.tracerstat     vdiff(salt:2,6,9_12:15_17,20)
```

will result in the sum of salinity concentration in layers 15,16,17 and 20 subtracted from the sum of salinity concentration of layers 2,6,9,10,11 and 12. The variable `strict` is given as 0 or 1 (with 0 used as the default). If `strict = 1` then the difference is given as zero if any of the layers in the `toprange` or `botrange` are not present, e.g. if one or more layers happens to lie below the sea bed.

The tracer statistics are computed in the order of the operation list provided above, hence it is possible to compute a statistic of a statistic if the order permits this. For example a vertical integral of a mean may be computed, but a mean of a vertical integral will result in operations performed at different time levels.

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In addition to the tracers in the tracer list, it is possible to compute tracers on the following 2D and 3D hydrodynamic variables;

```
eta    # sea level, 2D
Kz     # Vertical diffusivity, 3D
Vz     # Vertical viscosity, 3D
u1vh   # Horizontal viscosity in the e1 direction
u2vh   # Horizontal viscosity in the e1 direction
u1kh   # Horizontal diffusion in the e1 direction
u2kh   # Horizontal diffusion in the e1 direction
```

For example, the mean sea level may be calculated using:

```
TRACER?.name          mean_eta
TRACER?.long_name     Mean sea level
TRACER?.type          WC2D
TRACER?.tracerstat    mean(eta)
TRACER?.dt            12 hours
TRACER?.fill_value_wc 0
TRACER?.valid_range   -1e-10 1e10
TRACER?.advect        0
TRACER?.diffuse       0
TRACER?.diagn         0
```

The `exposure` tracerstat computes the time a nominated tracer's value is above or below a given threshold. The units of the exposure are the nominated tracer's units multiplied by days. To change the units, use the `scale_factor` (e.g. 7 days for units of <tracer units>.<weeks>). This tracerstat is effectively the integral of the tracer when its value is above/below the threshold. The optional `dt` provided is a time period that the tracer must be below/above the threshold in order for the exposure time to be reset to zero. The <exposure\_time> is the name of a tracer in the list that is used to keep track of how many days in the interval `dt` the tracer is below/above the threshold. This tracer is required primarily for housekeeping purposes. The `start` time is the time in model days that the exposure computation begins (the `START_TIME` is used as the default if this is absent). This allows the exposure tracerstat to operate with restarts. The <threshold> can be either a number or a tracer in the tracer list. The latter option allows a temporally and spatially varying threshold to be supplied. The threshold is the value the nominated tracer must be greater than by default; if this threshold is prefixed with '+' then the tracer must also be greater this threshold, if prefixed with '-' the tracer must be less than the threshold for the exposure to be incremented. For example, if an exposure is to be set up for salinity where the model salinity is integrated below values of 10 psu starting in summer 1990 (1 Dec 1990) using the tracer `salt_ex_time` as the exposure time, then use:

```
TRACER?.name          salt_exposure
TRACER?.long_name     Salinity exposure
TRACER?.units         psu days
TRACER?.tracerstat    exposure(salt:-10:salt_ex_time)
TRACER?.dt            1 day
TRACER?.start         334 days
TRACER?.fill_value_wc 0
TRACER?.valid_range   -1e-10 1e10
TRACER?.advect        0
TRACER?.diffuse       0
TRACER?.diagn         0

TRACER?.name          salt_ex_time
TRACER?.long_name     Salinity exposure time
TRACER?.units         days
TRACER?.fill_value_wc 0
TRACER?.valid_range   -1e-10 1e10
```

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```
TRACER?.advect      0
TRACER?.diffuse    0
TRACER?.diagn      0
```

In this case the salinity must be greater than 10 psu for 1 day at a location before the salinity exposure is reset to zero at that location. Note that `salt_exposure` may be integrated for periods greater than 1 day; the `dt` used only sets a time period for when `salt_exposure` is reset to zero. The salinity exposure time (`salt_ex_time`) contains the accumulated time (days) within the period `dt` that the salinity is actually below 10 psu; i.e. if salinity is below 10 psu for a full day then `salt_ex_time` will contain 1. If, for example, `dt` were 1 hour and salinity was below 10 psu for 36 minutes (0.6 hour) then `salt_ex_time` would contain 0.025 days. Although not the primary array of interest, the exposure time is required by this tracerstat to keep track of the instances when the exposure is reset to zero. The `salt_ex_time` must be zero for a period `dt` for the exposure to be reset to zero.

The `sectionflux` statistic is designed to calculate the integral of the flux of a tracer over a defined spatial area and time interval. The spatial area may be a vertical 'curtain' in the e1-z or e2-z plane, or a horizontal layer in the e1-e2 plane. The spatial area is defined by a list of (i,j) coordinates input via ascii file, with an optional top and bottom layer included. If the top and bottom layer are not present, the section is integrated over the entire water column. The user must specify in which `direction` the flux is to be calculated (e.g. `u1`, `u2` or `w`); it is the users responsibility to ensure this direction is perpendicular to the plane of the section (e.g. a flux in the `u1` direction must have a section defined in the vertical e2-z plane, or a flux in the `w` direction must have a section defined in the horizontal e1-e2 plane ). Note that the section must be defined along constant e1, e2 or z coordinates; if the section is defined across e1, e2 or z planes then the spatial integral will not be conservative.

The file containing a list of <i j> locations (or optionally <i j topk botk>) defining the section is specified using the `data` attribute. Again, if the `direction` is `u1`, then this list should contain constant i coordinates, etc.

The section is integrated in time over a timescale defined by the `dt` attribute, and subsequently output to an ascii file specified by the `output` attribute. Note that the integrating timescale may not be exactly the specified `dt`, since if `dt` is not an integral number of model time-steps output will be written to file at the next larger time-step. The output file contains the time and value of integrated flux over the section and interval `dt`.

A start time may be optionally defined by the `startt` attribute. The default is the model start time. The default time unit in the output file is that defined by `OUTPUT_TIMEUNIT` in the parameter file. This may be scaled by supplying optional attributes `tscale` and `tunit`, where output time format is `OUTPUT_TIMEUNIT / tscale (tunit)`. Similarly the units of the calculated flux may be optionally scaled using the attributes `outscale` and `outunit`, where integrated fluxes are written to the output file in units of (3D tracer unit) / `outscale (outunit)`.

This form of tracer statistic computes one number for each section which is written to a time series file, i.e. the result of the calculation is not a 2-D or 3-D field and is therefore not sensible to output to a 2-D or 3-D tracer. The syntax for the specification of `sectionfluxes` is therefore different. An example is given below, where the prefix `RTSTAT` refers to 'run time statistic'.

```
NRTSTAT 1
RTSTAT.name sectionflux(salt:u1) # type of run time statistic
RTSTAT.data bay_mouth.sect      # file containing (i,j) list
RTSTAT.dt 6 hours                # time interval to write output
RTSTAT.startt 3182 days          # (optional); start time for the
                                # section integration. Default is
                                # the model start time.
RTSTAT.tscale 6 hours           # (optional) time interval to
                                # write output.
RTSTAT.tunit minutes            # time interval to write output
RTSTAT.outscale 1000            # (optional) scaling factor for
                                # output flux.
```

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RTSTAT.outunit kg # (optional) output flux units.

The user may submit any number of individual sections.

A step attribute may be specified to compute `tracerstats` at a particular point in the sequence of computations within a time-step. This is invoked by prescribing:

```
TRACER?.step          n
```

Where the computational sequence is:

n = 1 : After computation of mixed layer depth, vorticity balance, flushing times, tracer percentiles, steric height and numbers.

n = 2 : After tracer decay, relaxation, increments and computation of totals.

n = 6 : After the wave library is called.

n = 3 : After the sediment library is called.

n = 4 : After the biogeochemistry library is called.

n = 5 : After the `tracerstats` library is called (i.e. statistics of statistics can be computed using `step = 5`).

Alternatively, these steps may be invoked via keywords, where:

PRE\_DECAY or POST\_DIAG corresponds to n=1

PRE\_WAVE or POST\_DECAY corresponds to n=2

PRE\_SED or POST\_WAVE corresponds to n=6

PRE\_ECO or POST\_SED corresponds to n=3

PRE\_RTSTAT or POST\_ECO corresponds to n=4

POST\_RTSTAT corresponds to n=5

For example, if `tracerstats` were to be invoked before the ecology library is called, then set:

```
TRACER?.step          PRE_ECO
```

or

```
TRACER?.step          POST_SED
```

If no step is specified, the standard `tracerstats` library call is between `step 4` and `5`.

The `tracerstats` library may be easily expanded to provide functionality suited to a user's specific needs.



## 14 CoastMesh (COMPAS only)

CoastMesh is a utility that allows extraction of coastlines for input into the meshing utility JIGSAW (Section 4.7.5) used with COMPAS.

An ascii file of closed loops containing the coastline must be supplied to coastmesh via the COASTFILE keyword.

```
COASTFILE          coast.cst
```

For each loop in the coastline file the format is:

```
lon1 lat1
lon2 lat2
.
.
lonn latn
lon1 lat1
NaN NaN
```

The coastline file may contain many small features that are not required to be in the mesh (e.g. small islands). These may be removed via several methods.

A CUTOFF orders the loops by the number of coordinate pairs in the loop, and only includes a certain top percentage of loops, e.g. if the smallest 80% of loops are to be removed use;

```
CUTOFF          80 # Exclude smallest 80% of loops
```

The RADIUS only includes loops with a radius greater than a certain distance (in m), e.g;

```
RADIUS          500 # Include loops with radius > 500 m
```

The LENGTH only include loops with a maximum end-to-end length of the feature greater than a certain distance (in m), e.g;

```
LENGTH          500 # Loops with end-to-end length > 500 m
```

A bounding box can be specified, and only loops residing within this box are included, e.g;

```
MINLON          146.66
MINLAT          -44.0
MAXLON          148.1
MAXLAT          -42.7
```

Individual loops in the coastline file may be removed by supplying a list of loop numbers to remove, e.g;

```
REMOVE_SEGMENT  2 5 12 # Remove loops 2, 5 and 12.
```

The coastline may be smoothed and resampled to assist in controlling the creation of very small meshes in detailed coastlines. This may be done prior or after small features have been removed (default is prior). Smoothing is prescribed using:

```
SMOOTH          # Number of smoothing passes
SMOOTHZ         # Number of coordinate pairs to include in smoothing
                # (boxcar filter size).
SMOOTH_PRE     # Same as SMOOTH
SMOOTHZ_PRE    # Same as SMOOTHZ
SMOOTH_POST    # As for SMOOTH, but performed after feature removal.
SMOOTHZ_POST   # Same as SMOOTHZ, but performed after feature removal.
```

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Note that `SMOOTHZ` is the number of coordinate pairs included in the smoothing either side of a central coordinate, i.e. the boxcar filter size is actually  $2 * \text{SMOOTHZ}$ .

Individual loops may be smoothed using:

```
SMOOTH_SEGMENT      S1:SM1:SZ1 S2:SM2:SZ2 ...   Sn:SMn:SZn
```

Where

$s_n$  = loop number

$sm_n$  = number of smoothing passes for this loop

$sz_n$  = Boxcar filter size for this loop

The coastline can be resampled, where every  $n^{\text{th}}$  coordinate pair is chosen from the coastline file to represent the coast;

```
RESAMPLE      n
```

Usually only a sub-sample of the largest coastline loop is to be used, and consequently a `START_COORD` and `END_COORD` must be supplied. These do not have to be exact coordinates from the coastline file; `coastmesh` will choose the coordinate pairs having the minimum distance to the supplied start and end. Since the coastline the start and end applies to should itself be a closed loop, different coastline paths may result if the loop is traversed in a clockwise or anticlockwise manner. Often the user does not know if the coastline has been defined in a clockwise or anti-clockwise sense, so we use a `MID_COORD` to define which portion of the loop is to be used. The `MID_COORD` should lie somewhere along the coast segment to be used in-between the `START_COORD` and `END_COORD`.

An example may be;

```
START_COORD      146.9214 -43.5995
END_COORD        147.7995 -43.2424
MID_COORD        146.9235 -43.581
```

There may be a need to link several coastline loops, for example a narrow estuary may not be required to be resolved to its limit but rather truncated at its mouth, or a narrow channel separating two loops may be desired to be breached so that one continuous coastline represents the two loops. A number of links may be defined to accomplish this, using:

```
LINKS           n
LINK0.start lon0s lat0s
LINK0.end   lon0e lat0e
LINK1.start lon1s lat1s
LINK1.end   lon1e lat1e
.
.
LINKn.start lonns latns
LINKn.end   lonne latne
```

Once a link connects one closed loop to another, the direction (clockwise or anticlockwise) the second loop is traversed should also be specified. This can be done using `LINKn.mid`, where the direction traversed is that which results in the minimum distance between `LINKn.end` and `LINKn.mid`. Alternatively `LINKn.dir` can be specified, where `+` corresponds to the direction the loop is represented as in the file, and `-` corresponds to the opposite direction the loop is represented as in the file. For example, if the loop is defined in a clockwise sense, then `-` will traverse the loop from the `LINKn.end` coordinate in an anti-clockwise sense.

An example may be:

```
LINKS           4
LINK0.start     147.1875 -42.7429
LINK0.end       147.1861 -42.7408
```

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```
LINK1.start      147.0553 -43.0409
LINK1.end        147.0549 -43.0402
LINK2.start      147.2734 -43.0247
LINK2.end        147.2727 -43.0244
LINK3.start      147.8023 -42.893
LINK3.end        147.8031 -42.894
LINK3.dir        +
```

Coordinates between link start and end locations are joined by a straight line. If some other path is desired to be inserted instead, then use:

```
LINKn.path <pathname.xy>
```

Where <pathname.xy> is an ascii file containing a list of longitude and latitude pairs (e.g. see the OBC path file specification below).

An example is illustrated in Fig. 14.1, where the red dots are the `START`, `END` and `MID` coordinates, the green dots are a link to remove an estuary, and the orange dots are a link to breach a channel. *It is the user's responsibility to ensure that the correct order and sense of link start and end coordinates are supplied so that a continuous path results.*

Open boundaries are usually required to close the coastline loops. These are included by specifying a number of path files, where each path file is a list of coordinates, e.g;

```
NOBC          1          # Number of open boundaries
OBC0          path1.xy   # File with path coordinates
```

The format of the path file is:

```
lon1 lat1
lon2 lat2
.
.
lonn latn
```

The purpose of the OBC is to join the `END_COORD` to the `START_COORD` and close the coastline path. If the OBC is itself a closed loop, within which the coastline loops reside, then specification of a `START_COORD` and `END_COORD` is not necessary (e.g. if, for instance, an island is to be represented within a single offshore boundary).

In Fig. 14.1 the open boundary is represented by the green segment. The closed loop within which a mesh is created then consists of starting at the `START` location on the coastline loop `LOOP0`, traversing the loop to the `MID` location and continuing to `LINK0`, where a section of the coast loop is excluded. The closed loop then continues to `LINK1` following the smaller coastline loop `LOOP1` in the direction through `Link1.mid` and terminating at the `END` location. The loop is closed by connecting the `END` location to the `START` location via the green `OBC0` segment.

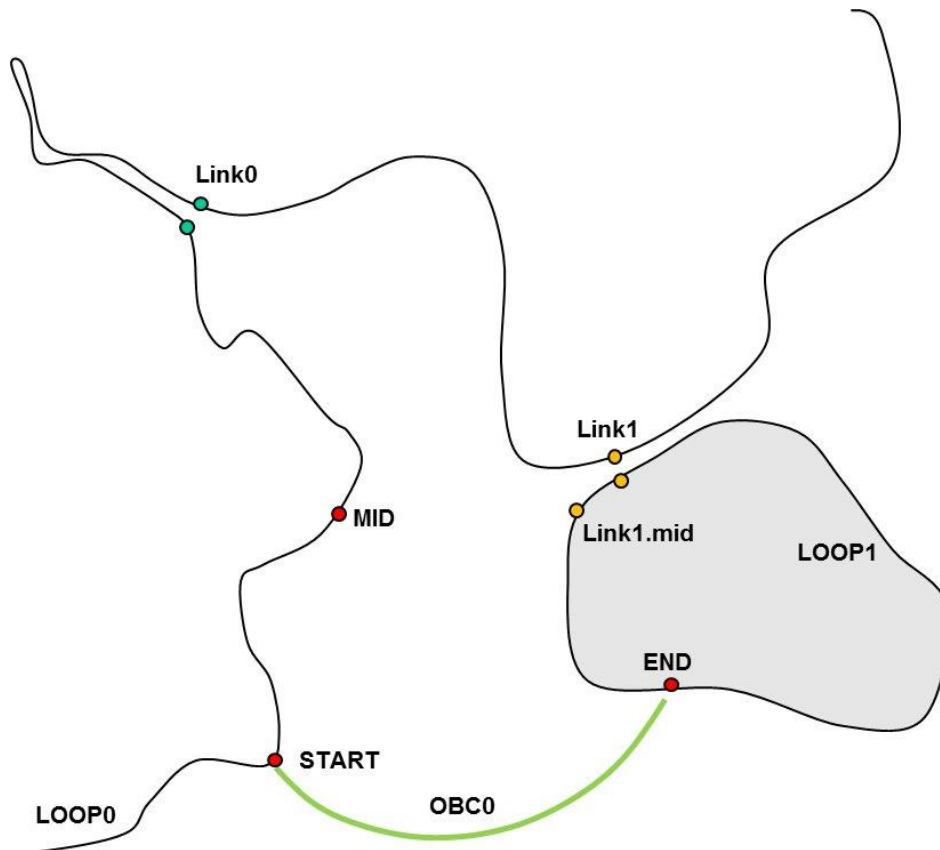


Figure 14.1: Example coastmesh configuration

A weighting can be supplied for input into JIGSAW:

```
HFUN_FILE <weighting.msh>
```

This must be in a JIGSAW compatible format (see <https://github.com/dengwirda/jigsaw> ).

Alternatively, a weighting function can be created based on bathymetry supplied via netCDF or text file:

```
HFUN_BATHY_FILE <bathy.nc> # netCDF file
HFUN_BATHY_FILE <bathy.bty> # ASCII file with format
                        # lon lat bathy
```

In this case, if present, HFUN\_FILE will be created containing a JIGSAW compatible .msh weighting file.

The bathymetry variable and dimension names that coastmesh will accept in the netCDF file are:

Variable name	X dimension	Y dimension	X coordinate	Y coordinate
bot_z	i_centre	j_centre	x_centre	y_centre
height	lon	lat	lon	lat

Alternatively, any 2D variable or time dependent 3D variable may be substituted for bathymetry using, e.g.:

```
HFUN_VAR salt # Use salinity as the weighting variable
```

In this case the HFUN\_BMIN and HFUN\_BMAX limits (see below) should be scaled relative to this variable's values. For three-dimensional data, the layer corresponding to 0.0 m is

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extracted from the netCDF file. For time dependent variables, by default the time record extracted from the file is at 0 days. An alternative record may be extracted using:

```
HFUN_TIME    <n> days
```

where <n> is the record time relative to the time units in the netCDF file.  
This bathymetry is interpolated onto a grid using an interpolation rule:

```
HFUN_INTERP_RULE <rule> # <rule>=linear: baycentric linear
                       # <rule>=cubic: cubic spline
                       # <rule>=nn_sibson: Sibson natural neighbours
                       # <rule>=nn_non_sibson: Non-Sibson natural
                       # neighbours.
```

The grid the bathymetry is interpolated onto may either be a regular rectangular grid using the bounding box specified for `coastmesh` (MINLON, MINLAT, MAXLON, MAXLAT) or a triangulation using the closed coastline loop specified in `coastmesh`. The former grid is specified using:

```
HFUN_GRID    yes
```

The gridded bathymetry may be smoothed `n` times using:

```
HFUN_SMOOTH  n
```

A minimum bathymetry (HFUN\_BMIN) is then mapped to a minimum mesh size (HFUN\_HMIN) and maximum bathymetry (HFUN\_BMAX) to maximum mesh size (HFUN\_HMAX), e.g:

```
HFUN_HMIN    500.0
HFUN_HMAX    5000.0
HFUN_BMIN    -2.0
HFUN_BMAX    -200.0
```

Note that the convention used for bathymetry is that if bathymetries are less than zero, then maximum bathymetries (HFUN\_BMAX) are the deepest values and minimum bathymetries (HFUN\_BMIN) the shallowest values, such that  $HFUN\_BMAX < HFUN\_BMIN$ .

All bathymetries between the minimum and maximum are mapped using some function defined by HFUN\_TYPE, where:

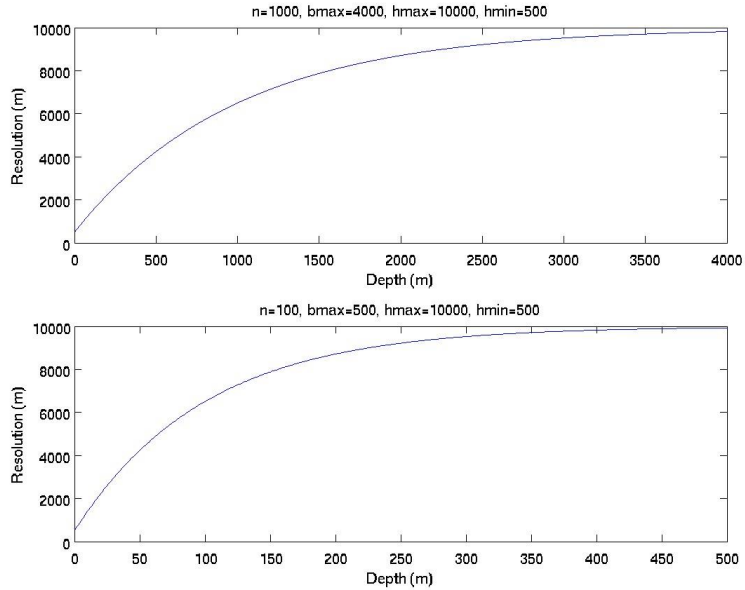
```
HFUN_TYPE    n    # n = 0: Linear mapping
                # n > 0: Exponential mapping
                # n < 0: Cosine mapping
```

The exponential mapping is computed via:

$$\text{Weight} = \frac{(HFUN\_HMIN - HFUN\_HMAX) \cdot \exp(\text{bathy} / n) + [HFUN\_HMAX - HFUN\_HMIN] \cdot \exp(-|HFUN\_BMAX| / n)}{2}$$

Examples of the exponential mapping are shown below:

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A cosine mapping is computed via:

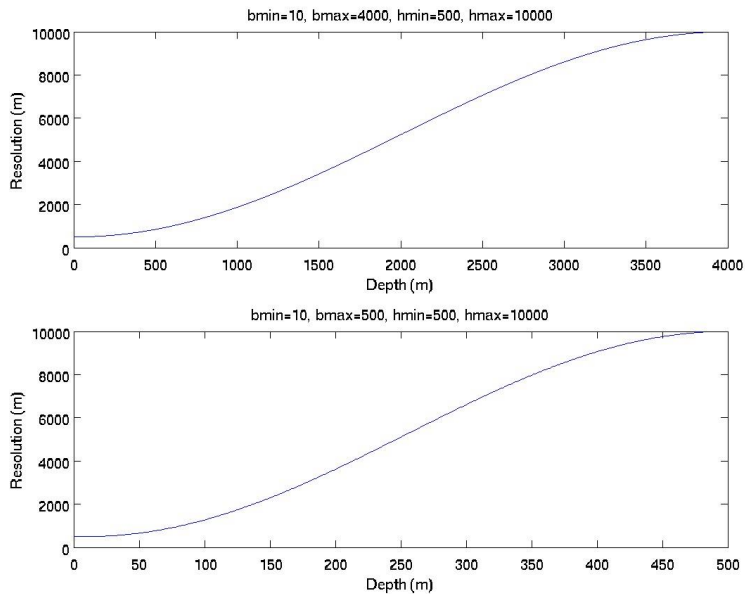
$$\text{Weight} = 0.5 [D * \cos(|\text{bathy}| \pi / DD - |\text{HFUN\_BMIN}| \pi / DD) + P]$$

$$D = \text{HFUN\_HMIN} - \text{HFUN\_HMAX}$$

$$P = \text{HFUN\_HMIN} + \text{HFUN\_HMAX}$$

$$DD = |\text{HFUN\_BMAX}| - |\text{HFUN\_BMIN}|$$

Examples of the cosine mapping are shown below:



The mapping function may be assembled with multiple functions using:

```
NHFUN    <n>          # Number of mappings
HMIN0    20           # Minimum resolution 0
HMAX0    200         # Maximum resolution 0
BMIN0    -2          # Minimum depth 0
BMAX0    -50         # Maximum depth 0
TYPE0    0           # Mapping type 0
```

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```
HMIN1      200      # Minimum resolution 1
HMAX1      1000     # Maximum resolution 1
BMIN1      -50      # Minimum depth 1
BMAX1      -200     # Maximum depth 1
TYPE1      100      # Mapping type 1
.
.
HMINn      1000     # Minimum resolution <n>
HMAXn      10000    # Maximum resolution <n>
BMINn      -200     # Minimum depth <n>
BMAXn      -5000    # Maximum depth <n>
TYPEn      -10      # Mapping type <n>
```

The bathymetry values used in the weighting function may be over-riden from that read from file for a given radius around a longitude / latitude coordinate. This is useful for maintaining coarse resolution on open boundaries near the coast where bathymetry may be shallow, which assists in maintaining adequate boundary nesting ratios if downscaling. Bathymetry over-ride is invoked using:

```
HFUN_OVERRIDE      n      # Number of over-ride locations
lon1 lat1 radius1 value1      # 1st over-ride specification
lon2 lat2 radius2 value2      # 2nd over-ride specification
.
.
.
lonn latn radiusn valuen      # nth over-ride specification
```

If `value <= 0` then it is assumed a bathymetry value (m) is supplied that is subjected to the mapping function to obtain a weighting value. If `value > 0` it is assumed a weighting value (m) is directly supplied. Bathymetries/weightings within a distance `radius` (m) of (`lon,lat`) are linearly interpolated from `value` to the bathymetry/weighting value at the limit of the radius.

The bathymetry may be processed to allow specification of the resolution as a function of the gravity wave speed ( $\sqrt{g * bathy}$ ). Note that the `BMIN` and `BMAX` limits must then be in terms of this speed. This is invoked using:

```
HFUN_BATHY_FILE    GWS <bathy.nc>
```

Resolution may also be specified using the bathymetry gradient with:

```
HFUN_BATHY_FILE    GRAD <bathy.nc>
```

Again, the `BMIN` and `BMAX` limits must then be gradient values, and in this case the `HFUN_GRID` must be turned on.

An alternative weighting function may be generated using the distance from the coast, where the minimum distance from the coast (or `HFUN_BMIN` if present) is mapped to maximum resolution and the maximum distance from the coast (or `HFUN_BMAX` if present) is mapped to minimum resolution. Note that this approach does not require a bathymetry file to be interpolated onto a grid for the weighting function to be computed; only a coastline in `COASTFILE` need be supplied. This option is invoked using:

```
HFUN_BATHY_FILE    COAST
```

A weighting function based on distance to a discrete number of user specified locations may be used (as opposed to distance from the coast). The mapping from distance to the points to resolution is the same as used for `COAST` (e.g. using `HFUN_HMIN` or `NHFUN` above). This is achieved via:

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```
HFUN_BATHY_FILE    POINT
HFUN_POINTS        n
lon1 lat1        # seed point 1
lon2 lat2        # seed point 2
.
.
lonn latn resn
```

A weighting function can be based on the distance from a closed polygon, with resolution within the polygon being HMIN.

```
HFUN_BATHY_FILE    POLY      # Polygon distance definition
HFUN_POLY          poly.xy   # Ascii file containing the polygon
```

The resolution inside individual polygons may be explicitly specified using:

```
HFUN_POLY    poly.xy:r1 poly2.xy:r2 ... polyn.xy:rn
```

Alternatively, the polygons may be specified using:

```
NHFUN_POLY      n
HFUN_POLY0      poly1.xy:r1
HFUN_POLY1      poly2.xy:r2
.
.
HFUN_POLYn      polyn.xy:rn
```

For example, if a domain has three polygons and `poly1.xy` were to have 100 m resolution, `poly2.xy` is not explicitly specified (distance set to HMIN) and `poly3.xy` have a resolution of 300 m, then use;

```
HFUN_POLY    poly.xy:100 poly2.xy poly3.xy:300
```

A combination of COAST, POLY or POINT may be used, where the distance used to map to the resolution is the minimum distance from the coast, a polygon or a point.

Finally an explicitly specified weighting function may be specified via:

```
HFUN_BATHY_FILE    1000.0 # Constant resolution of 1000 m

HFUN_BATHY_FILE    n
lon1 lat1 res1    # resolution (in m) at (lon1,lat1)
lon2 lat2 res2    # resolution (in m) at (lon2,lat2)
.
.
lonn latn resn
```

Note that HFUN\_HMIN and HFUN\_HMAX must still be specified for these explicit options to operate.

Output may be written in a format compatible with import into JIGSAW; the file output is written to is specified as:

```
JIG_GEOM_FILE      outfile.msh
```

A file of the coastline used may also be plotted using:

```
PLOTFILE           <plotname>
```



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In this case a file is created with a summary of all `coastmesh` options used, and the lon,lat coordinates of the original coastline in `plotname_in.txt`. A file containing the processed coastline is written to `plotname_out.txt`.

The `HFUN_OVERRIDE` option also functions with distance weighting functions, where values  $\leq 0$  assume a distance value (m) is supplied that is subjected to the mapping function to obtain a weighting, and values  $> 0$  it is assume a weighting value (m) is directly supplied.

The distance to the coast or a point is not computed along open boundaries or links (i.e. these regions receive minimum resolution). The coast-distance or point-distance weighting function may be excluded from use around a given longitude / latitude coordinate for a given radius. This is also useful for maintaining coarse resolution on open boundaries near the coast where bathymetry may be shallow, which assists in maintaining adequate boundary nesting ratios if downscaling. To achieve this, nominate a longitude / latitude near the location where the open boundary intersects the coast, and provide a radius sufficient to exclude increasingly higher resolution from being achieved as the coast is approached. Weighting function exclusion is invoked using:

```
HFUN_EXCLUDE          n      # Number of over-ride locations
lon1 lat1 radius1     # 1st exclusion specification
lon2 lat2 radius2     # 2nd exclusion specification
.
.
.
lonn latn radiusn     # nth exclusion specification
```

## 15 Getting Started

The steps required to compile SHOC/COMPAS, run on a simple test case and generate a custom application are detailed below. Note that visualisation and grid generation requires the matlab based software package PLUM.

### 15.1 Compile SHOC/COMPAS

Install the source code depicted by the directory structure Figure 2.1. Configure the code making sure any netCDF library paths are correctly specified (Section 2.2);

```
./conf/configure
```

Make the executable;

```
make
```

The SHOC executable now resides in `ems/src/model/hd`

The COMPAS executable now resides in `ems/src/model/hd-us`

The version number is retrieved using:

```
shoc -v
```

### 15.2 Run a test case

Test cases for SHOC are located in;

```
ems/src/model/tests/hd
```

A useful first test case is test 7, where a wind with positive curl is blown over a closed basin with sloping bathymetry (Section 12.7). To run this test:

Make an input file (Section 2.3 and 8):

```
shoc -g test7.prm in7.nc
```

Make sure no output files exist:

```
rm out7_z.nc
```

Run the model:

```
shoc -p test7.prm
```

View the output.

### 15.3 Generate a custom grid (SHOC only)

The generation of custom grids requires the matlab based package PLUM ([john.andrewartha@csiro.au](mailto:john.andrewartha@csiro.au) for details) with the executables `gridgen` and `gridbathy` installed. The executable `gridbathy` is located in `ems/utilities/grid/`, however `gridgen` is currently not a member of `ems`. Refer to the README documentation supplied with PLUM for installation. Note that dedicated bathymetry and coastline databases may be required for custom grid generation of certain areas. Default databases are supplied with PLUM.

1. Invoke matlab and PLUM, for unix/linux;  

```
matlab -nodesktop -nosplash -nojvm  
>> plum
```

2. Generate a grid, in this case a geographic rectangular grid. This is a spherical grid where the spheroid is rotated so that the equator passes through the centre of the grid (Section 4.6.4). On the main PLUM menu, click on 'GRID GENERATION' and the following is displayed;

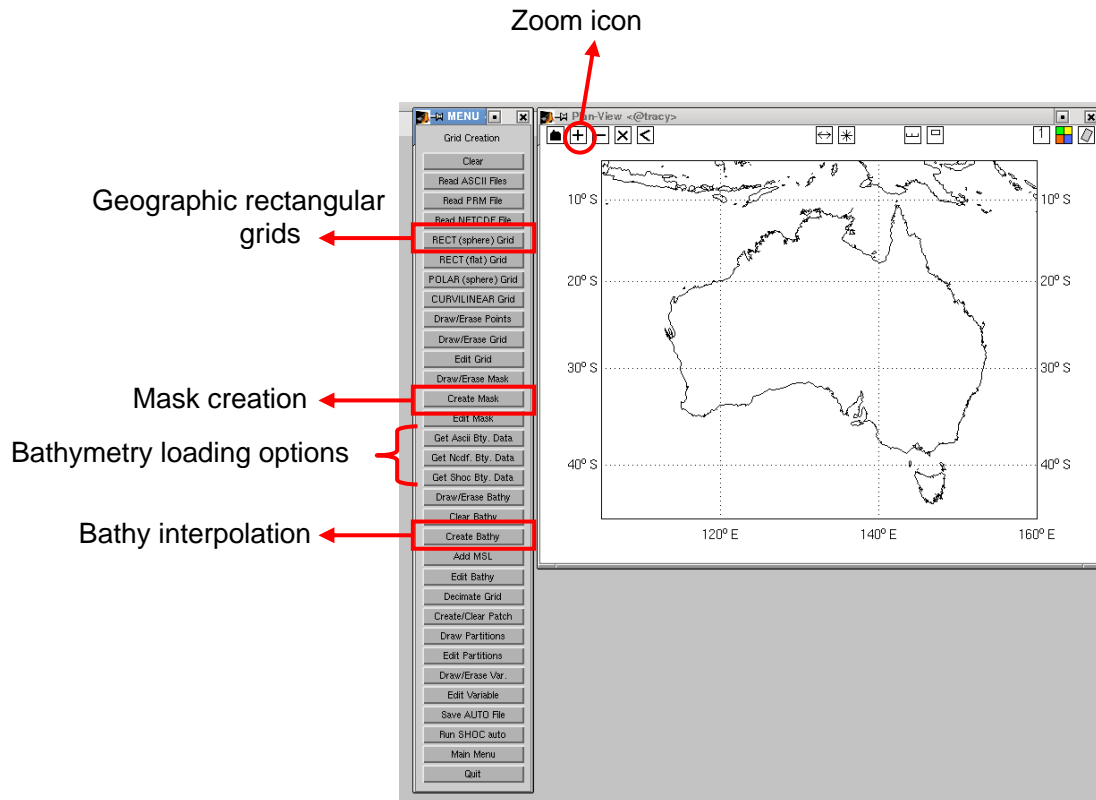


Figure 14.3.1. PLUM grid generation menu.

Zoom in on the location the grid is to be constructed for using the '+' icon at the top-left of the Plan-View screen. Click on 'RECT (sphere) Grid' to generate a spherical geographic rectangular grid. Other options are a non-geographic grid, polar grid or orthogonal curvilinear grid. Follow the instructions in the matlab window (i.e. click on the grid centre, left and right bottom corners). A grid is then created, e.g. Figure 14.3.2. The grid can be rotated, relocated or scaled by clicking and dragging the blue dots. The number of cells in the x-direction is specified by entering 'x' followed by the number of cells in the matlab window, and similarly for cells in the y-direction. Right-click the mouse to exit and define the grid, or click 'RECT (sphere) Grid' again for further definition of the grid. An example of the final grid is shown in Figure 14.3.3, in this case focussed on the South Australian Gulfs. Note the '+', 'x' and '-' icons in the Plan-View pane can be used to zoom in, centre and zoom out around the image while creating the grid (right click to exit from 'x').

3. Create a land mask. Click on the 'Create Mask' button (see Figure 14.3.1). The land in the domain is coloured green. Land, water or outside cells (Section 4.8) can be manually reset using the 'Edit Mask' button. The resulting masked image is shown in Figure 14.3.4. The number of 2D wet cells is displayed in the matlab window.

4. Load the bathymetry from a database. Bathymetry can be loaded from pre-existing ascii or netCDF databases, or can be loaded from a SHOC output file. In this case bathymetry is loaded from the AGSO 2002 database by clicking 'Get Ncdf. Bty. Data' and choosing the appropriate database. Bathymetry is loaded onto the image as depicted in Figure 14.3.5 (a). Return to the 'GRID CREATION' menu and click on 'Get Ncdf. Bty. Data' again. A decimation value for the bathymetry dataset may be then entered (enter 0 for default), and the bathymetry is truncated to the grid domain size (Figure 14.3.5 (b)).

5. Interpolate the bathymetry onto the grid. Click on 'Create Bathy' (Figure 14.3.1); a list of interpolation methods is listed in the matlab window. Enter the interpolation method required. In this case a '(7) for weighted area' is used. It is possible that the interpolation scheme will not fill all the cells in the domain. In this case click on 'Create Bathy' again and use '(6) for inverse distance (fill-in)'. This may be required to be performed several times. The

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resulting interpolated bathymetry is displayed in Figure 14.3.6. Sometimes the interpolation scheme may fail, and no cells are interpolated. In this case try another interpolation method. Bathymetry cells may be manually edited by using the 'Edit Bathy' button.

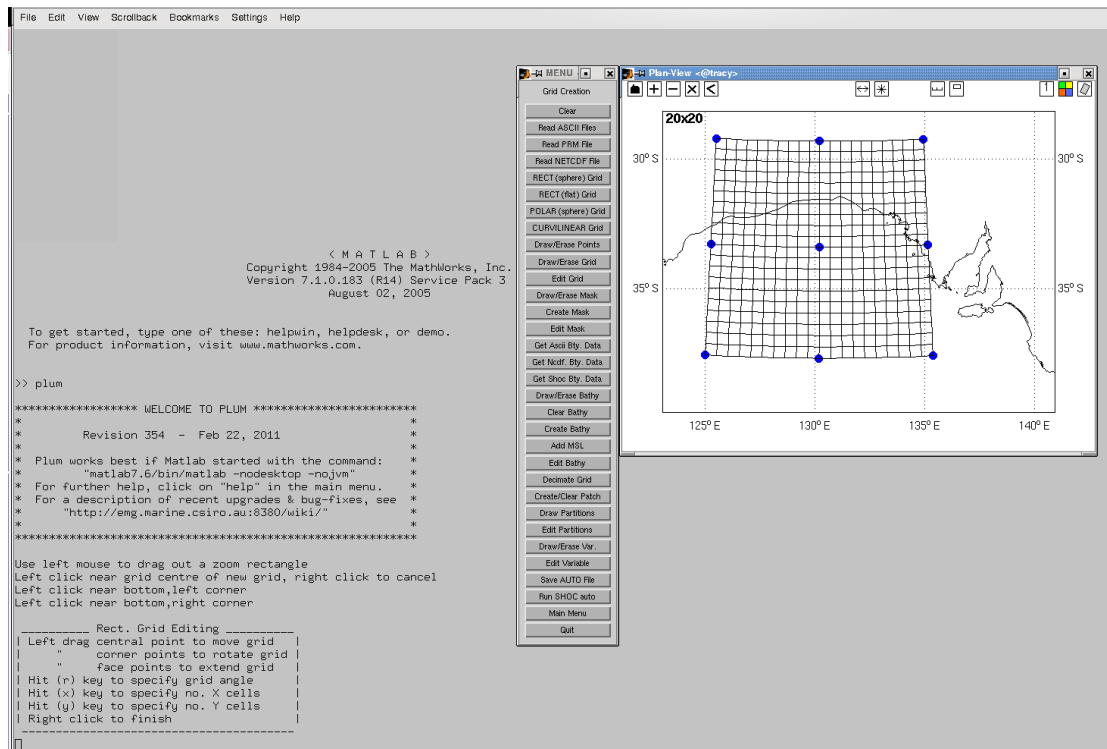


Figure 14.3.2. Geographic rectangular grid of the Great Australian Bight.

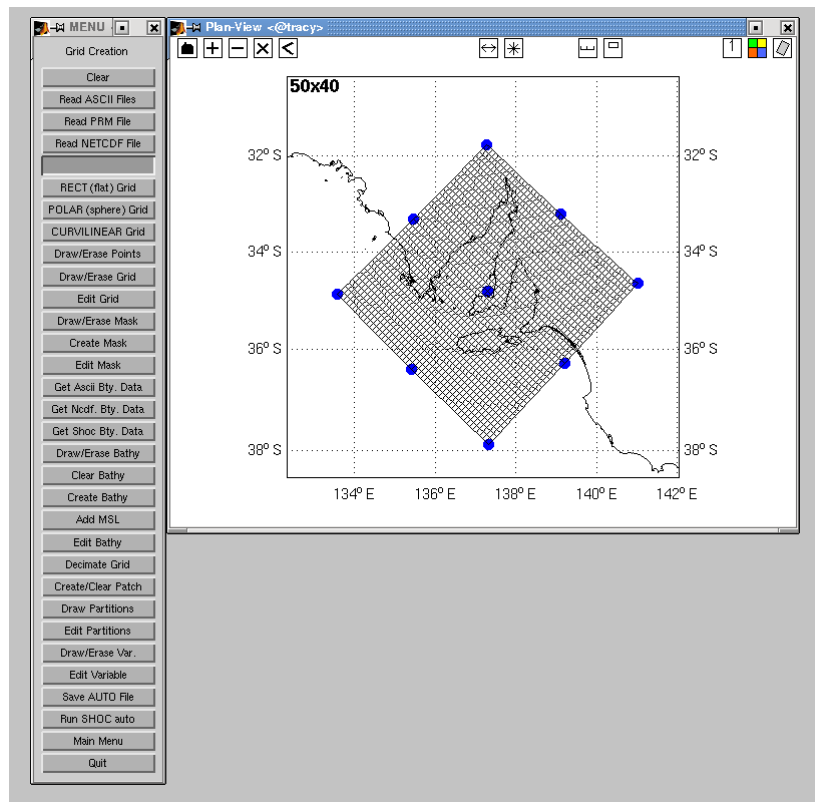


Figure 14.3.3. Geographic rectangular grid of the South Australian Gulfs.

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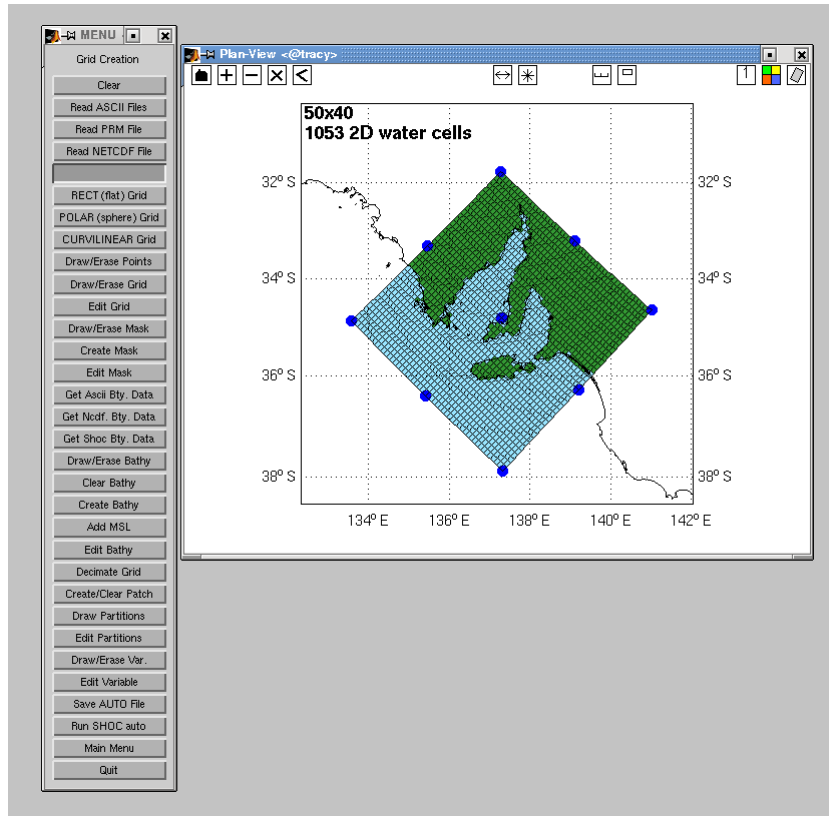
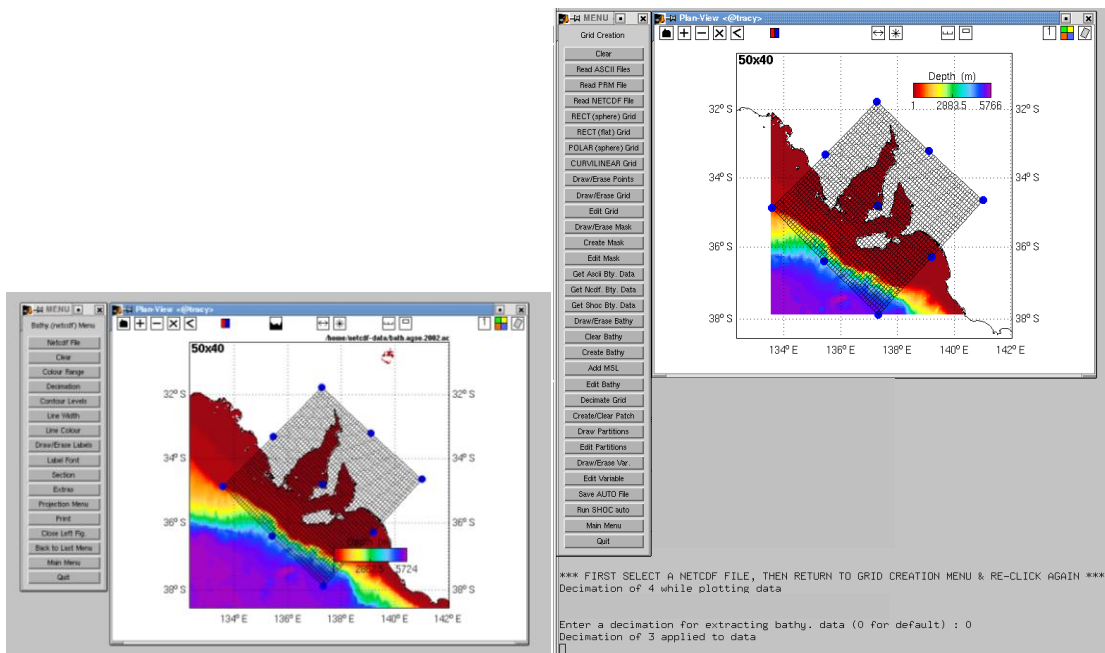


Figure 14.3.4. Masked image of the South Australian Gulfs.



(a) Database loaded

(b) Decimated and truncated to grid

Figure 14.3.5. Bathymetry loaded onto the South Australian Gulfs.

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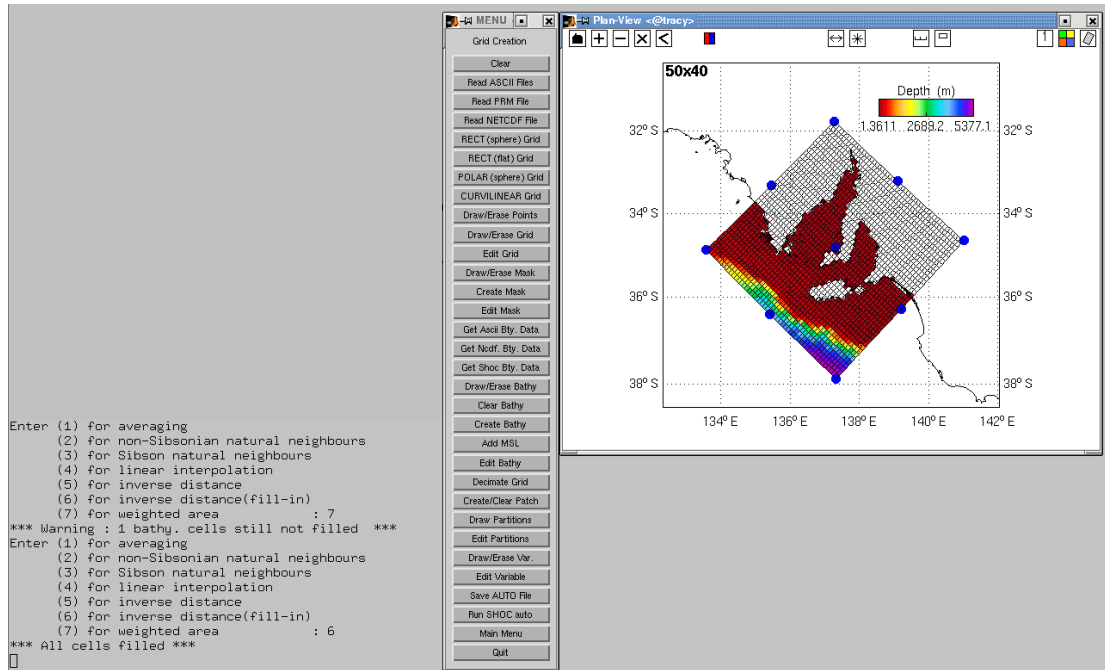
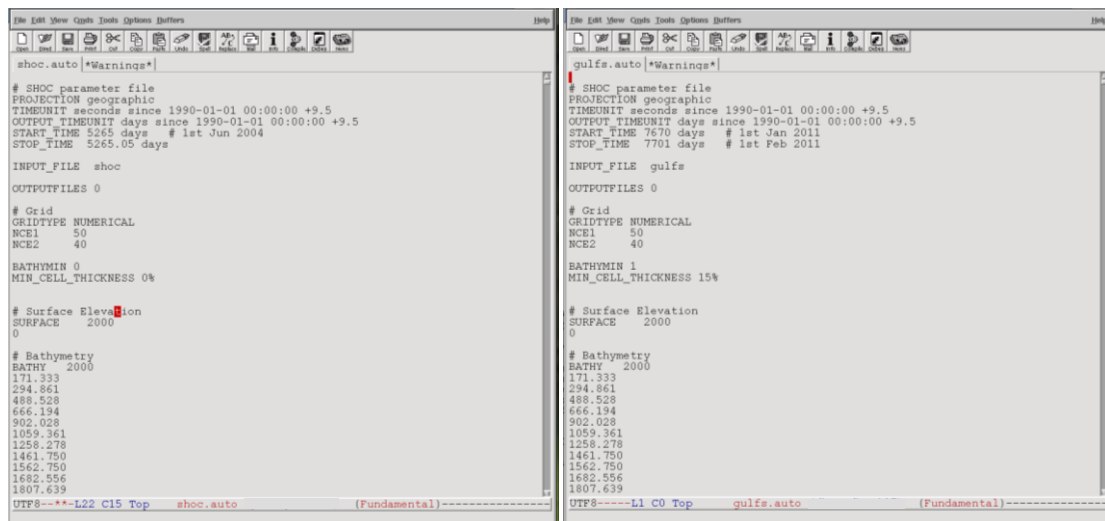


Figure 14.3.6. Bathymetry interpolated onto the South Australian Gulfs.

6. Create a SHOC auto file. Click on 'Save AUTO file' to create an auto file (Section 5) suitable for generating a full parameter file and netCDF input file. The auto file will be saved to `shoc.auto`. This file should be edited before invoking the `-a` option to modify the `START_TIME` and `STOP_TIME` to the start and end times desired, `INPUT_FILE` should be changed to a unique name and `BATHYMIN` and `MIN_CELL_THICKNESS` should be set to desired values. The original `shoc.auto` is shown in Figure 14.3.7 (a), and the modified file in 14.3.7 (b), now renamed to `gulfs.auto`. Additionally, any optional parameterisations outlined in Section 5 may be added at this stage, e.g. if the model forcing, initial conditions or boundary data are known, they may be included and will be propagated into the parameter file generated by the `-a` option. Alternatively, this generated parameter file may be edited to include forcing and initial conditions. The parameter file (`gulfs.prm`) and input file (`gulfs.nc`) may then be generated using:

```
shoc -ag gulfs.auto
```



(a) Original file from PLUM

(b) Modified file

Figure 14.3.6. Parameter files for the South Australian Gulfs.

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7. Edit the parameter file `gulfs.prm`. This generally includes initial condition data for temperature, salinity and surface elevation, surface fluxes (wind, pressure, heatflux and saltflux) and specification of open boundary conditions. For example, if BLUElink data were available where the file `jan2011_ets.nc` contained the variables `temp`, `salt` and `eta`, the file `jan2011_uv.nc` contained 3D velocities `u` and `v` and ACCESS-A data `jan2011_met.nc` were available containing variables `pressure`, `u` and `v`, then `gulfs.prm` may be modified thus:

In the tracer list add (see Section 4.9);

```
TRACER0.data          jan2011_ets.nc
and
TRACER1.data          jan2011_ets.nc
```

Surface initial condition (see Section 4.12);

```
SURFACE              jan2011_ets.nc
```

Wind and pressure forcing (see Section 4.13 & 4.14);

```
WIND_TS              jan2011_met.nc
WIND_INPUT_DT        10 minutes
WIND_SPEED_SCALE     1.0
DRAG_LAW_V0          10.0
DRAG_LAW_V1          26.0
DRAG_LAW_CD0         0.00114
DRAG_LAW_CD1         0.00218
```

```
PRESSURE             jan2011_met.nc
PRESSURE_INPUT_DT    10 minutes
```

Open boundary forcing (see Section 4.10.7 & 4.10.17);

```
NBOUNDARIES          3

BOUNDARY0.NAME        West
BOUNDARY0.TYPE        u1
BOUNDARY0.BCOND_NOR   CUSTOM
BOUNDARY0.CUSTOM.u1   uv_to_u1  jan2011_uv.nc
BOUNDARY0.BCOND_TAN   CUSTOM
BOUNDARY0.CUSTOM.u2   uv_to_u2  jan2011_uv.nc
BOUNDARY0.BCOND_ELE   NOTHIN|FILEIN
BOUNDARY0.BCOND_salt  UPSTRM
BOUNDARY0.BCOND_temp  UPSTRM
BOUNDARY0.ADJUST_FLUX 200 seconds      # ~ 0.2 x DT
BOUNDARY0.DATA        jan2011_ets.nc
BOUNDARY0.RANGE        (0,0) - (0,14)

BOUNDARY1.NAME        East
BOUNDARY1.TYPE        u1
BOUNDARY1.BCOND_NOR   CUSTOM
BOUNDARY1.CUSTOM.u1   uv_to_u1  jan2011_uv.nc
BOUNDARY1.BCOND_TAN   CUSTOM
BOUNDARY1.CUSTOM.u2   uv_to_u2  jan2011_uv.nc
BOUNDARY1.BCOND_ELE   NOTHIN|FILEIN
BOUNDARY1.BCOND_salt  UPSTRM
BOUNDARY1.BCOND_temp  UPSTRM
BOUNDARY1.ADJUST_FLUX 200 second
BOUNDARY1.DATA        jan2011_ets.nc
BOUNDARY1.RANGE        (50,0) - (50,23)
```

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```
BOUNDARY2.NAME           Offshore
BOUNDARY2.TYPE           u2
BOUNDARY2.BCOND_NOR      CUSTOM
BOUNDARY2.CUSTOM.u1      uv_to_u1   jan2011_uv.nc
BOUNDARY2.BCOND_TAN      CUSTOM
BOUNDARY2.CUSTOM.u2      uv_to_u2   jan2011_uv.nc
BOUNDARY2.BCOND_ELE      NOTHIN|FILEIN
BOUNDARY2.BCOND_salt     UPSTRM
BOUNDARY2.BCOND_temp     UPSTRM
BOUNDARY2.ADJUST_FLUX    200 seconds
BOUNDARY2.DATA           jan2011_ets.nc
BOUNDARY2.RANGE          (0,0) - (49,0)
```

If a tide is required to be included using the CSR tide model, then set `TIDE_CSR_CON_DIR` to the nodal correction directory, and `TIDE_CSR_ORTHOWEIGHTS` to the orthoweight database (see Section 4.10.20) and use the elevation boundary condition:

```
BOUNDARY0.BCOND_ELE      NOTHIN|FILEIN|TIDALH
```

Numerous other parameters may be edited in the file `gulfs.prm` to suit the application (e.g. `PARAMETERHEADER`, `DESCRIPTION`, `NAME`, netCDF output files (Section 4.31.6), time series output (Section 4.31.5), `WINDOWS` (Section 4.2), horizontal friction (Section 4.22), turbulence closure (Section 4.21), `HEATFLUX` (Section 4.17) or diagnostics (Section 4.30). The example here is the minimum required to set up a simulation, and many alternative parameterisations or options may be invoked as described in this manual. Note that the parameterisation demonstrated here does not guarantee model stability, and parameters or schemes may require alteration to achieve a stable model run. Describing the process of stability analysis is beyond the scope of this manual. Once a satisfactory parameter file is created, the input file must be re-created so that the specified initial conditions are included:

```
rm gulfs.nc
shoc -g gulfs.prm gulfs.nc
```

It is good practice to view `gulfs.nc` graphically to ensure initial conditions and bathymetry are satisfactory. The resolution of this example is  $\sim 9.5 \times 12.2$  km with maximum depth of  $\sim 5400$  m resolved by 52 layers.

### 8. Run the simulation;

```
shoc -p gulfs.prm
```

Any warnings encountered during setup are written to the file `runlog`, model progress is written to `diag.txt` and the model parameterisation as used internally by the model is listed in `setup.txt` (see Section 4.32). It is good practice to view the `setup.txt` file to ensure the model configuration is as expected. Output may be viewed using PLUM, or a similar java based application DIVE (see <http://www.emg.cmar.csiro.au/www/en/emg/software/Visualization.html>).

The process of stability analysis, sensitivity analysis and calibration may now commence.



## 16 Sediment Transport

The sediment transport routines may be fully coupled to SHOC/COMPAS by invoking:

```
DO_SEDIMENTS      YES
```

or

```
DO_SEDIMENTS      DO
```

Additionally, a sediment layer structure must be defined for sediments transport to operate, e.g;

```
NSEDLAYERS  4      # The number of sediment layers
0.005        # Depth in the sediment of the 1st layer face
0.020        # Depth in the sediment of the 2nd layer face
0.080        # Depth in the sediment of the 3rd layer face
0.320        # Depth in the sediment of the 4th layer face
```

The tracer list must also include a number of sediment fractions, with corresponding attributes (e.g. particle size, settling velocity etc.) defined. There are also a number of global parameters that must be defined; see the Sediment Transport User Guide for a full explanation. The sediment transport parameters and tracer attributes can be automated, where a set of user defined defaults are used in preference to a fully defined specification in the parameter file. This involves defining the tracer sediment classes that are to be used, the attributes that will be defined for those tracers, and the global parameters used for the sediment transport. The sediment tracer classes are defined using:

```
SED_VARS      <class1> <class2> ... <class_n>
```

Where `<class_n>` is the name of the sediment class the user wishes to be include. These classes are hardwired into the sediment interface module (`sediments/sediments.c`) and can be expanded as desired. Currently, the classes consist of;

```
Gravel
Sand
Mud
FineSed
Dust
```

SHOC will check if the classes defined in `SED_VARS` are included in the list of hardwired names, and if so then will automatically include that tracer in the tracer list. Additionally, a 3D diagnostic tracer named `tss` is automatically generated, and 2D tracers named `ustrcw_skin` and `depth_sed`. Again, these additional tracers are hardwired into `sediments/sediments.c` and can be expanded as desired. The sediment tracer attributes associated with these tracer classes are defined using:

```
SED_VARS_ATTS  <specification_name>
```

Where `<specification_name>` is the name of a default set of attributes the tracers will be assigned to. These default attributes are hardwired to the tracers in `sediments/sediments.c` and can be expanded as desired. Currently the default sets available are:

```
standard      # standard set of attributes
estuary       # Attributes applicable to an estuarine environment
```

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If any of the tracer classes are explicitly defined in the tracer list, then any attributes associated with that tracer takes precedence over the defaults defined by `SED_VARS_ATTS`. Furthermore, and tracer attribute can be defined in the parameter file using:

```
TRACER<m>.attname  
or  
<name>.attname
```

Where `<m>` is the tracer number in the list, `attname` is the tracer attribute name (see the MecoSed Users Guide for a list of attribute names) and `<name>` is the name of the tracer, e.g.

```
Mud.svel      -0.0001      # Redefine the settling velocity for Mud
```

Various sediment parameters may be spatially varying (e.g. settling velocity). If the settling velocity attribute is the name of a 2D tracer in the tracer list, then the values of that tracer will be used as the settling velocity. In automated mode, if a 2D tracer is found in the tracer list with the name of a sediment tracer class appended with `_svel` (e.g. `Mud_svel`, `Sand_svel`), then that 2D tracer's values will be used as the settling velocity for that sediment tracer class, e.g. `Mud` may be spatially variable if a 2D tracer exists with the name `Mud_svel`, or, for example, if a 2D tracer exists with the name `settling_mud` and the settling velocity attribute for `Mud` is redefined as;

```
Mud.svel      settling_mud
```

The global sediment transport attributes are defined in automated mode using;

```
SEDFILE      <param_filename>
```

Where `<param_filename>` may be:

1. The name of a file containing the global parameters,
2. A default name for hardwired parameters. Currently the names `standard` and `estuary` are accepted. The initialisation of these parameters exists in `model/lib/sediments/sed_init.c` and may be expanded as desired,
3. `auto`, where the parameters may be dynamically prescribed in the routine `sed_params_auto()` in `model/lib/sediments/sed_init.c`. Currently this routine is empty.
4. If none of the above are specified, the parameters are assumed to be listed in the main parameter file.

The sediment specification is written in full in the diagnostic file `setup.txt` (see Section 4.31). If a transport parameter file is generated from a full parameter file using `TRANS_DATA` (see Section 9) then the sediment specification is also written to this file. Outputting these sediment specifications may be invoked without running the full sediment transport by using;

```
DO_SEDIMENTS      WRITE
```

## 17 Ecology

The ecology routines may be fully coupled to SHOC/COMPAS by invoking:

```
DO_ECOLOGY YES
```

or

```
DO_ECOLOGY DO
```

Additionally, a sediment layer structure must be defined for ecology to operate, (see Section 15).

Ecology also requires a process definition and a parameter specification. These are defined via:

```
processfname <processes> # name of ecology processes
```

The name `<process>` may be one of the following:

```
<filename>
standard
estuary
auto
```

If `<filename>` is specified, then the BGC processes are defined in a file bearing that name. If `defaults` is specified, then the processes are hardwired into the module `process_defaults.c` in the ecology library. Additional process lists may be included in this module, with associated modifications to the calling routines `get_eco_processes()` in `process_defaults.c` and `read_process_group_from_defaults()` in `ecology.c`. Additionally, there is scope to define processes dynamically using the (currently empty) routine `eco_process_auto()` in `process_defaults.c`. This dynamical specification is invoked if `auto` is specified for `<processes>`.

The ecological parameters are specified using:

```
biofname <parameters> # name of ecology parameters
```

The name `<parameters>` may be one of the following:

```
<filename>
standard
estuary
auto
```

If `<filename>` is specified, then the BGC parameters are defined in a file bearing that name. If `default` is specified, then the processes are hardwired into the module `parameter_defaults.c` in the ecology library. Additional parameter lists may be included in this module, with associated modifications to the calling routine `get_eco_params()` in `parameter_info.c`. Additionally, there is scope to define processes dynamically using the (currently empty) routine `eco_params_auto()` in `parameter_info.c`. This dynamical specification is invoked if `auto` is specified for `<parameters>`.

Note that the default parameters include hardwiring of the phytoplankton growth rates that have traditionally been specified as netcdf files. It is no longer necessary to supply this netcdf file, just specifying the name '10pp1kINP' or '10benINP' is sufficient.

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If a tracer list of the tracers required for the ecology processes is not explicitly specified, then these tracers will be automatically generated based on the defined processes. The attributes for these tracers are defined using:

```
ECO_VARS_ATTS      <attributes>      # name of tracer attribute set
```

The name <attributes> may be one of the following:

```
    standard
    estuary
```

If `standard` is specified, then the attributes for all possible ecology tracers are hardwired into the routine `eco_defaults_standard()` in `/hd/ecology/ecology.c` and can be expanded as desired by creating additional attribute routines and adding them to the calling function `eco_set_tracer_defaults()` in the same module. Note that a list of all possible ecology tracer names and long names (water column/sediment and benthic) must be maintained in the structures `ECONAME3D` and `ECONAME2D` in `ecology.c` in order for tracer automation to operate correctly.

If any of the tracer classes are explicitly defined in the tracer list, then any attributes associated with that tracer takes precedence over the defaults defined by `ECO_VARS_ATTS`. Furthermore, any tracer attribute can be defined in the parameter file using:

```
TRACER<m>.attname
or
<name>.attname
```

Where <m> is the tracer number in the list, `attname` is the tracer attribute name and <name> is the name of the tracer, e.g.

```
PhyL_N.svel -4e-6 # Redefine the settling velocity for large
                  # phytoplankton nitrogen.
```

The ecology specification is written in full in the diagnostic file `setup.txt` (see Section 4.31). If a transport parameter file is generated from a full parameter file using `TRANS_DATA` (see Section 9) then the ecology specification is also written to this file. Outputting these ecology specifications may be invoked without running the full sediment transport by using;

```
DO_ECOLOGY WRITE
```

Ecology requires a `LIGHT` variables, which historically was a daily mean but with newer versions of the ecology processes can be a copy of short wave radiation (i.e. diurnally variable). This can be input via file:

```
LIGHT           light.nc
LIGHT_INPUT_DT  1 hour
ALBEDO_LIGHT    0.0
```

`LIGHT` can point to a tracer which reads `LIGHT` via the reset function, e.g.

```
LIGHT           inlight
LIGHT_INPUT_DT  1 hour
ALBEDO_LIGHT    0.0
```

with

```
TRACER?.name    inlight
TRACER?.name    Light input from swr
```

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TRACER?.units	W m-2
TRACER?.type	WC2D
TRACER?.fill_value	0.0
TRACER?.valid_range	0.0 2000.0
TRACER?.reset_file	swr.nc
TRACER?.reset_dt	1 hour

If `swr` is included in the transport files, then `LIGHT` can be read from this variable along with all other transport variables using;

```
LIGHT          file
```

## 18 Troubleshooting

### **Bathymetry altered on successive input file generations :**

The bathymetry written to the input file using the `-g` option is modified from that read in from the parameter file by the `BATHYMIN`, `BATHYMAX` and `MIN_CELL_THICKNESS` parameters. If the input file bathymetry is to be modified (using `jvismeco`) and used in a successive parameter file, make sure the abovementioned parameters are set to zero, a very large value and zero respectively. Note also that the `SMOOTHING` option will also have this effect.

### **Heat flux increasing with time :**

Using the `HEATFLUX = NET_HEAT` with a `HEATFLUX_FILE_INPUT_DT > DT` (3D time-step) in conjunction with a `RADIATION` file (`SWR_ATTENUATION > 0`, `SWR_TRANSMISSION > 0`) will result in the heatflux increased by the surface short wave contribution during the period `HEATFLUX_FILE_INPUT_DT`. Set `HEATFLUX_FILE_INPUT_DT = DT` to overcome this effect.

### **Model crashes :**

There are many instances that may cause this.

Check that `momsc = ORDER2`. SHOC is a second order model in time and space and 1<sup>st</sup> order momentum schemes have proved consistently unsuccessful.

### **Negative variable values inexplicably appear in output :**

Set `bytespervalue` in the output file to 4. Using short representation of output may make very large or small values wrap bits and become negative. Use double representation to avoid this.

### **Open boundaries appear as OUTSIDE cells :**

Each `u1` or `u2` open boundary should be associated with a `FRONT`, `BACK`, `LEFT` or `RIGHT` edge. If an open boundary cell location list contains both `FRONT` and `BACK`, or `LEFT` and `RIGHT` edge cells then they will be masked as `OUTSIDE`.

### **Output file does not record further dumps :**

Check that the 2.0 Gb limit for output files has not been exceeded. Use `netCDF v4`.

### **Reading parameter file difficulties :**

Check that no white space, tabs or `^M` exists after entries in the parameter file.

### **River open boundaries aren't advecting tracers :**

Make sure there are at least 3 wet cells in the normal direction to the open boundary, or change the boundary condition for tracers from `UPSTRM` to `FILEIN`. The `UPSTRM` condition uses a velocity one cell into the interior of the domain to reflect dynamics occurring in the interior rather than the prescribed boundary dynamics when solving the 1 dimensional advection equation that constitutes the `UPSTRM` condition. If this interior cell falls on a solid boundary (i.e. only 2 wet cells exist normal to the boundary) then the velocity will be zero and tracer concentration will not change due to the `UPSTRM` condition.

### **Segmentation fault using -g option :**

There are potentially many parameter combinations that may cause this.

**(a)** Open boundaries in the inside of the domain (i.e. open boundaries not on the edges of the grid) must be adjacent to 'outside' cells. Check that interior open boundaries are adjacent to outside cells using `jvismeco`.

**(b)** Solid boundaries on the edge of the grid. SHOC requires a land cell to surround all wet cells, even along the edges of the grid. This is so that there exists a ghost cell location adjacent to each wet cell for setting lateral boundary conditions.

### **When to re-make an input file using the -g option :**

The input `netCDF` file must be re-generated if changes are made to the bathymetry list, the number of layers or layer spacings used, data used for tracer initialisation, `BATHYMIN`, `BATHYMAX`, `MIN_CELL_THICKNESS`, `SMOOTHING`.

19 References

- Arakawa, A. and Lamb, V.R. (1977)** Computational design of the basic dynamical process of the UCLA general circulation model. *Methods in Computational Physics*, 17. Academic Press, pp. 173-265.
- Blackadar, A.K. (1962)** The vertical distribution of wind and turbulent exchange in neutral atmosphere. *J. Geophys. Res.*, 67, 3095-3102.
- Blanc, T.V. (1985)** Variation of bulk-derived surface flux, stability and roughness results due to the use of different transfer coefficient schemes. *J. Phys. Oceanogr.*, 15, 650-669.
- Blumberg, A.F. and J. Herring (1987)** Circulation modelling using orthogonal curvilinear coordinates, in *Three-Dimensional Models of marine and Estuarine Dynamics*, Ed. J.C.J. Nihoul and B.M. Jamart, Elsevier.
- Blumberg, A.F. and G.L. Mellor (1986)** A description of a three-dimensional coastal ocean circulation model. In: N. Heaps (Ed), *Three-dimensional shelf models, Coastal and Estuarine Sciences*, 5, American Geophysical Union.
- Burchard, H., K., O. Peterson and T.P. Rippeth (1998)** Comparing the performance of the Mellor Yamada and the  $k-\epsilon$  turbulence models. *J. Geophys. Res.*, 103, 10,543 – 10,554.
- Bowden, K.F. and P. Hamilton (1975)** Some experiments with a numerical model of circulation and mixing in a tidal estuary, *Estuarine and Coastal Marine Science*, 3, 281-301.
- Bunker, A. F. (1976)** Computations of surface energy flux and annual air-sea interaction cycles of the North Atlantic ocean. *Mon. Wea. Rev.*, 104, 1122-1140.
- Burchard, H., K., Bolding and M.R. Villarreal (1999)** GOTM, a general ocean turbulence model. Theory implementation and test cases. Technical Report EUR 18745EN, European Commission, 103pp.
- Burchard, H., K., O. Peterson and T.P. Rippeth (1998)** Comparing the performance of the Mellor Yamada and the  $k-\epsilon$  turbulence models. *J. Geophys. Res.*, 103, 10,543 – 10,554.
- Bye, J.A.T. (1977)** The flow series of Thalasso – models. Selected topics in atmospheric and marine sciences, No 6, Flinders University of South Australia, 59pp.
- Bye, J.A.T. (1977a)** The flow series of Thalasso – models. The FLOWM model, supplement to the FLOWC model. Selected topics in atmospheric and marine sciences, No 6, Flinders University of South Australia.
- Camerlengo. A.L. and J.J. O'Brien (1980)** Open boundary condition in rotating fluids. *J. Compt. Physics*, 35, 12 – 35.
- Cartwright, D.E. and R.D. Ray (1990)** Oceanic tides from Geosat altimetry. *J. Geophys. Res.*, 95 C3, 3069-3090.
- Chapman, D.G. (1985)** Numerical treatment of cross-shelf open boundaries in a barotropic coastal ocean model, *J. Phys. Oceanogr.*, 15, 1060-1075.
- Craig, P.D., Banner, M.L. (1994)** Modelling wave-enhanced turbulence in the ocean surface-layer. *J. Geophys. Res.*, 24, 2546-2559.
- Csanady, G.T. (1982)** *Circulation in the coastal ocean*, D. Reidel Publishing company.
- Delhez, J.M., Deleersnijder, E. (2007)** Overshootings and spurious oscillations caused by biharmonic mixing. *Ocean Modelling*, 17, 183-198.
- Demirov, E., E. Eifler, M. Ouberdous, and N. Hibma (1998)** ISPRAMIX – a three-dimensional free surface model for coastal ocean simulations and satellite data assimilation on parallel computers. Technical report EUR 18129EN, European Commission, 76pp.
- Dyer, K.R. (1997)** *Estuaries, a physical introduction*. J. Wiley & Sons, Chichester.
- Ebert, E.E. (2008)** Fuzzy verification of high-resolution gridded forecasts: a review and proposed framework. *Meteorological Applications*, 15, 51-64.
- Eifler, W. and W. Schrimpf (1992)** ISPRAMIX, a hydrodynamic program for computing regional sea circulation patterns and transfer processes. CEC Report EUR 14856 EN.
- Eringen, A.C. (1962)** *Nonlinear theory of continuous media*. McGraw Hill, New York.
- Evenden, G.I. (1995)** *Cartographic Projection Procedures for the UNIX Environment – A User's Manual*, United States Department of the Interior Geological Survey, Open-File Report 90-284.
- Gassmann A. (2013)**. A global hexagonal C-grid non-hydrostatic dynamical core (ICON-IAP) designed for energetic consistency. *Q. J. R. Meteorol. Soc.* 139: 152–175. DOI:10.1002/qj.1960
- Galperin, B., L.H. Kantha, S. Hassid and A. Rosati (1988)** A quasi-equilibrium turbulent energy model for geophysical flows. *J. Atmos. Sci.*, 45, 55 – 62.

## SHOC User Manual

- Gill, A. E. (1982)** Atmosphere-Ocean Dynamics. *Academic Press Inc.*
- Griffies, S.M., Hallberg, R.W. (2000)** Biharmonic friction with a Smagorinsky-like viscosity for use in large-scale eddy-permitting ocean models. *Mon. Wea. Rev.*, 128, 2935-2946.
- Gottlieb (2005)** On high order strong stability preserving Runge–Kutta and multi step time discretizations. *J. Scientific Comput.* 25, 105-128.
- Grant, W.D. and O.S. Madsen (1986)** The continental shelf bottom boundary layer, *Ann. Rev. Fluid Mech.*, 18, 265-305.
- Harcourt, R.R. (2015)** An improved second-moment closure model of Langmuir turbulence. *Journal of Physical Oceanography*, 45, 84-103.
- Herzfeld, M. (2006)** An alternative coordinate system for solving finite difference ocean models. *Ocean Modelling*, 14, 174 – 196.
- Herzfeld, M., Andrewartha, J.R. (2012)** A simple, stable and accurate Dirichlet open boundary condition for ocean model downscaling. *Ocean Modelling*, 43-44, 1-21.
- Herzfeld, M. and M. Tomczak (1999)** Bottom driven upwelling generated by eastern intensification in closed and semi-closed basins with a sloping bottom. *Mar. Freshwater Res.*, 50 (7), 613 – 627.
- Herzfeld, M, J. Waring, J. Parslow, N. Margvelashvili, P. Sakov and J. Andrewartha (2002)** SHOC : Model for estuaries and coastal oceans, scientific manual. CSIRO Marine Research.
- Herzfeld, M., Gillibrand, P.A. (2015)** Active open boundary forcing using dual relaxation time-scales in downscaled ocean models. *Ocean Modelling*, 89, 71-83.
- Herzfeld, M., Rizw, F. (2019)** A two-way nesting framework for ocean models. *Environmental modeling and software*, 117, 200-213. <https://doi.org/10.1016/j.envsoft.2019.03.015>
- Israeli, M. and S.A. Orszag (1981)** Approximation of radiation boundary conditions. *J. Comput. Physics*, 41, 115 – 135.
- Jones, N.L., Monosmith, S.G. (2008)** Modelling the influence of wave-enhanced turbulence in a shallow tide- and wind-driven water column. *J. Geophys. Res.*, 113, C03009, doi:10.1029/2007JC004246.
- Kitaigorodskii, S.A., O. A. Kuznetsov and G. N. Panin (1973)** Coefficients of drag, sensible heat and evaporation in the atmosphere over the surface of the sea. *Izv. Acad. Sci. USSR, Atmos. Ocean Phys.*, 9, 644-647.
- Kondo, J. (1975)** Air-sea bulk transfer coefficients in diabatic conditions. *Boundary-Layer Meteorology*, 9, 91-112.
- Kowalik, Z. and T.S. Murty (1993)** Numerical modelling of ocean dynamics. BULK series on ocean engineering, Volume 5. World Scientific, Singapore. 481pp.
- Large, W.G. and S. Pond (1981)** Open ocean momentum flux measurements in moderate to strong winds, *J. Phys. Oceanogr.*, 11, 324-336.
- Large, W.G. and S. Pond (1982)** Sensible and latent heat flux measurements over the ocean. *J. Phys. Oceanogr.*, 12, 464-482.
- Leonard, B.P. (1991)** The ULTIMATE conservative difference scheme applied to unsteady one-dimensional advection. *Comp. Methods in Appl. Mech. and Eng.*, 19, 17 – 74.
- Leonard, B.P., Lock, A.P. MacVean, M.K. (1996)** Conservative explicit unrestricted-time-step multidimensional constancy-preserving advection schemes. *Mon. Wea. Rev.*, 124, 2588-2606.
- Lin, S., Rood, R.B. (1996)** Multidimensional flux-form semi-Lagrangian transport schemes. *Mon. Wea. Rev.*, 124, 2046-2070.
- Madsen, O. S. (1994)** Spectral wave-current bottom boundary layer flows, in *Coastal engineering 1994 Proceedings, 24<sup>th</sup> international conference Coastal engineering Research Council/ASCE*, pp. 384-398.
- Masagutov, T. F. (1981)** Calculation of vertical turbulent fluxes in the near-water atmospheric layer over the ocean in tropical latitudes. *Meteor. Gidrol.*, 12, 61-68.
- Martinsen, E.A. and H. Engedahl (1987)** Implementation and testing of a lateral boundary scheme as an open boundary condition in a barotropic ocean model. *Coastal Eng.*, 11, 603-627.
- Mellor, G.L. and T. Yamada (1982)** development of a turbulence closure model for geophysical fluid problems. *Rev. Geophys.*, 20, 851 – 875.
- Mesinger F. and A. Arakawa (1976)** Numerical methods used in atmospheric models, GARP Publ. Ser. No. 17 WMO-ICSU.
- Müller, P. (1995)** Ertel's potential vorticity theorem in physical oceanography. *Reviews of Geophysics*, 33, 67-97.



## SHOC User Manual

- Miller, M.J. and A.J. Thorpe (1981)** Radiation conditions for the lateral boundaries of limited-area numerical models. *Q. J. R. Meteorol. Soc.*, 107, 615 - 628.
- Moon, I. (2005)** Impact of a coupled ocean-tide-circulation system on coastal modelling. *Ocean Modelling*, 8, 203-236.
- Orlanski, I (1976)** A simple boundary condition for unbounded hyperbolic flows. *J. Comput. Physics*, 21, 251 – 269.
- Palma, E.D. and R.P. Matano (1998)** On the implementation of passive open boundary conditions for a general circulation model: The barotropic mode. *J. Geophys. Res.*, 103(C1), 1319 - 1341.
- Pielke, R.A., W.R. Cotton, R.L. Walko, C.J. Tremback, W.A. Lyons, L.D. Grasso, M.E. Nicholls, M.D. Moran, D.A. Wesley, T.J. Lee, and J.H. Copeland (1992)** A comprehensive meteorological modeling system -- RAMS. *Meteorol. Atmos. Phys.*, 49, 69-91.
- Ringler, T.D., Thuburn, J., Klemp, J.B., Skamarock, W.C. (2010)** A unified approach to energy conservation and potential vorticity dynamics for arbitrarily-structured C-grids. *J. Comput. Phys.* 229, 3065-3090.
- Romanou, A., Rossow, W.B., Chou, S., (2006)** Decorrelation scales of high-resolution turbulent fluxes at the ocean surface and a method to fill in gaps in satellite data products. *Journal of Climate*, 19, 3378 – 3393.
- Sakamoto, K., Tsujino, H. Nakano, H., Hirabara, M., Yamanaka G. (2013)** A practical scheme to introduce explicit tidal forcing into an OGCM. *Ocean Sci.*, 9, 1089–1108.
- Schiller, A., Godfrey, J.S. (2003)** Indian Ocean intraseasonal variability in an ocean general circulation model. *Journal of Climate*, 16, 21-39.
- Simons, T.J. (1974)** Verification of numerical models of lake Ontario. Part I, circulation in spring and early summer. *Journal of Physical Oceanography*, 4, 507 - 523.
- Shapiro, R. (1970)** Smoothing, filtering, and boundary effects. *Reviews of Geophysics and Space Physics*, 8, 359 – 387.
- Shu and Osher (1998)** Efficient implementation of essentially non-oscillatory shock-capturing schemes. *J. Comput. Phys.* 77, 439-471.
- Skamarock WC, Klemp JB, Duda MG, Fowler L, Park SH. (2011).** A multi-scale onhydrostatic atmospheric model using centroidal Voronoi tessellations and C-grid staggering. *Mon. Weather Rev.* DOI:10.1175/MWR-D-11-00215.1.
- Sommerfeld, A. (1949)** Partial differential equations, *Lect. Theoret. Phys.*, vol 6, Academic, San Diego.
- Spiteri and Ruuth (2002)** A new class of optimal high-order strong-stability-preserving time discretization methods. *SIAM J. Numer. Anal.*, 40, 469-491.
- Tartinville, B., E. Deleersnijder and J. Rancher (1997)** The water residence time in the Mururoa atoll lagoon: sensitivity analysis of a three-dimensional model. *Coral Reefs*, 16, 193 – 203.
- Weller, H. (2012)** Controlling the Computational Modes of the Arbitrarily Structured C Grid. *Mon. Wea. Rev.*, 140, 3220-3234.
- Wilcox, D.C. (1988)** Reassessment of the scale-determining equation for BULK turbulence models. *AIAA Journal*, 26(11), 1299-1310.
- Yu, Y.G., Wang, N., Middlecoff, J., Peixoto, P.S., Govett, M.W., (2020).** Comparing numerical accuracy of icosahedral A-Grid and C-Grid schemes in solving the shallow-water model. *Mon. Wea. Rev.*, 148, 4009-4033.

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